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UAH MATHEMATICAL MODEL OF THE VARIABLE
POLARITY PLASMA ARC WELDING SYSTEM CALCULATION

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ABSTRACT

Significant advantages of Variable Polarity Plasma Arc (VPPA) welding process include faster welding, fewer repairs, less joint preparation, reduced weldment distortion, and absence of porosity. In this report, a mathematical model is presented to analyze the VPPA welding process. Results of the mathematical model have been compared with the experimental observation accomplished by the GDI team.

I. INTRODUCTION

The plasma arc is a concentrated energy source commonly used in welding and cutting processes. It is composed of a partially ionized gas stream produced by forcing an inert gas to flow through an electric arc and emerge from a constricting nozzle. With its high energy density and velocity, the plasma arc, when impinging on the workpiece, can create a hole in the molten pool generated by its heat and can penetrate through the workpiece. Depending on the operating parameters employed, this hole may either become self-healing or remain open as the arc transverses along the workpiece. A "keyhole" welding process occurs in the self-healing case, in which the molten metal in front of the arc flows around the arc column and resolidifies behind the arc. On the other hand, a cutting operation is achieved if the hole remains open (O'Brien, 1968).

The plasma welding process is essentially an extension of gas tungsten-arc welding (GTAW); however, constraining the arc to flow through a nozzle produces much higher energy density in the arc and much higher gas velocity and momentum. The process produces deep penetration welds by forming a keyhole in the workpiece by the pressure of the gas flow. The metal melted in front of the advancing keyhole flows around to the rear where it solidifies to form the weld bead. This is distinct from the essentially surface melting produced by the GTAW process (which cannot normally penetrate to a depth equal to the width of a weld pool).

In 1955 Linde Air Products introduced a plasma arc torch for metal cutting applications, and by 1965 Linde had developed an automatic plasma arc welding facility for Westinghouse Electric Corporation to fabricate a 120 in. diameter, 3/8 in. thick D6AC steel rocket motor case for the Titan III-C booster assembly (Miller and Filipski, 1966; Privoznik and Miller, 1966). The plasma arc welding process was reported to halve the welding time required. Then in 1965 Thermal Dynamics Corporation reported the use of direct current reversed polarity (workpiece negative) plasma arc to join 1/4 in. thick aluminum plate (Cooper et al., 1965). At the end of the 1960's, Van Cleave at the Boeing Company began his efforts to combine the plasma arc process with a variable polarity feature in which the electrode polarity was periodically reversed. Alternating electrode potential for aluminum welding had been investigated as early as 1947 (Herbst, 1947). Difficulties with welding power supplies in this application were evident early-on. In addition, when variable polarity plasma arc (VPPA) welding was used in the U.S. Army Roland Missile Production Program, development problems such as arc pressure pulsation were noted (Nunes et al., 1981; 1983). As a result of Van Cleave's promising work at Boeing, a VPPA research and development project was initiated in 1978 at the NASA Marshall Space Flight Center, to determine the potential for replacing the GTAW system used in the fabrication of the Space Shuttle External Tank (ET). After the original used in the fabrication and process were

improved, VPPA welding finally exceeded the expectations (Nunes et al., 1984a; 1984b).

The Space Shuttle ET (diameter 28.6 ft., length 154 ft.) is the largest known "drop tank," carrying 140,000 gallons of liquid oxygen and 380,000 gallons of liquid hydrogen. From the outset of ET production, the conventional GTAW system operating in the direct current electrode negative mode was used. With the GTAW system, in spite of the requisite careful joint preparation, weld porosity and defects had been ever-present problems since the fabrication of the Saturn lunar rocket first stage. Therefore, the decision was made at the outset to use 100% radiographic inspection. Weld porosity and defects had to be ground out and repaired systematically.

The VPPA process significantly reduced porosity and defects with less stringent joint preparation and, in addition, reduced weldment distortion, and speeded up the welding process.

In this study, the power distribution for an argon plasma gas has been analyzed along its course through the VPPA welding system. The study includes the following sections:

- (1) Electric potential distribution of straight and reverse polarities, and potential intensities for the VPPA welding system;
- (2) VPPA welding system electric power input at the electrode, within orifice, in the free plasma jet column and in the keyhole of workpiece;

- (3) Power loss at electrode, within the gap between electrode and within orifice, standoff column and the workpiece;
- (4) Determination of plasma arc enthalpy;
- (5) Determination of crown and root bead widths;
- (6) Determination of crown and root heights;
- (7) Determination of leading edge angle of keyhole.
- (8) Comparison between modeling and experimental measurements

II. VARIABLE POLARITY PLASMA ARC WELDING SYSTEM

ELECTRIC POTENTIAL CALCULATION

The significant current carriers in a welding arc are electrons and positive ions. Electrons carry the bulk of the current, moving rapidly from negative cathode to positive anode. The positive ions drift more slowly through the interelectrode space. In a fixed polarity arrangement, the differential drift rate results in an asymmetrical heating of the welding arc's ends. The cathode receives less heat and the anode more heat. The straight polarity mode of operation entails a negative electrode (cathode) and a positive workpiece (anode). Where the primary object of the weld process is to deliver the maximum heat to the workpiece with minimum deterioration of the electrode, straight polarity is used.

Reverse polarity, which entails positive electrode and negative workpiece, has the advantage that the workpiece is subjected to a cleaning process (cathodic cleaning) by the impingement of positive ions on the workpiece surface. Recent work suggests that heavy positive ion weight is irrelevant to the cleaning process which seems to be more like capacitor breakdown than hammer impact. In the case of plasma arc welding, reverse polarity action appears to condition the surface of the aluminum alloy so that the molten metal flows easily and controllably under the arc. It is conjectured that this fluid control is accomplished through breaking up of surface oxide films. Cutoff of reverse

polarity during VPPA welding transforms a weld metal flow which closes smoothly and soundly behind the keyhole to an irregular, intermittent, globular flow. This process leaves a rough, lumpy bead sunken below the parent metal surface and protruding jaggedly from the root of the weld. However, continuous reverse polarity is not necessary to provide adequate cathodic cleaning action.

The variable polarity square-wave with unequal straight and reverse polarity time intervals offered a combination of the high heating capability of straight polarity with the cleaning feature of reverse polarity. Adequate cleaning is obtained by incorporating a relatively short ($1/10$ to $1/5$ the duration of the straight polarity current) pulse of reverse polarity current into the welding current waveform.

Figure 1 shows the VPPA electric power system. During the straight polarity mode of operation, it employs a negative electrode (cathode) and a positive workpiece (anode); during the reverse polarity mode of operation it employs a positive electrode and a negative workpiece. Figure 1 at left illustrates the straight polarity mode; at right, reverse polarity mode.

Calculation of electric potential can be obtained from the following formulations:

(A) For Straight Polarity

$$V_E = V_F - \Delta V_a - \phi_w$$

$$V_G = V_E - \sum_i \left(\frac{dV}{dL} \right)_{3,i} \Delta L_{3,i}$$

$$V_C = V_G - \sum_i \left(\frac{dV}{dL} \right)_{2,i} \Delta L_{2,i}$$

$$V_D = V_C + \Delta V_a + \phi_M$$

$$V_B = V_C - \sum_i \left(\frac{dV}{dL} \right)_{1,i} \Delta L_{1,i}$$

$$V_A = V_B - \Delta V_c + \phi_E$$

$$\Delta V_m^+ = \Delta V_{FA} = V_F - V_A = -V_A$$

$$\Delta V_p^+ = \Delta V_{DA} = V_D - V_A$$

where ϕ_E = Electrode Work Function

ϕ_M = Orifice Work Function

ϕ_w = Workpiece Work Function

ΔV_a = Anode Drop

ΔV_c = Cathode Drop

$\left(\frac{dV}{dL} \right)_{1,i}, \left(\frac{dV}{dL} \right)_{2,i}, \left(\frac{dV}{dL} \right)_{3,i}$ = Electric Potential Intensities in segment i of L_1 , L_2 and L_3 , respectively

$\Delta L_{1,i}, \Delta L_{2,i}, \Delta L_{3,i}$ = Length of segment i in L_1 , L_2 , and L_3 , respectively

(B) For Reverse Polarity

$$V_E' = V_F' + \Delta V_c - \phi_w + \epsilon_R$$

$$V_G' = V_E' + \sum_i \left(\frac{dV}{dL} \right)_{3,i} \Delta L_{3,i}$$

$$V_C' = V_G' + \sum_i \left(\frac{dV}{dL} \right)_{2,i} \Delta L_{2,i}$$

$$V_D' = V_C' - \sum_i \left(\frac{dV}{dL} \right)_{2,i} \Delta L_{2,i} + \Delta V_a + \phi_X$$

$$V_B' = V_C' + \sum_i \left(\frac{dV}{dL} \right)_{1,i} \Delta L_{1,i}$$

$$V_A' = V_B' + \Delta V_a + \phi_E$$

$$\epsilon_R = \text{Reverse Polarity Rise} = A + B \frac{t_-}{t_+ + t_-}$$

where A, B = constant varying with workpiece materials

t_+ = Straight Polarity Time Period

t_- = Reverse Polarity Time Period

$$\Delta V_m^- = \Delta V_{A \cdot F} = V_{A \cdot} - V_{F \cdot} = V_{A \cdot}$$

$$\Delta V_p^- = \Delta V_{A \cdot D} = V_{D \cdot} - V_{A \cdot}$$

(C) For Potential Intensities

Electric potential intensities of the plasma fluid in the plasma column can be calculated from the electric conductivity, σ_E , of plasma fluid at the location of interest. The value of electric conductivity at the location of interest is determined by the local plasma jet pressure and temperature. By using the data provided by Devoto (1973), Lancaster (1986) has calculated the electrical conductivity of argon plasma gas as it varies with temperature at one atmosphere pressure. Figure 2 shows the variation of argon gas electrical conductivity with temperature at one atmospheric pressure. In this model

calculation, we have divided the lengths of plasma column along the axial direction into several segments with ΔL_i as the length of segment i . Joule heating, and radiative and convective heat transfer losses at the segment i are calculated with the assumed value of electric potential intensity of that segment, $(\Delta V/\Delta L)_i'$, and the given inlet values of power and enthalpy of plasma fluid at that segment. Outlet values of power and enthalpy of plasma fluid at that segment are then calculated based on these parameters. The value of electric conductivity $\sigma_{E,i}$ at segment i is thus determined from the average fluid temperature at that segment. The value of average temperature is obtained from the corresponding average value of plasma fluid enthalpy at that segment which is calculated from the average value of inlet and outlet plasma fluid enthalpies at that segment. Electrical resistance, R_i ; electric potential difference, ΔV_i ; and electric field intensity, $(\Delta V/\Delta L)_i$, at segment i can be determined from the computed value of electric conductivity $\sigma_{E,i}$ at that segment. Convergent solution is obtained through the trial and error computations between the computed value of $(\Delta V/\Delta L)_i$ and the assumed value of $(\Delta V/\Delta L)_i'$ at segment i . From these calculations, it is clearly shown that the values of electric potential of the plasma fluid and heat transfer computations are mutually coupled together. Furthermore, the values of plasma

electrical conductivity fluctuate with local variations of temperature. The physical parameters affecting the plasma temperature, such as plasma and shielding gas flow rates, radiative and convective heat transfer losses, values of main and pilot electric currents, standoff distance, etc., all influence the values of electric potential and electric field intensity in the plasma fluid.

The effect of shielding gas flow rate occurs through shielding gas mixing into the plasma standoff column L_3 and vice versa. The continuous mixing between plasma gas and shielding gas induced by the plasma jet stream in plasma column results in local variations of species constituent concentration and temperature along the axial direction. Thus, the effect of jet mixing in column streams between plasma and shielding gases must be taken into consideration in addition to heat transfer losses in computing electric potential along the plasma jet. Figure 3 shows the variation of electrical resistance with temperature for various argon-helium mixtures.

III. VPPA WELDING SYSTEM ELECTRIC POWER INPUT

VPPA Electric Power Input can be calculated as follows:

$$P_{total} = \frac{I_m^+ \Delta V_m^+ t_+ + I_p^+ \Delta V_p^+ t_+ + I_m^- \Delta V_m^- t_- + I_p^- \Delta V_p^- t_-}{t_+ + t_-} \quad (3-1)$$

where I_m^+ = Straight Polarity Main Current

I_p^+ = Straight Polarity Pilot Current

I_m^- = Reverse Polarity Main Current

I_p^- = Reverse Polarity Pilot Current

Equation (3-1) is the total electric power input of the system which is the summation of power input for the plasma arc jet in the gap between electrode and orifice, power input within orifice, power input in free jet column (standoff), and power input within keyhole of workpiece.

The power input can be itemized, and calculated as follows:

(III-A) Power Input at the Electrode

$$P_E = \frac{(I_m^+ + I_p^+) (\Delta V_c - \phi_E) t_+ + (I_m^- - I_p^-) (\Delta V_A + \phi_E) t_-}{t_+ + t_-} \quad (3-2)$$

(III-B) Power Input in the Gap Between Electrode and Orifice

(Joule Heating)

$$P_{J,1} = \frac{(I_m^+ + I_p^+) \left[\sum_i \left(\frac{dV}{dL} \right)_{1,i} \Delta L_{1,i} \right] t_+ + (I_m^- - I_p^-) \left[\sum_i \left(\frac{dV}{dL} \right)_{1,i} \Delta L_{1,i} \right] t_-}{t_+ + t_-} \quad (3-3)$$

(III-C) Power Input Within Orifice

This includes power input through the work function of metal

$$P_{M,1} = \frac{I_p^+ \phi_M t_+ + I_p^- \phi_M t_-}{t_+ + t_-} \quad (3-4)$$

Power input through anode drop,

$$P_{M,2} = \frac{I_p^+ \Delta V_a t_+ + I_p^- \Delta V_a t_-}{t_+ + t_-} \quad (3-5)$$

and power input through Joule heating within the orifice

$$P_{J,2} = \frac{I_m^+ \left[\sum_i \left(\frac{dV}{dL} \right)_{2,i} \Delta L_{2,i} \right] t_+ + (I_m^- - I_p^-) \left[\sum_i \left(\frac{dV}{dL} \right)_{2,i} \Delta L_{2,i} \right] t_-}{t_+ + t_-} \quad (3-6)$$

(III-D) Power Input in the Free Plasma Jet Column (Standard)
(Joule Heating)

$$P_{J,3} = \frac{I_m^+ \left[\sum_i \left(\frac{dV}{dL} \right)_{3,i} \Delta L_{3,i} \right] t_+ + I_m^- \left[\sum_i \left(\frac{dV}{dL} \right)_{3,i} \Delta L_{3,i} \right] t_-}{t_+ + t_-} \quad (3-7)$$

It is important to note that shielding gas surrounding the plasma jet, is induced into the plasma jet column due to the flow generated by the plasma jet stream. Power of shielding gas introduced into the plasma jet, $P_{s,d}$, shown in Equation (4-29), shall be included as a part of the plasma jet power input, in addition to the power input shown in Equation (3-7).

(III-E) Power Input in the Keyhole of Workpiece

This includes power input through the work function of metal and reverse polarity potential rise

$$P_{V,1} = \frac{I_m^+ \phi_w t_+ + I_m^- (\epsilon_R - \phi_w) t_-}{t_+ + t_-} \quad (3-8a)$$

and power input through anode and cathode drops

$$P_{w,2} = \frac{I_m^+ \Delta V_a t_+ + I_m^- \Delta V_c t_-}{t_+ + t_-} \quad (3-8b)$$

(III-F) Total Power Input to the VPPA Welding System

Total power input of VPPA welding system, shown in Equation (3-1) shall be equal to the summation of power input shown in Equation (3-2) to (3-8) and plasma jet induced shielding gas power input, P_{sd} , namely

$$P_{total} = P_E + P_{J,1} + P_{M,1} + P_{M,2} + P_{J,2} + P_{J,3} + P_{V,1} + P_{V,2} + P_{sd} \quad (3-9)$$

IV. POWER LOSS CALCULATION OF VPPA WELDING SYSTEM

(IV-A) Electrode Heat Conduction Loss

A one-dimensional formulation of the electrode heat conduction loss is given by

$$Q_E = k_E \cdot A_E \frac{(T_E - T_0)}{L_E} \quad (4-1)$$

where

Q_E = Electrode Heat Conduction Loss

k_E = Thermal Conductivity Coefficient of Electrode

A_E = Cross-sectional Area of Electrode

L_E = Length of Electrode (from tip to water-cooled collet)

$T_E - T_0$ = Temperature Difference of Electrode Between Tip and
Collet Position

(IV-B) Radiation Heat Loss Between Electrode and Orifice

Plasma arc heat radiation loss within the gap between electrode and orifice can be computed from the following equation (Evans and Tankin, 1967; Cram, 1985):

$$Q_G(W) = V_G(m^3) (4 \times 10^{10}) \left[\frac{T(^{\circ}K)}{15000} \right]^{16} / \left\{ 1 + \left[\frac{T(^{\circ}K)}{15000} \right]^{16} \right\} \quad (4-2)$$

where

Q_G = Heat Radiation Loss Within the Gap Between Electrode
and Orifice (W)

V_G = Plasma Arc Jet Volume Within Gap Between Electrode
and Orifice (m^3)

T = Absolute Temperature ($^{\circ}K$)

(IV-C) Power Loss Within the Orifice

Power Loss within the orifice is comprised of the following items:

(IV-C-1) Heat Convection Loss Within the Orifice

Heat convection loss within the orifice can be computed from the following formulation of convective heat transfer model (Hsu and Rubinsky, 1987):

$$Nu = 0.2233(X^+)^{-0.7455} + 3.66 \quad (4-3)$$

where

$$X^+ = \frac{X}{R_0} \cdot \frac{1}{(Re \cdot Pr)_m}$$

Here

X = Axial Distance, (Distance from the entrance of orifice to the half distance of the segment of interest)

R_0 = Radius of Orifice

Re = Reynolds Number of Plasma Arc Fluids

Pr = Prandtl Number of Plasma Arc Fluids

Nu = Nusselt Number of Plasma Arc Fluids

Subscript m = mean values

Heat convection loss within the orifice, thus, can be computed from the Nusselt number obtained from Equation (4-3), namely,

$$Q_{N,c} = Nu \cdot A_N \cdot \frac{k}{D} \cdot \frac{(h_{\text{plasma}} - h_N)}{c_p} \quad (4-4)$$

where

$Q_{N,c}$ = Heat Convection Loss within the Orifice

A_N = Heat Transfer Area of Segment of Interests

D = Diameter of Orifice = $2 R_o$
 k = Thermal Conductivity of Plasma Arc
 c_p = Constant Pressure Specific Heat of Plasma Arc
 h_{plasma} = Average Enthalpy of Plasma Arc through the Orifice
 h_N = Average Enthalpy of plasma in Orifice corresponding to the Orifice Wall Temperature

All thermal properties used in this model are determined at the temperature corresponding to the average enthalpy of plasma arc.

(IV-C-2) Direct Power Loss to Surface of Orifice

Direct power loss to the orifice surface includes $P_{N,1}$, orifice work function induced power input; and part of $P_{N,2}$, orifice anode drop induced power input, namely

$$Q_{N,G} = P_{N,1} + \psi P_{N,2} \quad (4-5)$$

where,

$Q_{N,G}$ = Direct power loss from the orifice surface

ψ = Fraction power generated by anode drop lost to orifice

$(1-\psi)P_{N,2}$ = Plasma arc power input from power generated at orifice anode drop

(IV-C-3) Electron Collision Power Loss Within Orifice

Power loss due to free electrons entering the surface of orifice can be calculated from the following equation:

$$Q_{N,e} = \frac{I}{e} \left(\frac{3}{2} KT \right) \quad (4-6)$$

where

$Q_{N,e}$ = Free electron power loss to the orifice

e = Electron charge = 1.602×10^{-19} coulomb/mole

K = Boltzman constant = 1.38×10^{-16} erg/mol.K

T = Plasma arc temperature;

and I is the electric current which can be computed as follows:

$$I = \frac{I_p^+ t_+ + I_p^- t_-}{t_+ + t_-} \quad (4-7)$$

Total power loss in orifice, Q_N , is the summation of Equations (4-4), (4-5), and (4-6), namely,

$$Q_N = Q_{N,c} + Q_{N,g} + Q_{N,e} \quad (4-8)$$

(IV-D) Power Loss from Standoff Column

Power loss from the standoff column includes radiative heat loss, $Q_{s,r}$, and convective heat loss, $Q_{s,c}$.

Calculation of radiative heat loss is similar to Equation (4-2) for that in the gap between electrode and orifice, namely

$$Q_{s,r}(W) = V_s(m^3) (4 \times 10^{10}) \left[\frac{T(^{\circ}K)}{15000} \right]^{16} \left/ \left\{ 1 + \left[\frac{T(^{\circ}K)}{15000} \right]^{16} \right\} \right. \quad (4-9)$$

where V_s denotes plasma arc volume within the standoff column; and T is the absolute temperature corresponding to the average value of plasma arc enthalpy.

Radiative heat loss is strongly dependent on fluid temperature. This and what follows require trial and error computations.

To compute the convective heat loss, $Q_{s,c}$, from the standoff column, jet stream mixing theory is employed. Turbulent mixing between plasma jet and the surrounding shielding gas is shown schematically in Figure 4a. r_1 stands for the inner boundary of jet boundary layer, and r_2 expresses the outer boundary of jet boundary

layer. Both are functions of axial distance x from the outlet end of the orifice. The inner jet core region, surrounded by $r_1(x)$ is a non-perturbed zone of jet core. The jet boundary layer lies between $r_2(x)$ and $r_1(x)$. Jet stream parameters in the jet boundary layer, including velocity, temperature and species concentration, vary from original (pure plasma gas jet) parameters at $r = r_1$ to ambient (pure shielding gas) parameters at $r = r_2$. The jet core extends to $x = x_H$. As $x > x_H$, the jet core disappears and the jet boundary layer occupies the entire extent from $r = 0$ to $r = r_2$. The initial region from $x = 0$ to $x = x_H$ is the region of jet mixing. Boundary thickness at transition $x = x_H$ is $r_{2,H}$.

Based on the formulations of Abramovich (1963), the boundary layer within the initial region of jet mixing is governed by the following equations:

$$\frac{R_0 - r_1}{cx} = \frac{1 - m}{1 + m} \left[0.416 + 0.134m + 0.021 \frac{cx}{R_0} \left(\frac{1 - m}{1 + m} \right) \cdot (1 + 0.8m - 0.45m^2) \right] \quad (4-10)$$

$$\frac{R_0 - r_1}{r_2 - r_1} = 0.416 + 0.134m + 0.021 \frac{(r_2 - r_1)}{R_0} (1 + 0.8m - 0.45m^2) \quad (4-11)$$

where R_0 denotes the radius of orifice; r_1 , the radius of inner boundary of jet boundary layer; r_2 , the radius of outer boundary of jet boundary layer; and x , the axial distance from the outlet end of orifice to the point of interest. $m = u_H/u_0$, where u_H is ambient fluid velocity; and u_0 , the original jet flow velocity inside jet core. c is empirical constant which is 0.27 when $u_0 \gg u_H$.

Substituting the values of $m = 0$ and $c = 0.27$ in Equations (4-10) and (4-11), we have

$$\frac{R_0 - r_1}{x} = 0.27 \left(0.416 + 0.00567 \frac{x}{R_0} \right) \quad (4-12)$$

$$\frac{R_0 - r_1}{r_2 - r_1} = 0.416 + 0.021 \left(\frac{r_2 - r_1}{R_0} \right) \quad (4-13)$$

From equation (4-12), we can solve for the jet inner boundary r_1 in term of the axial distance x which is given by

$$\frac{r_1}{R_0} = 1 - 0.1123 \frac{x}{R_0} - 0.0015 \left(\frac{x}{R_0} \right)^2 \quad (4-14)$$

Similarly, from Equation (4-13), we can determine the boundary layer thickness, $r_2 - r_1$, i.e.,

$$r_2 - r_1 = \frac{1}{2} \{ -19.81R_0 + [392.44R_0^2 + 190.48 (R_0 - r_1) R_0]^{1/2} \} \quad (4-15)$$

To determine the axial distance of jet initial region x_H , we can solve Equation (4-14) by substituting $r_1 = 0$, i.e.,

$$\frac{x_H}{R_0} = 8 \quad (4-16)$$

In our case, the radius of orifice $R_0 = 1.5875$ mm, and the axial distance of the jet initial region $x_H = 8(1.5875) = 12.7$ mm. In the present study, the range of standoff distance considered is between 1 to 10 mm, so that all standoff values considered in the present study lie within the range of the initial region of jet mixing. Let us consider velocity, temperature and species concentration profiles within the range of jet initial region as follows:

$$\frac{u_0 - u}{u_0 - u_H} = (1 - \eta^{1.5})^2 \quad (4-17)$$

$$\frac{T_0 - T}{T_0 - T_H} = 1 - \eta \quad (4-18)$$

$$\frac{\rho_{p1}}{\rho_{p1} + \rho_{sd}} = \eta \quad (4-19)$$

where u_0 and T_0 denote original velocity and temperature of jet core, respectively; and u_H and T_H , the ambient velocity and temperature at the outer layer of jet boundary layer, respectively. Dimensionless coordinate parameter $\eta = (r_2 - r)/(r_2 - r_1)$. ρ_{sd} and ρ_{p1} denote masses of shielding gas and plasma gas per unit of volume within the jet boundary layer, respectively.

In the present model, the effect of the mole fraction of shielding gas induced by jet mixing into the plasma column has been fully taken into consideration.

It is convenient to employ partial pressure P_{p1} and P_{sd} , rather than density in the calculation. By using equation of state, Equation (4-19) can be rewritten as

$$\frac{P_{sd}}{P_{p1}} = \frac{M_{p1}}{M_{sd}} \left(\frac{1}{\eta} - 1 \right) \quad (4-20)$$

Since

$$P_{p1} + P_{sd} = P_H \quad (4-21)$$

We can solve partial pressure P_{p1} and P_{sd} from Equations (4-20) and (4-21) as follows:

$$P_{p1} = \frac{P_H}{\left[1 + \frac{M_{p1}}{M_{sd}} \left(\frac{1}{\eta} - 1 \right) \right]} \quad (4-22)$$

and

$$P_{sd} = P_H - P_{p1} \quad (4-23)$$

where P_{p1} and P_{sd} denote partial pressures of plasma and shielding gases, respectively; and M_{p1} and M_{sd} stand for molecular weights of plasma and shielding gases, respectively. For example, $M_{p1} = 39.95$ kg/k-mol for argon gas, and $M_{sd} = 4.003$ kg/k-mol for helium gas. Also, P_H is ambient pressure of gases.

Plasma and shielding gas density, ρ_{p1} and ρ_{sd} , can be determined from Equation (4-18) for temperature profile and Equations (4-22) and (4-23) for partial pressure of plasma and shielding gases, i.e.,

$$\rho_{p1} = \frac{P_{p1} M_{p1}}{R T} \quad (4-24)$$

$$\rho_{sd} = \frac{P_{sd} M_{sd}}{R T} \quad (4-25)$$

where R denotes the universal gas constant which is 8315 J/kmol·K. Furthermore, plasma and shielding gas enthalpies can be obtained from the table at their corresponding values of temperature. Finally, jet stream power P_{Jet} can be calculated from the following integration.

$$P_{Jet} = \int_0^{r_2} 2\pi r u (\rho_{p1} h_{p1} + \rho_{sd} h_{sd}) dr \quad (4-26)$$

It is noted that $\rho_{p1} = (\rho_{p1})_0$, $(\rho_{sd})_0 = 0$, $h_{p1} = (h_{p1})_0$, and $u = u_0$ within the region of jet core. Thus, Equation (4-26) can

be rewritten as follows:

$$P_{jet} = \pi r_1^2 u_0 (\rho_{p1})_0 (h_{p1})_0 + \int_{r_1}^{r_2} 2\pi r u (\rho_{p1} h_{p1} + \rho_{sd} h_{sd}) dr \quad (4-27)$$

At the outlet end of standoff column, the total power of plasma jet can be expressed as

$$P'_{j,0} = P_{j,1} + P_{j,3} - Q_{s,r} + P_{s,d} \quad (4-28)$$

where $P_{j,1}$ denotes the plasma jet power at the inlet end of standoff column (or at the outlet end of orifice); $P_{j,3}$, the plasma jet power due to Joule heating within the standoff column; $Q_{s,r}$, the radiative heat power loss from the standoff column; and $P_{s,d}$, the induced power from surrounding shielding gas into plasma jet boundary layer, namely,

$$P_{s,d} = \dot{m}_{sd} h_{sd,H} \quad (4-29)$$

Here, $h_{sd,H}$ denotes shielding gas enthalpy corresponding to the ambient temperature of shielding gas; \dot{m}_{sd} , mass flow rate of shielding gas

$$\dot{m}_{sd} = \int_{r_1}^{r_2} 2\pi r u \rho_{sd} dr \quad (4-30)$$

In this calculation, total power of plasma jet $P'_{j,0}$ shown in Equation (4-28), contains the power within the whole cross section of jet boundary layer where temperature varies radially from more than 10^4 K at the inner layer of jet boundary layer to ambient temperature (say 298 °K) at the outer layer of jet boundary layer. The welding process requires sufficiently high temperature difference to maintain heat conduction and to promote sufficient heat flow to melt

the workpiece metal. More important than promoting heat flow by convection is the maintenance of a conducting plasma path for current. Spot welding electrodes do not have to be hot at all to provide a molten weld nugget by resistance heating. Resistance heating due to plasma sheath voltage drop and work function drop are more important (Eckert and Pfender, 1967).

Let R_c be a half size of the crown width. This is also equivalent to the radius of the inlet end of keyhole (See Figure 4b). As $R_c \leq r_2$,

$$P_{3,0} = \int_0^{R_c} 2\pi r u (\rho_{p1} h_{p1} + \rho_{sd} h_{sd}) dr \quad (4-31)$$

and as $R_c > r_2$,

$$P_{3,0} = \int_0^{r_2} 2\pi r u (\rho_{p1} h_{p1} + \rho_{sd} h_{sd}) dr + \pi(R_c^2 - r_2^2) u_H \rho_{sd} \quad (4-32)$$

The difference between $P'_{3,0}$, calculated from Equation (4-28), and $P_{3,0}$, calculated from Equations (4-31) or (4-32), is the convective heat loss or power increment due to injecting shielding gas $Q_{s,c}$, within the standoff column, i.e.,

$$Q_{s,c} = P'_{3,0} - P_{3,0} \quad (4-33)$$

In short, workpiece heating is mainly contributed by the plasma jet, comprising a mixture of plasma and shielding gases, with the power of $P_{3,0}$. Throughout the keyhole all plasma gas properties used in heat transfer calculations are based upon the mixture of plasma and shielding gas established at the inlet of the keyhole.

A detailed description of how to determine radius R_c will be discussed in Section VI of this report.

(IV-E) Total Workpiece Power Loss

Total power loss in the workpiece is comprised of the following items:

(IV-E-1) Convective Heat Loss in Workpiece

Local power loss to the workpiece from heat conduction can be computed from Equation (4-34), namely,

$$Q_{w,c_z} = Nu_z \cdot A_v \cdot \frac{k}{D} \frac{(h_{\text{plasma}} - h_w)}{c_p} \quad (4-34)$$

where Nu_z is the Nusselt number along the axial direction; A_v stands for heat transfer area per unit length along the axial direction of the workpiece ($A_v = \pi R$) i.e. the plasma contact area in the keyhole taken to resemble a finger ring comprising somewhat more than one half of the circumferential area of the keyhole; R is the radius of plasma contact area in the keyhole which varies with respect to axial distance z and is determined by the calculation; and D is the diameter of the keyhole equal to twice the effective radius of plasma contact area ($2R$). The rest of symbols are the same as used in the orifice.

The Nusselt number is computed as in Equation (4-3), used in orifice, which is

$$Nu_z = 0.2233(z^+)^{-0.7455} + 3.66 \quad (4-35)$$

where

$$z^+ = \frac{z}{R} \frac{1}{(Re \cdot Pr)_m}$$

Here R denotes effective radius of plasma contact area in the keyhole at the axial location of z . z is the distance between the entrance of keyhole to the half thickness of the section of interest in the workpiece considered. The rest of the symbols stand for the same

definition used in the orifice.

Total convective heat loss in the workpiece is

$$Q_{v,c} = \int_0^{L_4} Q_{v,c,z} dz = \int_0^{L_4} Nu_z A_v \cdot \frac{k}{D} \frac{(h_{\text{plasma}} - h_v)}{c_p} dz \quad (4-36)$$

(IV-E-2) Direct Power Loss from the Surface of Keyhole

Direct power loss to the keyhole surface includes $P_{w,1}$, the power generated by the workpiece work function; and part of $P_{v,2}$, the power generated at the workpiece anode and cathode drops, namely,

$$Q_{v,g} = P_{w,1} + \psi P_{v,2} \quad (4-37)$$

where

$Q_{v,g}$ = Direct power loss to the keyhole surface

ψ = Fraction of power generated by anode and cathode drops

that is transmitted to the keyhole surface

$(1-\psi)P_{v,2}$ = Power transmitted to the plasma from that generated at anode and cathode drops

(IV-E-3) Electron Collision Power Loss in Keyhole

Power carried by free electrons into the surface of the keyhole can be calculated from the following equation:

$$Q_{v,e} = \frac{I}{e} \left(\frac{3}{2} KT \right) \quad (4-38)$$

where $Q_{v,e}$ denotes power carried by free electrons in to the keyhole wall; T , the mean electron temperature entering the wall taken as the average temperature between plasma arc and wall of keyhole; and I , the straight polarity component of the transmitted current, which can be computed from the following equation:

$$I = \frac{I_m t_+}{t_+ + t_-} \quad (4-39)$$

Thus, total power loss to the workpiece, Q_v , is the summation of losses computed by Equations (4-36), (4-37), and (4-38), namely

$$Q_v = Q_{v,c} + Q_{v,g} + Q_{v,e} \quad (4-40)$$

(IV-F) Power Discharge Loss

The power carried away by the plasma jet discharge from the exit end of keyhole, Q_{dis} , can be computed from the plasma arc enthalpy and mass flow rate, i.e.,

$$Q_{dis} = (h_{p1} \dot{m}_{p1} + h_{sd} \dot{m}_{sd})_{dis} \quad (4-41)$$

where the values of $h_{p1} \dot{m}_{p1}$ and $h_{sd} \dot{m}_{sd}$ are the results of integration at the cross-section of the outlet end of the keyhole from $r = 0$ to $r = R_r$. R_r is the radius of the outlet end of the keyhole. A detailed description of how to determine R_r will be discussed in Section VI of this report.

Obviously, summation of power loss throughout the entire VPPA welding system is equivalent to the total power input of the system, P_{total} , namely

$$P_{total} = Q_E + Q_G + Q_N + Q_s + Q_N + Q_{dis} \quad (4-42)$$

Calculation of power loss at each part of VPPA welding system will be illustrated in Section VII of this report.

V. CALCULATION OF PLASMA ARC ENTHALPY

To give an example, the density of argon gas at a pressure of 1 atmosphere and a temperature of 298 °K is

$$\begin{aligned}\rho_{pl} &= \frac{PM_{Ar}}{RT} = \frac{101320 \text{ (N/m}^2\text{)} \cdot 39.95 \text{ (kg/kmol)}}{8315 \text{ (N}\cdot\text{m/kmol } ^\circ\text{K)} \cdot 298 \text{ (}^\circ\text{K)}} \\ &= 1.6336 \text{ (kg/m}^3\text{)}\end{aligned}$$

where

P = Atmospheric pressure

M_{Ar} = Molecular weight of argon

R = Universal gas constant

T = Absolute Temperature

The mass flow rate of argon gas in terms of volumetric flow rate can be computed as

$$\begin{aligned}\dot{m} &= (\dot{V} \text{ ft}^3/\text{hr}) \left(\frac{1}{3600} \text{ hr/s} \right) \left(\frac{1}{35.3147} \text{ m}^3/\text{ft}^3 \right) \rho_{Ar} \\ &= \frac{1.6336}{(3600)(35.3147)} (\dot{V} \text{ ft}^3/\text{hr}) \\ &= 1.285 \cdot 10^{-5} (\dot{V} \text{ ft}^3/\text{hr}) \quad (\text{kg/s}) \\ &= 1.285 \cdot 10^{-2} (\dot{V} \text{ ft}^3/\text{hr}) \quad (\text{g/s})\end{aligned}$$

(V-A) Plasma Arc Enthalpy Within the Gap Between Electrode and Orifice

Let us assume that entrance and exit ends of plasma arc enthalpy in the gap between electrode and orifice are $h_{1,1}$ and $h_{1,2}$ respectively.

The plasma arc power entering the gap, $P_{1,1}$, is the power

generated at the electrode, P_E , minus the power loss by electrode heat conduction, Q_E , namely

$$P_{1,i} = P_E - Q_E \quad (5-1)$$

Plasma arc enthalpy at the entrance end of the gap, thus, can be calculated as

$$h_{1,i} = \frac{P_{1,i}}{\dot{m}} \quad (5-2)$$

The plasma arc power at the exit end of the gap, $P_{1,o}$, has been augmented through Joule heating, $P_{J,i}$, and diminished through radiative heat loss, Q_G . It is

$$P_{1,o} = P_{1,i} + P_{J,i} - Q_G \quad (5-3)$$

Thus, plasma arc enthalpy at the exit end of the gap can be calculated from the expression

$$h_{1,o} = \frac{P_{1,o}}{\dot{m}} \quad (5-4)$$

(V-B) Plasma Arc Enthalpy Within Orifice

Let us assume that the enthalpy of the plasma at the entrance and exit ends of the orifice are $h_{2,i}$ and $h_{2,o}$, respectively.

The power, $P_{2,i}$, and enthalpy, $h_{2,i}$, of the plasma arc at the entrance end of the orifice are identical to the power, $P_{1,o}$ and enthalpy, $h_{1,o}$, respectively, of the plasma arc at the exit end of the gap between electrode and orifice. Thus,

$$\left. \begin{aligned} P_{2,i} &= P_{1,o} \\ h_{2,i} &= h_{1,o} \end{aligned} \right\} \quad (5-5)$$

The plasma arc power at the exit end of orifice, $P_{2,o}$, is increased by part of the power generated at the orifice anode drop, (1-

$\psi) P_{X,2}$, and by all the power generated by Joule heating within orifice, $P_{J,2}$, and is reduced by convective heat loss to the orifice, $Q_{X,c}$, and free electron power loss to the orifice, $Q_{X,e}$. Thus,

$$P_{2,0} = P_{2,1} + (1-\psi)P_{X,2} + P_{J,2} - Q_{X,c} - Q_{X,e} \quad (5-6)$$

The corresponding plasma arc enthalpy at the exit end of orifice is

$$h_{2,0} = \frac{P_{2,0}}{\dot{m}} \quad (5-7)$$

(V-C) Plasma Arc Enthalpy Within Standoff Column

Let us assume that the plasma enthalpies at the entrance and exit ends of the standoff column are $h_{3,1}$ and $h_{3,0}$, respectively.

The plasma arc power, $P_{3,1}$, and enthalpy, $h_{3,1}$, at the entrance end of standoff column are identical to the plasma arc power, $P_{2,0}$, and enthalpy, $h_{2,0}$, respectively, at the exit end of orifice. Thus,

$$\left. \begin{aligned} P_{3,1} &= P_{2,0} \\ h_{3,1} &= h_{2,0} \end{aligned} \right\} \quad (5-8)$$

Plasma arc power at the exit end of standoff column, $P_{3,0}$, is increased by Joule heating in standoff column, $P_{J,3}$, and induced shielding gas mixing power, $P_{s,d}$, and reduced by radiative heat loss, $Q_{s,r}$, and convective heat loss, $Q_{s,c}$, from the same column. Thus,

$$P_{3,0} = P_{3,1} + P_{J,3} + P_{s,d} - Q_{s,r} - Q_{s,c} \quad (5-9)$$

The corresponding plasma arc enthalpy at the exit end of standoff column is

$$h_{3,0} = \frac{\dot{m}_{p1}h_{p1} + \dot{m}_{sd}h_{sd}}{\dot{m}_{p1} + \dot{m}_{sd}} \quad (5-10)$$

where the values of \dot{m}_{p1} , \dot{m}_{sd} , $\dot{m}_{p1}h_{p1}$, and $\dot{m}_{sd}h_{sd}$ are the results of integration at the cross-section of outlet end of standoff column from

$r = 0$ to $r = R_c$ where R_c is the half crown width.

(V-D) Plasma Arc Enthalpy Within Keyhole of Workpiece

Let us assume that the plasma enthalpy at the entrance and exit ends of the keyhole of the workpiece are $h_{4,i}$ and $h_{4,o}$, respectively.

The plasma arc power, $P_{4,i}$, and enthalpy, $h_{4,i}$, at the entrance end of the keyhole of workpiece are identical to the plasma arc power, $P_{3,o}$, and enthalpy, $h_{3,o}$, respectively, at the exit end of standoff column. Thus,

$$\left. \begin{aligned} P_{4,i} &= P_{3,o} \\ h_{4,i} &= h_{3,o} \end{aligned} \right\} \quad (5-11)$$

Plasma arc power at the exit end of the keyhole of workpiece, $P_{4,o}$, is increased by a portion of the power generated at the workpiece anode and cathode drops, $(1-\psi)P_{v,2}$, and is reduced by convective heat loss to the keyhole surface, $Q_{v,c}$ and the loss of hot electrons to the keyhole, $Q_{v,e}$. Thus,

$$P_{4,o} = P_{4,i} + (1-\psi)P_{v,2} - Q_{v,c} - Q_{v,e} \quad (5-12)$$

The corresponding plasma arc enthalpy at the exit end of the keyhole of the workpiece is

$$h_{4,o} = \frac{\dot{m}_{p1}h_{p1} + \dot{m}_{sd}h_{sd}}{\dot{m}_{p1} + \dot{m}_{sd}} \quad (5-13)$$

where the values of \dot{m}_{p1} , \dot{m}_{sd} , $\dot{m}_{p1}h_{p1}$, and $\dot{m}_{sd}h_{sd}$ are the results of integration at the cross-section of outlet end of keyhole from $r = 0$ to $r = R_r$.

(V-E) Plasma Arc Enthalpy Discharged from the Workpiece

Plasma arc power, Q_{d1} , and enthalpy, h_{d1} , discharged from the keyhole of workpiece is identical to the plasma arc power, $P_{4,o}$, and enthalpy, $h_{4,o}$, at the exit end of keyhole, namely

$$\left. \begin{aligned} Q_{dis} &= P_{4,0} \\ h_{dis} &= h_{4,0} \end{aligned} \right\} \quad (5-14)$$

Calculation of plasma arc enthalpy at each part of VPPA welding system will be illustrated in Section VII of this report.

VI. CALCULATION OF CROWN AND ROOT BEAD WIDTHS

Bead width is calculated from the heat absorbed in the workpiece, Q_w . As shown in Equation (4-40) Q_w is the summation of convection heating (the empirical relation actually includes radiation.) from the plasma, "direct" heating of the surface by current passing through localized surface voltage drops, and heat carried into the surface by hot electrons from the plasma.

The heat input source in the keyhole during the actual welding process is neither a point source nor a line source along the axial direction in which the input energy is not uniformly distributed. To make a calculation closer to the actual situation, we adopted a calculated result at various locations of z along the axial direction as a heat source distribution. As the magnitude of the heat source per unit length along the z axis is closely related to the area of heat transfer (radius of keyhole at various locations of z), both heat absorbed by the keyhole per unit length along the axial direction and the radius of the keyhole at various locations of the z -axis shall be solved by simultaneous iteration.

The temperature field within the confined space between the two surfaces (assumed nonconducting) of the workpiece is constructed out of moving heat sources in an infinite continuum. "Image" sources are added outside the workpiece space so as to produce planes of symmetry across which no heat flows at the location of the workpiece surfaces. Given coordinate z zeroed at the top of the workpiece and extending down into the workpiece body and locating the heat source $Q_{w,z}$ at location z , then an image heat source above the top of the plate of

strength $Q_{w,z}$ located at $-z$ creates a plane of zero heat flow at $z = 0$, the location of the top surface of the workpiece. The latter plane will remain and a further plane of zero heat flow at the site of the bottom surface of the workpiece will be created if an infinite array of image heat source pairs is constructed along the z -axis, each heat source pair of strength $Q_{w,z}$ spaced at $\pm z$ about an infinite array of points spaced at $2L_4$ and including $z = 0$. See Figure 5 for illustration.

The temperature T_c at location (x_c, y_c, z_c) within the workpiece due to the welding power input to the workpiece is then:

$$T_c - T_0 = \sum_{i=-\infty}^{\infty} \frac{Q'_{w,z} dz}{4\pi K R_i} \exp \left(- \frac{u(R_i + x_c)}{2\alpha} \right) \quad (6-1)$$

where

T_0 = Ambient temperature of workpiece

K = Thermal conductivity of workpiece

u = Weld speed (in the x -direction)

α = Thermal diffusivity of workpiece

R_i = Distance between the i^{th} point heat source and the point of interest

R_i is computed as follows:

$$R_i = \sqrt{x_c^2 + y_c^2 + (z_i - z_c)^2} \quad (6-2)$$

$$z_i = \left[i + \frac{1 + (-1)^{i+1}}{2} \right] L_4 + (-1)^i z \quad (6-3)$$

Weld bead width is determined by locating the largest value of y_c for which $T_c = T_m$, the melting temperature of the workpiece, at $z = 0$

(crown) and $z_c = L_k$ (root). The weld widths are twice the values of these y_c 's. A converging computer search routine is used to make the computation.

One approximation is used in the computations. The summation is truncated. 35 source points are used, 17 image sources on each side of the weld heat source. The values of z_i are generated by a recurrence relation:

$$z_i = z_{i-2} + 2L_k \quad (6-3)$$

where the starting values are:

$$z_0 = z \quad (6-4)$$

$$z_1 = 2L_k - z \quad (6-5)$$

where $0 \leq z \leq L_k$

z_0 ($=z$) is the weld heat source position located in the workpiece.

After truncation, Equation (6-1) becomes

$$T_c - T_o = \sum_{i=-17}^{17} \frac{Q'_{w,z} dz}{4\pi k R_i} \exp \left[-u \left(\frac{R_i + x_c}{2\alpha} \right) \right] \quad (6-6)$$

As we indicated earlier for the computation of heat source distribution along the z -axis, the temperature distribution within the workpiece can be obtained by integrating Equation (6-6) which is

$$\begin{aligned} T_c - T_o &= \int_0^{L_k} \sum_{i=-17}^{17} \frac{Q'_{w,z} dz}{4\pi k R_i} \exp \left[-u \frac{(R_i + x_c)}{2\alpha} \right] \\ &= \sum_{i=-17}^{17} \int_0^{L_k} \frac{Q'_{w,z} dz}{4\pi k R_i} \exp \left[-u \frac{(R_i + x_c)}{2\alpha} \right] \end{aligned} \quad (6-7)$$

Adopting temperature T_c to be the melting temperature T_m , one can

compute the melting isotherm surface from Equation (6-7). The geometric distribution of the keyhole can also be obtained for the maximum radius of the melting widths at various locations of z . Crown and root widths, $2R_c$ and $2R_r$, at the upper and lower ends of the workpiece can be calculated by a similar method.

Equation (6-7) is used to compute the temperature distribution within the workpiece in which $Q'_{w,z}$, denotes the power conducted away through the workpiece, or the strength of heat source per unit length at location z . This strength of the heat source in the workpiece is the heat absorption $Q_{w,z}$ contributed from the plasma jet, minus a power loss due to the radiative heat transfer from the surfaces of the workpiece Q_r . In the actual numerical integration of Equation (6-7), Q_r is included in $Q'_{w,z}$ at various locations of z by a method of weighing.

Since the distributions of $Q_{w,g}$ from Equation (4-37) and $Q_{w,e}$ from Equation (4-38) inside the keyhole are hard to determine, we assume the parabolic type of square approximation (see Figure 6 for schematic expression of the workpiece power distribution),

$$Q_z = a(1 - \frac{z}{L_k})^2 Q \quad (6-8)$$

where Q denotes either $Q_{w,g}$ or $Q_{w,e}$. a is a constant which will be determined from the integration of Equation (6-8) based on the value of Q in which the total value of either $Q_{w,g}$ or $Q_{w,e}$ shall be conserved. This is

$$Q = \int_0^{L_4} Q_z dz = \int_0^{L_4} a \left(1 - \frac{z}{L_4}\right)^2 Q dz$$

which leads to $a = 3/L_4$, and Equation (6-8) becomes

$$Q_z = \frac{3}{L_4} \left(1 - \frac{z}{L_4}\right)^2 Q \quad (6-9)$$

Radiation losses from both sides of the workpiece surfaces are computed. The radiative heat transfer loss can be computed as

$$Q_R = \sum A_i \epsilon_i \sigma T_i^4 \quad (6-10)$$

where A_i denotes a small element i of surface area; ϵ_i is emissivity of the workpiece; T_i stands for the average temperature ($^{\circ}\text{K}$) of the surface area element A_i ; and σ is Stefan-Boltzman constant ($= 5.67 \times 10^{-8} \text{ W/m}^2 \cdot \text{K}^4$).

Workpiece power absorption per unit length along the z -axis due to melting heat can be computed from the following relation:

$$Q_{m,z} = u \rho_w Q_f d_z \quad (6-11)$$

where

u = Traveling speed of welding

ρ_w = Density of workpiece

Q_f = Melting heat of workpiece

d_z = Bead width at position z

Based on this analysis, power transfer per unit length in workpiece $Q'_{w,z}$ can be computed as follows:

$$Q'_{w,z} = Q_{w,c_s} + \frac{3}{L_4} \left(1 - \frac{z}{L_4}\right)^2 (Q_{w,g} + Q_{w,s}) - Q_{m,z} - Q_R \left(\frac{Q_{w,z}}{Q_w}\right) \quad (6-12)$$

The total net power absorbed by workpiece is then

$$Q'_w = \int_0^{L_1} Q'_{w,z} dz \quad (6-13)$$

Substituting Equations (6-12) in (6-13), we have

$$Q'_w = Q_w - Q_R - Q_m \quad (6-14)$$

where

$$\begin{aligned} Q_w &= \int_0^{L_1} Q_{w,c,z} dz + Q_{w,g} + Q_{w,e} \\ &= Q_{w,c} + Q_{w,g} + Q_{w,e} \end{aligned}$$

is similar to Equation (4-40), and Q_R is from Equation (6-10).

Here,

$$Q_m = \int_0^{L_1} Q_{m,z} dz$$

is the total melting power.

VII. CALCULATION OF PARTIAL PENETRATION OF THE WORKPIECE

In Section VI, we have discussed the weld widths and power loss in the workpiece. An estimation of full penetration or partial penetration shall be made before we can proceed the calculation of Section VI. Before the keyhole is formed for partial penetration, the plasma jet impinges perpendicularly on the surface of the weld pool, and is deflected across the weld surface radially away from the stagnation area. Thus, the heat transfer from the plasma jet to the surface of the weld pool and the model of the heat source used to calculate the temperature field of the workpiece are different from those of the weld process in which keyhole has been formed in the workpiece.

(VII-A) Weld Pool Convective Heat Transfer

For the case of partial penetration, a concave shape melting puddle is formed while the plasma jet impinges on the surface of the workpiece. At this moment, there is a very complicated flow pattern developed within the melting puddle of the molten liquid metal. It is anticipated that heat transfer process, which causes the convective heat flow from the plasma jet to the workpiece, is also very complicated. It is hard to adopt a very suitable mathematical formulation to describe convective heat loss from the plasma jet to the workpiece. In this study in the determination of partial and full penetration of the workpiece, an axial symmetry circular plasma jet, which impinges perpendicularly on the surface of the weld pool of the workpiece, is assumed to compute the convective heat loss problem.

The power transferred to the workpiece by convection from the plasma arc jet can be written as:

$$Q_{w,c} = h \cdot A_w \cdot (H_{\text{plasma}} - H_w) / c_{pm} \quad (7-1)$$

where

A_w = Plasma arc jet impingement surface area
 $= \pi R_2^2$

R_2 = Outer boundary radius produced by plasma arc jet on the surface of the workpiece (see Figure 4b)

H_{plasma} = Average enthalpy of the plasma arc jet on the stagnation area A_w

H_w = Enthalpy of the plasma arc jet at the temperature of the weld pool

c_{pm} = Specific heat of the plasma corresponding to a temperature T_m at which the enthalpy of plasma is equal to the mean enthalpy at the temperature of the arc jet and the weld pool

h = Convective heat transfer coefficient

h can be computed from the following relation (Metcalf and Quigley, 1975):

$$N_u = 0.78 R_o^{0.5} P_r^{0.33} \quad (7-2)$$

where the dimensionless parameters are defined as follows:

$$N_u = \frac{h(2R_2)}{k}$$

$$R_o = \frac{\rho v(2R_2)}{\mu}$$

$$P_r = \frac{C_p \mu}{k}$$

Here, v is the average velocity of the plasma arc jet within the outer boundary on the surface of the workpiece. The rest of the parameters are the same as that defined earlier. In this calculation, the parameters of the plasma are determined based on the average enthalpy within the cross sectional area of radius R_2 .

Total power absorbed by the weld pool or the workpiece, Q_w , shall be the summation of Equations (7-1), (4-37) and (4-38), i.e.,

$$Q_w = Q_{w,c} + Q_{w,g} + Q_{w,e} \quad (7-3)$$

(VII-B) The Model of Temperature Field and Partial Penetration

In the determination of the formation of keyhole from the plasma arc jet impingement on the surface of the workpiece, it is assumed that there is a point source with an intensity of Q_w which moves with a speed of u acting on the surface of the workpiece. Point source model, proposed by Rosenthal, is adopted to compute the temperature field of the workpiece created by this moving point source. The depth of the weld pool, z_m , created by the moving point source can be computed by the constant temperature surface of the workpiece molten temperature which is the solid-molten pool interface of the workpiece weld pool. The impingement of the high speed plasma jet creates an intensive disturbance on the molten liquid of the workpiece and forms a concave hole on the surface of the workpiece. It may create a distributed heat source from the surface of the workpiece to the depth of the weld pool if the impingement of the plasma jet can reach the bottom of the molten

pool. To simplify the calculation, we may assume that there is a uniformly distributed heat source moving with a speed of u , and with an intensity of Q_w/Z_m (See Figure 7). The temperature field of the workpiece can be computed based on the effect of the moving uniformly distributed heat source. Determination of the depth of the partial penetration and the formation of the keyhole can be resulted from the distribution of the constant temperature surface of the workpiece molten temperature.

The temperature field produced by the point source at the surface of the workpiece moving with uniform velocity of u (at the same time a moving coordinate with a speed u moved with a point source). Location of the point source is at the origin) is

$$T_c - T_o = \sum_{i=1}^{\infty} \frac{Q'_w}{4\pi k R_i} \exp\left[-\frac{u}{2\alpha} (R_i + x_c)\right] \quad (7-4)$$

where

k = Heat conductivity of the workpiece

α = Thermal diffusivity of the workpiece

u = Moving speed of the point source

$$R_i = [x_c^2 + y_c^2 + (z_c - z_i)^2]^{1/2}$$

x, y, z = Location of the point of interests

$$z_i = \left[i + \frac{1 + (-1)^{i+1}}{2}\right] \cdot L_k$$

L_k = Thickness of the workpiece

Here,

$$Q'_w = Q_w - Q_m$$

Q_w can be computed from Equation (7-3), and

Q_m = Latent power of the workpiece

$$= \int_0^{z_m} Q_f \rho d_z dz$$

where

Q_f = Latent heat of the workpiece

ρ = Density of the workpiece

d_z = Width of the molten liquid of the workpiece at the corresponding location of z

Put $T_c = T_m$ (molten temperature of the workpiece) in Equation (7-4), one can solve the constant molten temperature surface of the workpiece. The depth of the workpiece molten pool under the effect of the heat source, thus, can be determined.

The temperature field created by the moving uniformly distributed heat source with intensity of Q_w'/Z_m located from $z = 0$ to Z_m is

$$T_c - T_o = \sum_{i=-\infty}^{\infty} \int_0^{z_m} \frac{(Q_w'/Z_m)}{4\pi k R_i} \exp\left[-\frac{u}{2\alpha}(R_i + x_c)\right] dz \quad (7-5)$$

where

$$R_i = [x_c^2 + y_c^2 + (z_i - z_c)^2]^{1/2}$$

$$z_i = \left[i + \frac{1 + (-1)^{i+1}}{2}\right] \cdot L_s + (-1)^i z$$

$$0 \leq z \leq Z_m$$

$$Q_w' = Q_w - Q_m$$

$$Q_m = \int_0^{z_1} Q_r u p d_z dz$$

z_1 = Molten metal depth of the workpiece under the effect of uniformly distributed heat source

The determination of full penetration or the formation of the keyhole is dependent upon whether z_1 is equal to the workpiece thickness L_k . In the realistic calculation, adoption of 35 terms of series summation in Equation (7-5) is good enough to assure the series convergence accuracy of the temperature field determination. In other words, the adoption of $-17 \leq i \leq 17$ together with solving simultaneous equations of Equation (7-5) and the computation of Q_m with iteration of related variables are required to solve the temperature field distribution.

It is due to the fact that there is no experimental data available for the variation of the depth of partial penetration with respect to control parameters of the welding processes. There is no way to compare the model results with the all of the stages of penetration processes during the plasma arc jet welding. In this study, model comparison with the experimental results of partial penetration and the possibility of the formation of the keyhole are made.

Equation (7-5) is used to calculate the probability of full penetration as the lower surface of the workpiece reaches the molten temperature. For the case of partial penetration, it may be due to the fact that the power supply is too small and/or the weld speed is too high. So long as the keyhole is formed, Section VI

will be used to compute the power absorbed by the workpiece in the keyhole, the weld widths, etc.

VIII. CALCULATION OF CROWN AND ROOT HEIGHTS

(VIII-A) Volume Conservation Equation of Materials

Assuming that reinforcement profiles of crown and root beads are paraboloid, as shown in Figure 8. These paraboloid profile can be expressed in the following equation:

$$Z = h_c \left[1 - \left(\frac{2y}{d_c} \right)^n \right] \quad (8-1)$$

where

h_c = Crown height

d_c = Crown bead width

n = Numerical value greater than 1

The cross-sectional area of the crown reinforcement is

$$\begin{aligned} A_c &= 2 \int_0^{d_c/2} \left\{ h_c \left[1 - \left(\frac{2y}{d_c} \right)^n \right] \right\} dy \\ &= \frac{n}{n+1} h_c d_c \end{aligned}$$

Similarly, cross-sectional area of the root reinforcement is

$$A_r = \frac{n}{n+1} h_r d_r$$

where

h_r = Root height

d_r = Root bead width

Volume conservation requires the equation of the material volume provided by welding wire to the reinforcement volume crown and root beads plus any gaps or holes in the weld site prior to welding:

$$\frac{n}{n+1} d_c h_c + \frac{n}{n+1} d_r h_r = \frac{\pi}{4} d_v^2 \frac{V_v}{u} - L_4 \cdot W_g \quad (8-2)$$

where

d_v = Diameter of wire

V_v = Feeding speed of wire

u = Welding speed

W_g = Initial gap at the weld seam

L_4 = Thickness of workpiece

(VIII-B) Force Equilibrium Equation

It should be noted that for the sake of tractability the force-equilibrium analysis has been greatly simplified. Longitudinal curvature of the weld puddle surface has been neglected as have the effects of Marangoni circulations and thermal variation of surface tension. There is a great deal of room for improvement of this first, very rough analysis. The cross-sectional areas a , b , and c , defined in Figure 9 which are given by

$$\begin{aligned} A_a &= 2 \int_0^{d_r/2} \left\{ h_c \left[1 - \left(\frac{2y}{d_c} \right)^n \right] \right\} dy \\ &= h_c d_r - \frac{1}{n+1} h_c d_c \left(\frac{d_r}{d_c} \right)^{n+1} \end{aligned} \quad (8-3)$$

$$A_b = d_r \cdot L_4 \quad (8-4)$$

$$A_c = A_r = \frac{n}{n+1} h_r d_r \quad (8-5)$$

The slopes of the reinforcement surfaces at points B (crown) and D (root), shown in Figure 9, are given by

$$\tan \theta_c = \left. \frac{dz}{dy} \right|_{y=d_r/2} = - \frac{2nh_c}{d_c} \left(\frac{d_r}{d_c} \right)^{n-1}$$

and

$$\tan \theta_r = \left. \frac{dz}{dy} \right|_{y=d_r/2} = \frac{2nh_r}{d_r}$$

It is due to the fact that both θ_c and θ_r are relatively small, and we can assume $\sin \theta_c \approx \tan \theta_c$ and $\sin \theta_r \approx \tan \theta_r$.

With reference to the free-body diagram shown in Figure 9, the force equilibrium equation for the body comprising areas a, b, and c is given by

$$\left[h_c d_r - \frac{1}{n+1} h_c d_c \left(\frac{d_r}{d_c} \right)^{n+1} + d_r \cdot L_4 + \frac{n}{n+1} d_r h_r \right] \rho g \\ = 4n \left[\frac{h_r}{d_r} - \frac{h_c}{d_c} \left(\frac{d_r}{d_c} \right)^{n-1} \right] \sigma - \bar{p} d_r \quad (8-6)$$

where the first term represents a gravitational force, g being the gravitational acceleration component perpendicular to the workpiece surface and directed from crown to root. The second term represents a surface tension force, σ being the molten weld puddle surface tension. The third term represents a pressure force, \bar{p} being the mean pressure acting on the weld crown surface.

(VIII-C) Calculation of Crown and Root Heights in Horizontal Welding (with Consideration of Gravity Force)

Experience suggests that the effect of external pressure \bar{p} is

much smaller than that of the surface tension. Therefore, the \bar{p} term will be deleted from the force equilibrium equation (8-6). Crown and root heights, thus, can be found by simultaneously solving Equations (8-2) and (8-6) which yield the following expressions:

$$h_c = \frac{- \left[1 - \frac{4}{d_r^2} (n+1) \frac{\sigma}{\rho g} \right] \left[\frac{\pi}{4} d_v^2 \frac{V_v}{u} - L_4 \cdot W_g \right] - d_r \cdot L_4}{d_r - \frac{n}{n+1} d_c + \frac{4n\sigma}{\rho g} \left[\frac{1}{d_c} \left(\frac{d_r}{d_c} \right) + \frac{d_c}{d_r^2} \right] - \frac{1}{n+1} d_c \left(\frac{d_r}{d_c} \right)^{n+1}} \quad (8-7)$$

$$h_r = \frac{\frac{\pi}{4} d_v^2 \frac{V_v}{u} - L_4 \cdot W_g - \frac{n}{n+1} d_c h_c}{\frac{n}{n+1} d_r} \quad (8-8)$$

(VIII-D) Calculation of Crown and Root Heights in Vertical Welding (Without Gravity Effect)

The gravity force component g perpendicular to the workpiece vanishes for the case of vertical welding and also for welding carried out in space. Ignoring both gravity force and external pressure in Equation (8-6) one obtains

$$h_r = h_c \left(\frac{d_r}{d_c} \right)^n \quad (8-9)$$

and substituting this equation to Equation (8-2),

$$h_c = \frac{\frac{\pi}{4} d_v^2 \frac{V_v}{u} - L_4 \cdot W_g}{\frac{n}{n+1} \left[d_c + d_r \left(\frac{d_r}{d_c} \right)^n \right]} \quad (8-10)$$

(VIII-E) Depression of Crown Height During Solidification

Figure 10 shows the configuration of the cross-section of puddle during the process of solidification. The solid-liquid interface lies along the melting temperature isotherm, which generally expand toward the hotter crown and contract toward the colder root. They come together, thus, first at the root as in Figure 10(B). This leaves a sector of molten metal which shrinks upon solidification. The height of the solidified crown must fall to accomodate the shrinkage volume reduction as shown in Figure 10(C). The cross-sectional area of the molten sector in Figure 10(B) can be approximated as

$$A_c = \frac{1}{2} L_4 \cdot d_c' \quad (8-11)$$

where L_4 stands for the thickness of the workpiece; and d_c' , the crown width in a state of molten metal. Given a volumetric shrinkage, $\Delta v/v$, a material property, the reduction in area ΔA_c of the molten material during solidification is

$$\Delta A_c = A_c \left(\frac{\Delta v}{v} \right) = \frac{1}{2} L_4 \cdot d_c' \left(\frac{\Delta v}{v} \right) \quad (8-12)$$

From Equation (8-5) for the cross-sectional area of the crown reinforcement, the reduction in the area can be related to the change in the crown reinforcement height $\Delta h_c'$

$$\Delta A_c = \Delta \left(\frac{n}{n+1} d_c' h_c' \right) = \frac{n}{n+1} d_c' \Delta h_c' \quad (8-13)$$

Equating Equations (8-12) and (8-13), leads to

$$\frac{1}{2} L_4 \cdot d_c' \left(\frac{\Delta v}{v} \right) = \frac{n}{n+1} d_c' \Delta h_c'$$

which gives upon simplification

$$\Delta h_c' = \frac{n + 1}{2n} L_4 \left(\frac{\Delta v}{v} \right) \quad (8-14)$$

Using King's (1987), value for specific volumetric shrinkage for aluminum during the solidification, $\Delta v/v$, is 6.7%. Therefore, crown height shrinkage for solidification of aluminum Equation (8-14) becomes

$$\Delta h_c' = 0.067 \frac{n + 1}{2n} L_4 \quad (8-15)$$

Detailed calculation results of crown and root heights are illustrated in Section IX of this report.

IX. LEADING EDGE ANGLE COMPUTATION

The leading edge angle of the keyhole of workpiece can be computed from thermal power equilibrium requirements as follows:

$$\tan\theta = \frac{\rho v [\mathcal{L} + c_s (T_m - T_o) + c_l (T_s - T_m)]}{P_w / \pi D L_k} \quad (9-1)$$

where

ρ = Density of workpiece (kg/m^3)

v = weld speed (m/s)

\mathcal{L} = Melting latent heat of workpiece (kJ/kg)

c_s = Specific heat of solid workpiece ($\text{Kj}/\text{kg}\cdot\text{K}$)

c_l = Specific heat of liquid workpiece ($\text{Kj}/\text{kg}\cdot\text{K}$)

T_m = Melting temperature of workpiece (K)

T_o = Original temperature (room temperature) of workpiece (K)

T_s = Temperature of superheated molten fluid at leading edge (K)

P_w = Thermal power absorbed by workpiece (Kw)

D = Keyhole diameter (m) or orifice diameter (m)

L_k = Thickness of workpiece (m)

θ = Leading edge angle

Theoretical computations and experimental measurements from rubber molds of keyholes (Nichols Research, 1992) are found to be in good agreement, at least with respect to velocity dependence except for four measurements at low plasma flow rates, which show experimental leading edge angles of $\theta > \text{or} = 30^\circ$. In other words, Equation (9-1) may hold only above some threshold value of plasma flow rate. Above the threshold value, for reasons not yet understood a "beam absorption" model may allow computation of the

leading edge angle of the VPPA keyhole; while another concept appears to be required to deal with this problem when the plasma flow rate is below the threshold value.

X. RESULTS OF COMPUTATION AND COMPARISON WITH MEASUREMENTS MADE BY THE GDI TEAM

A computer implementation of the proposed mathematical model for VPPA modeling computation is included in the Appendix A; and for VPPA partial penetration to the formation of the keyhole is included in the Appendix B. Input data for the computer program is provided for in Appendix C for aluminum; and Appendix D for mild steel. Nomenclature are listed in Appendix E.

For the purpose to explain VPPA modeling computation, and VPPA partial penetration computation listed in Appendices A and B, two block diagrams and corresponding explanations are included in Appendices F and G to explain the structures of VPPA partial penetration and VPPA modeling computation, respectively.

Model computations have been made and compared with the experimental measurements accomplished by Nichols Research Corporation (1992). These comparisons are included in Appendix H of this report.

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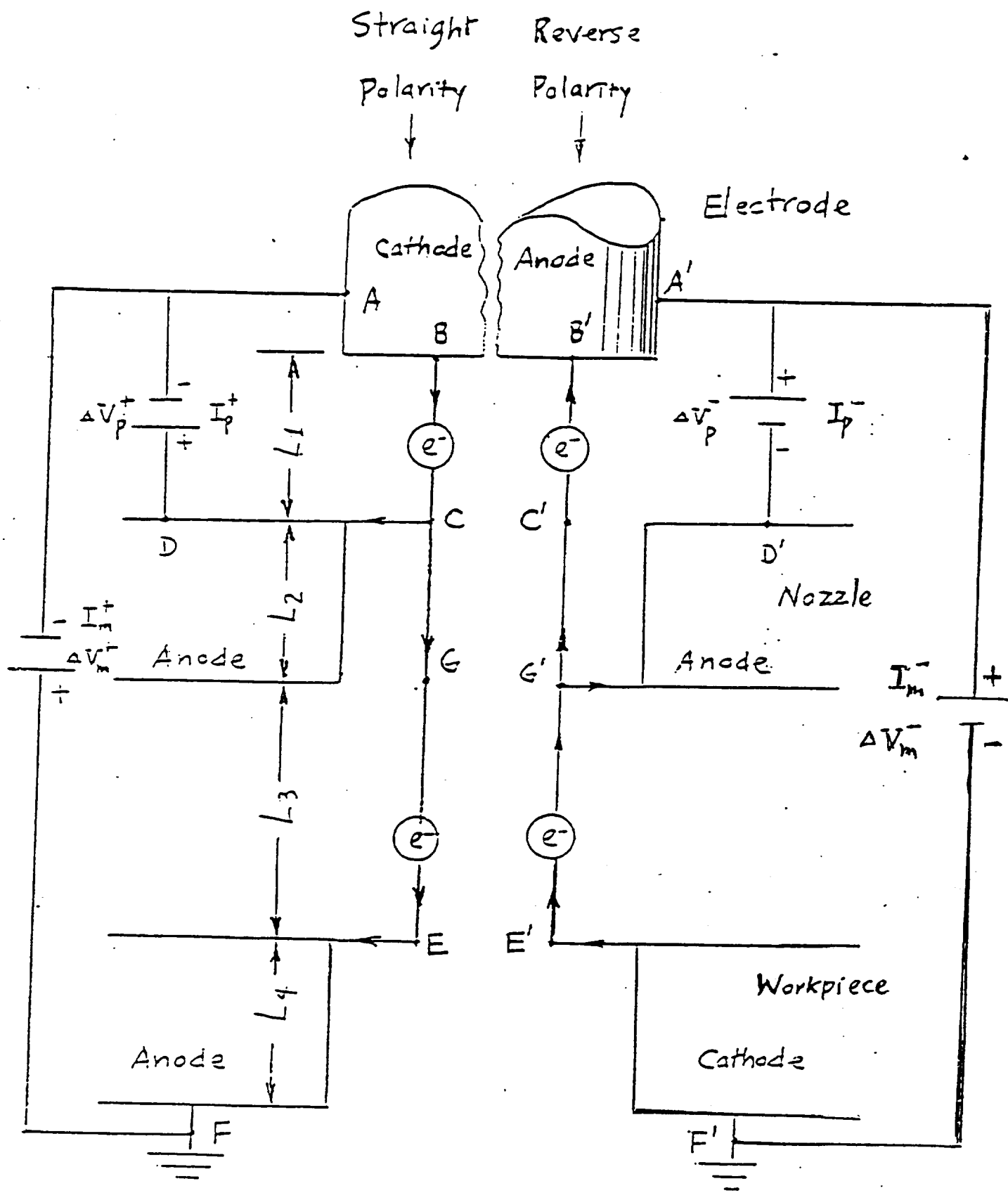


Fig. 1

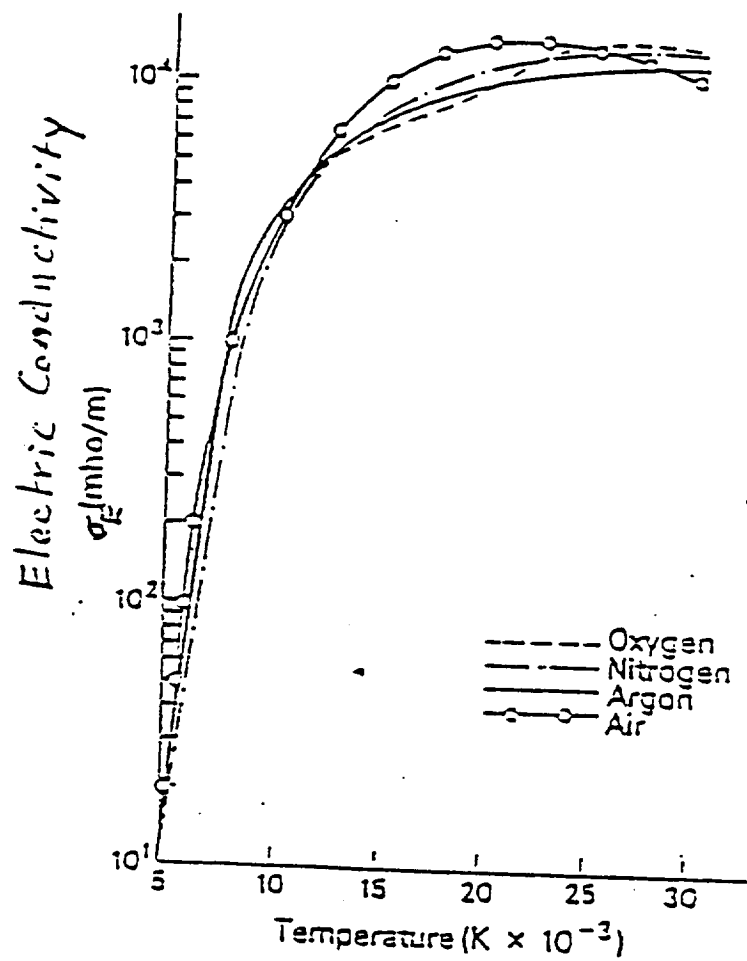


Fig. 2

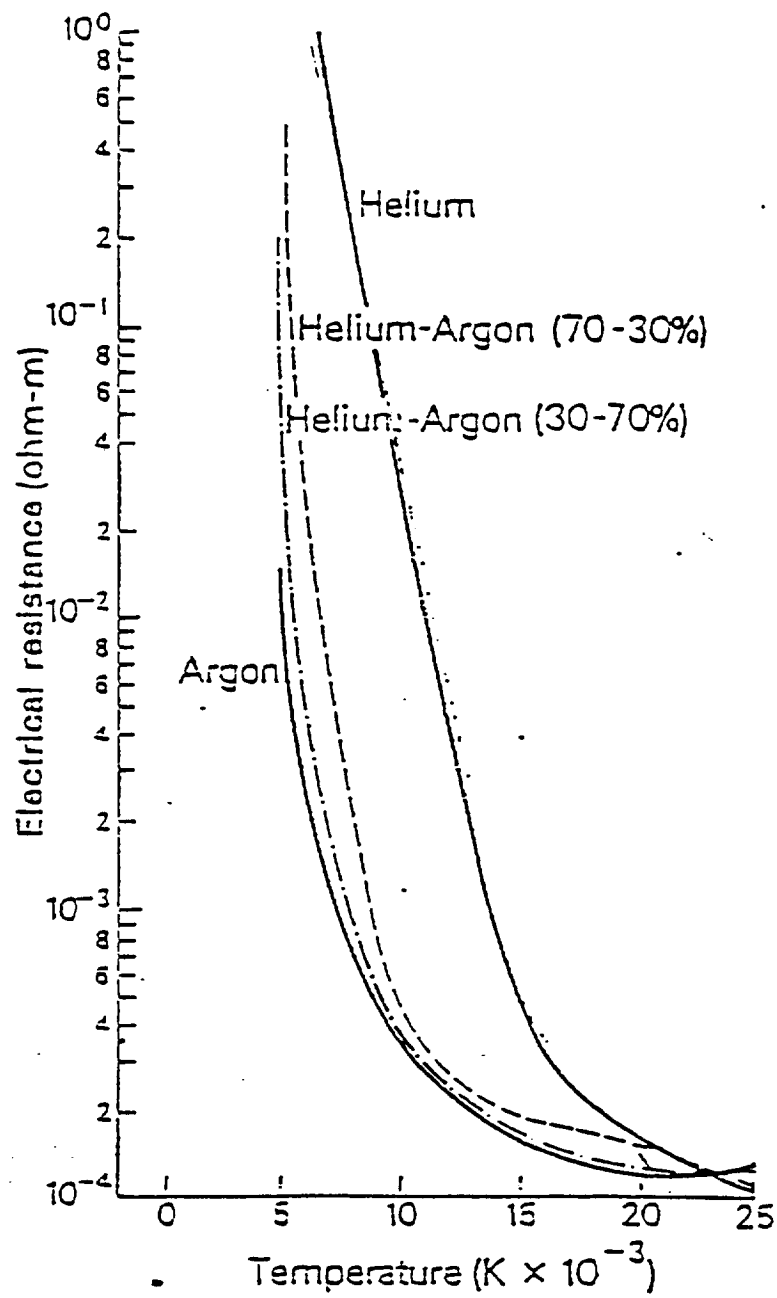


Fig. 3

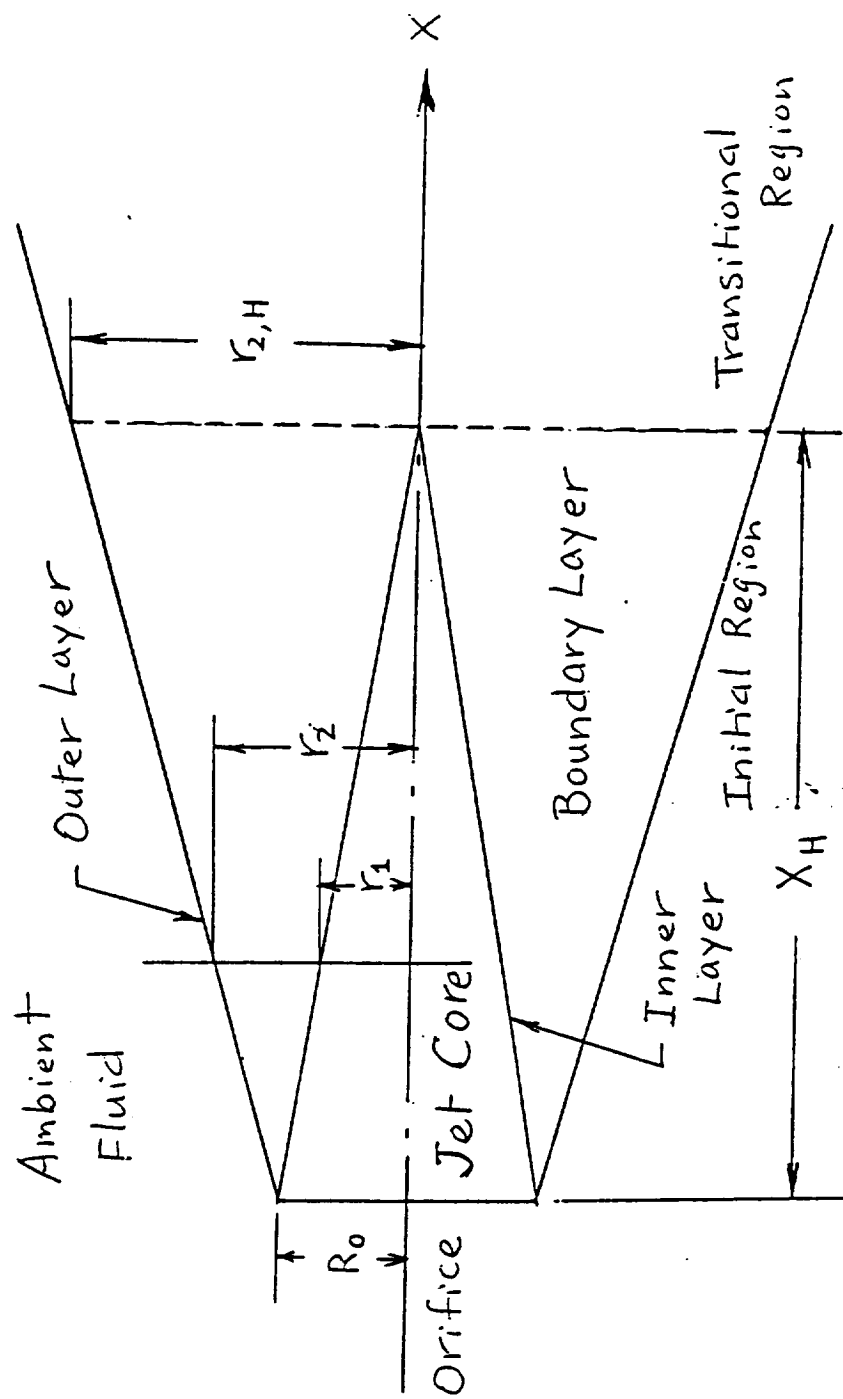


Fig. 4a

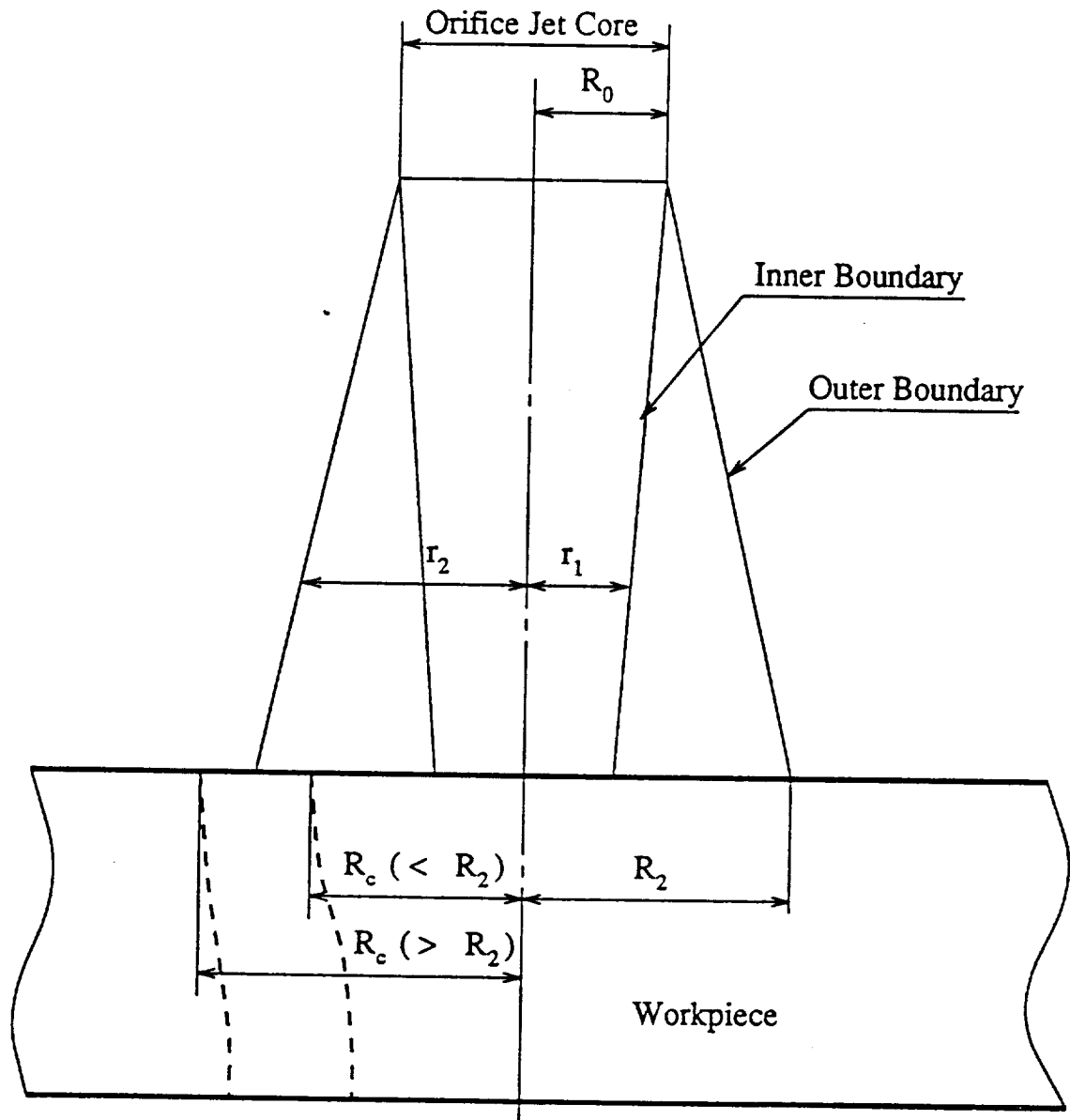


Fig. 4b Acting Range of Plasma Jet on Workpiece Surface

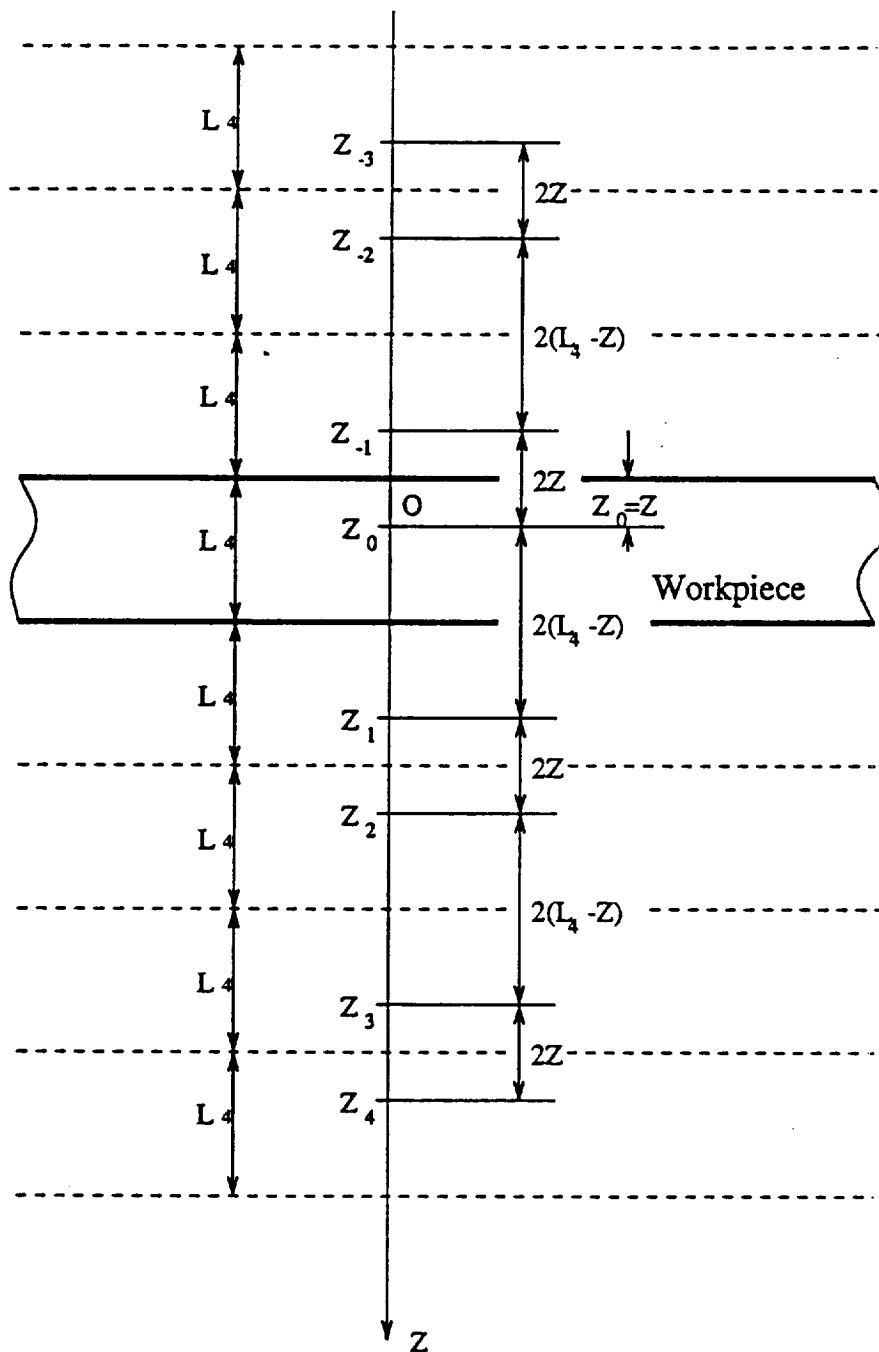


Fig. 5

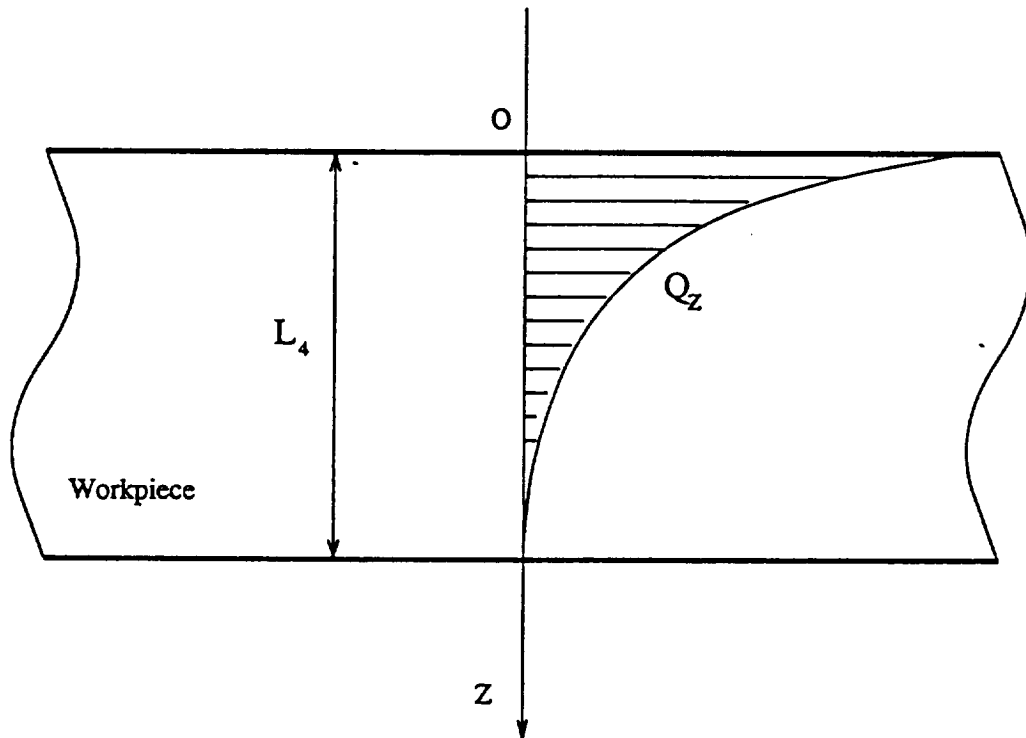


Fig. 6 Workpiece Heat Power Distribution

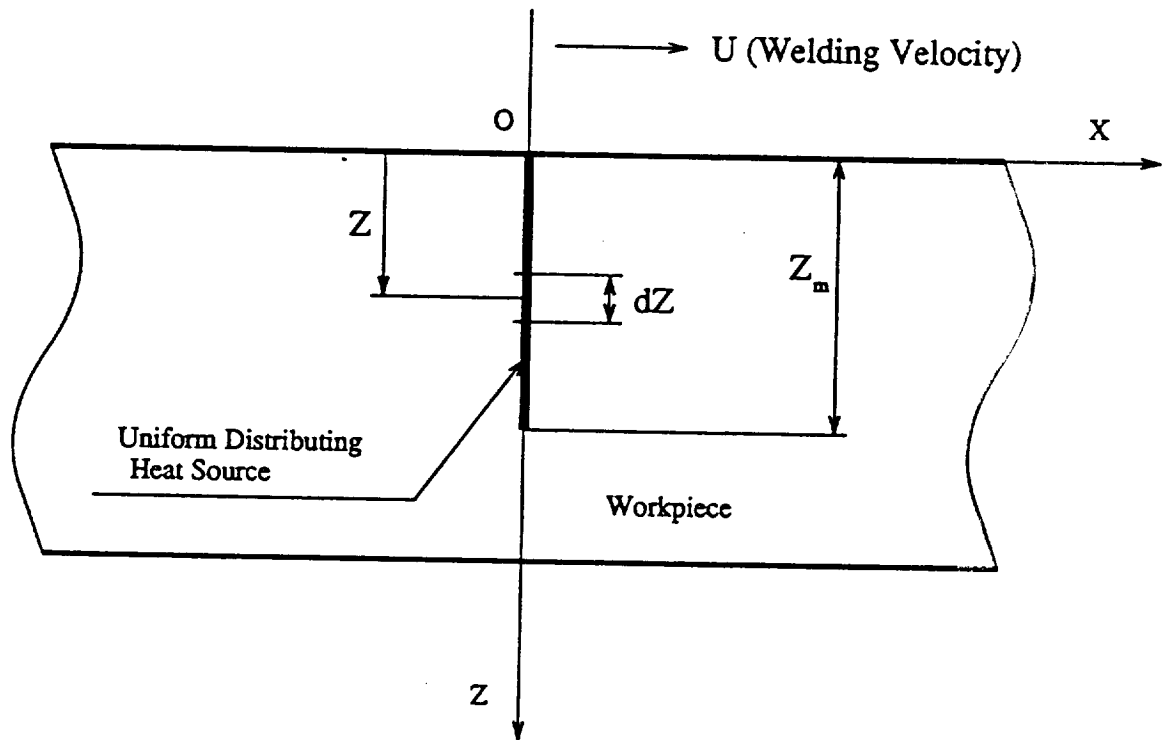


Fig. 7 Uniformly Distributed Heat Source

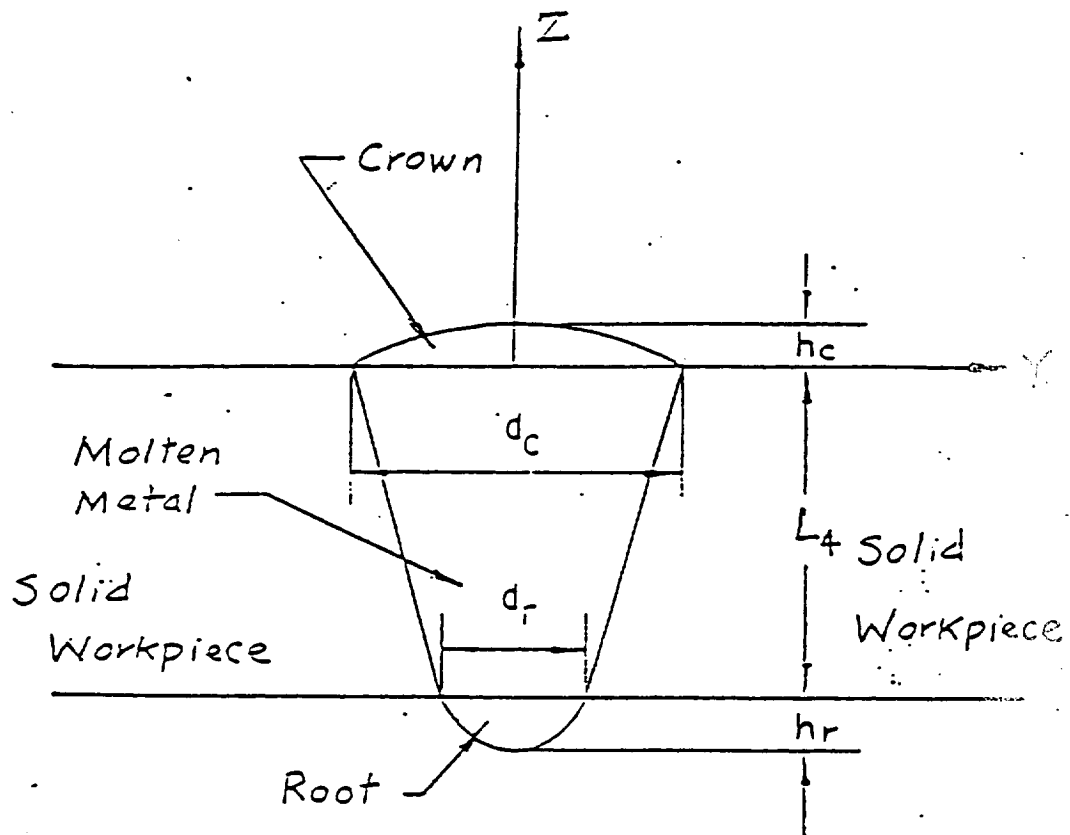


Fig. 8

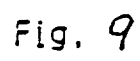


Fig. 9

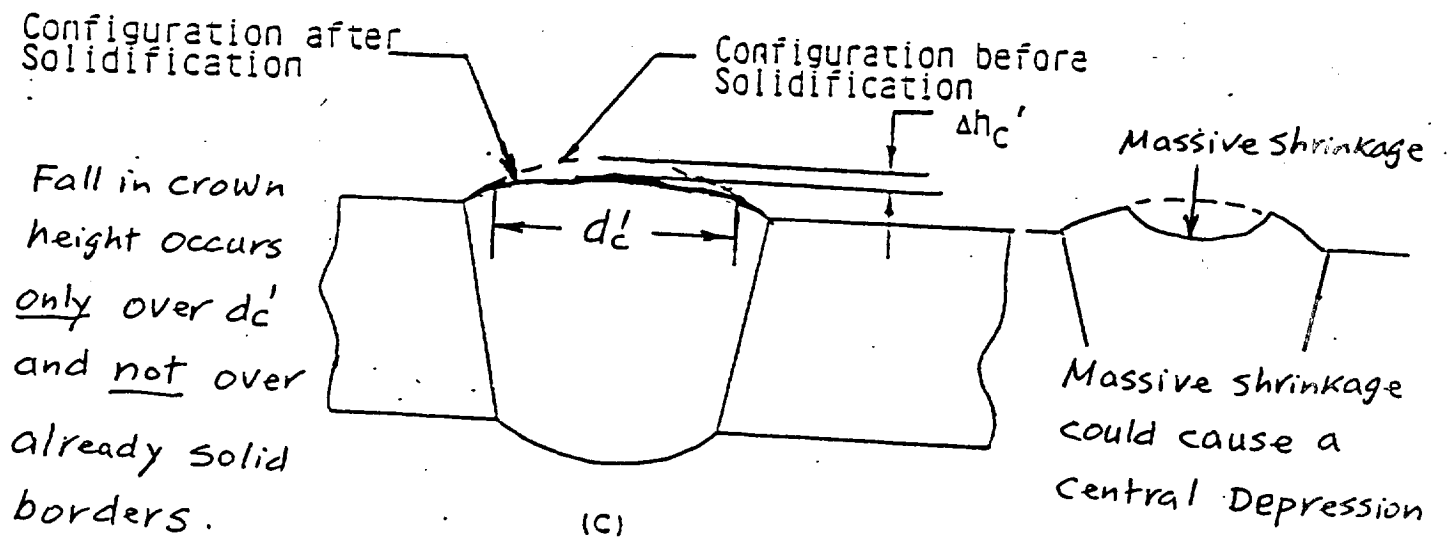
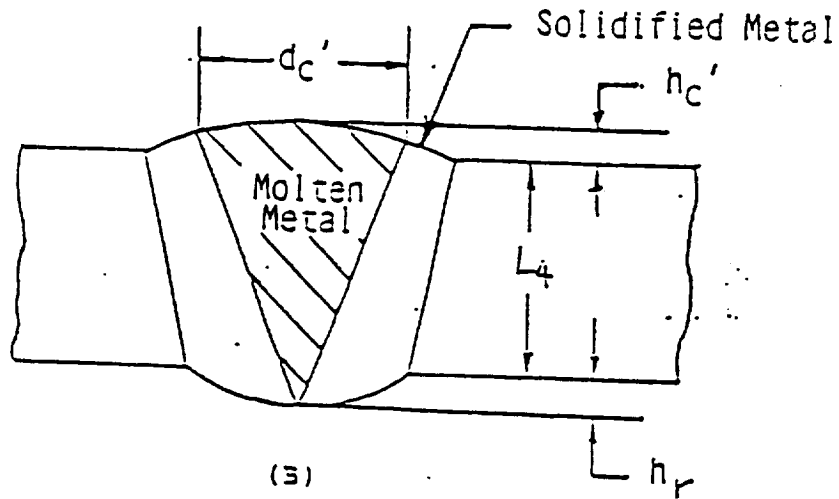
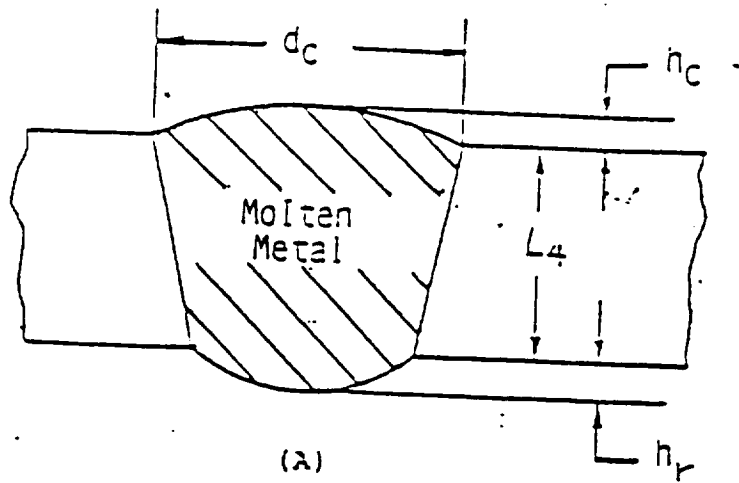


Figure 10 (A, B, C)

Appendix A

***** COMPUTER PROGRAM FOR VFPA MODELING *****

```
C-----
C      PROGRAM WELDBOTH.FOR, COMPILED ON FEB. 26, 1993
C
C      Line source , keyhole diameter is variable along the axis
C      of keyhole
C
      DIMENSION POW1(11), POW2(11), POW3(11), POW4(11)
      DIMENSION ENT1(11), ENT2(11), ENT3(11), ENT4(11), TABMPL(26)
      DIMENSION QLOS1(10), QLOS2(10), QLOS3(10), QLOS4(10), TABMSD(26)
      DIMENSION TEMP1(11), TEMP2(11), TEMP3(11), TEMP4(11), Bhole(10)
      DIMENSION ELOS2(10), ELOS4(10), QSEGM(10), XSOUR(10), Bhole0(10)
      DIMENSION AREA(10), DUDL1(10), DUDL2(10), DUDL3(10), QSOUR(10)
      DIMENSION R1(11), R2(11), FLWPL(11), FLWSD(11), ENERG(11)
      COMMON/DAT10/NX, NY, NZ, X(25), Y(20), TM, TO, THK, EPSL, DENS, HFUSI
      COMMON MMM
      COMMON TABTEM(26), TABIFL(26), TABCPL(26), TABKPL(26), TABISD(26)
      COMMON ITMAX, DHMAX, DTMAX
      COMMON TAMBI, DNOZL, FMPL
      COMMON TABCSD(26), TABKSD(26)
      COMMON TW4, MREG4, NREG4
      COMMON FLM, SDM
      OPEN(5, FILE='C:WELDTAB.USE')
      OPEN(6, FILE='C:WELDIN.USE')
      OPEN(7, FILE='C:WELDOU.USE')
      READ(5, *) MMM
      READ(5, *) (TABTEM(I), I=1, MMM)
      READ(5, *) (TABIFL(I), I=1, MMM)
      READ(5, *) (TABCPL(I), I=1, MMM)
      READ(5, *) (TABKPL(I), I=1, MMM)
      READ(5, *) (TABISD(I), I=1, MMM)
      READ(5, *) (TABCSD(I), I=1, MMM)
      READ(5, *) (TABKSD(I), I=1, MMM)
      READ(5, *) (TABMPL(I), I=1, MMM)
      READ(5, *) (TABMSD(I), I=1, MMM)
      READ(6, *) NREG1, NREG2, NREG3, NREG4
      READ(6, *) VA, VC
      READ(6, *) FIA1, FIA2, FIA3
      READ(6, *) TIME, TIMER
      READ(6, *) DISL1, DISL2, DISL3, DISL4
      READ(6, *) VVE, VVK
      READ(6, *) APIL, APILR, AMAI, AMAIR
      READ(6, *) DNOZL, DSHID, VPL, VSD
      READ(6, *) FLMOL, SDMOL, UR
      READ(6, *) ITMAX, DHMAX, DTMAX
      READ(6, *) TW1, TW2, TW4, HSUR2, HSUR4
      READ(6, *) DXW, TAMBI, DPOLAR, AMDW
      READ(6, *) PSIA, PAMBI, CPSD
      READ(6, *) ALFA, VWELD
      READ(6, *) NX, NY
      READ(6, *) X(1), X(NX)
      READ(6, *) Y(1), Y(NY)
```

```

READ(6,*) TM,TO
READ(6,*) THK,EPFL
READ(6,*) DENS,HFUSI
VOLPL=VPL/1.27133/1.E5
VOLSD=VSD/1.27133/1.E5
FMPL=VOLPL*FAMBI*PLMOL/8315./TAMBI
FMSD=VOLSD*FAMBI*SDMOL/8315./TAMBI
UH=VOLSD*4./3.14159/(DSHID**2-DNOZL**2)
AREAW=3.14159*DPOLAR**2/4.
WRITE(7,1030) DISL1,DISL2,DISL3,DISL4
WRITE(7,1040) APIL,APILR,AMAI,AMAIR
WRITE(7,1060) FIA1,FIA2,FIA3
WRITE(7,1070) VA,VC
WRITE(7,1130) PLMOL,SDMOL,UR
ELOS=1.5*VVK/VVE/1.E10
GHW=((AMAI+APIL)*(VC-FIA1)*TIME+(AMAIR-APILR)*(VA+FIA1)*
$   TIMER)/(TIME+TIMER)/1000.
CONDW=AMDW*AREAW*(TW1-TAMBI)/DXW
POW1(1)=GHW-CONDW
ENT1(1)=POW1(1)/FMPL
CALL INSEP(TABIPL,TABTEM,ENT1(1),TEMP1(1))
ELOS1=ELOS*TEMP1(1)*(AMAIR-APILR)*TIMER/(TIME+TIMER)
AMPCP1=((AMAI+APIL)*TIME+(AMAIR-APILR)*TIMER)/(TIME+TIMER)
DX1=DISL1/FLOAT(NREG1)
GEOL1=3.14159*((DPOLAR+DNOZL)/2.）**2/4./DX1
VOLUM1=3.14159*((DNOZL+DPOLAR)/2.）**2/4.*DX1
MREG1=NREG1+1
SUMQ1=0.
DUBC=0.
DO 40 M=2,MREG1
N=M-1
DUDL1(N)=2000.
QLOS1(N)=0.
NN1=0
10 CONTINUE
NN1=NN1+1
IF(NN1.GT.200) THEN
  WRITE(*,*)'      NN1.GT.200.  Erra stop'
  STOP
ENDIF
DP1=DUDL1(N)*DX1*AMPCP1/1000.-QLOS1(N)
POW1(M)=POW1(N)+DP1
ENT1(M)=POW1(M)/FMPL
ENTCP1=(ENT1(N)+ENT1(M))/2.
CALL INSEP(TABIPL,TABTEM,ENTCP1,TEMCP1)
QLOS1(N)=VOLUM1*4.*1.E7*(TEMCP1/15000.）**16/
$   (1.+(TEMCP1/15000.）**16)
CALL INSEP(TABTEM,TABMPL,TEMCP1,PLMHO)
OHM1=1./PLMHO/GEOL1
DUDL=AMPCP1*OHM1/DX1
DIFU=1.-DUDL/DUDL1(N)
IF(ABS(DIFU).GE.0.005) THEN
  DUDL1(N)=(DUDL+DUDL1(N))/2.
  GO TO 10

```

```

ENDIF
DUBC=DUBC+DUDL1(N)*DX1
SUMQ1=SUMQ1+QLOS1(N)
CALL INSEP(TABIFL,TABTEM,ENT1(M),TEMP1(M))
40 CONTINUE
C WRITE(7,1170) (POW1(I),I=1,MREG1)
C WRITE(7,1180) (ENT1(I),I=1,MREG1)
C WRITE(7,1190) (QLOS1(I),I=1,NREG1)
C WRITE(7,1200) (TEMP1(I),I=1,MREG1)
C WRITE(7,1220) (DUDL1(I),I=1,NREG1)
C WRITE(7,1210) SUMQ1,DUBC
C-----
POW2(1)=POW1(MREG1)
ENT2(1)=ENT1(MREG1)
TEMP2(1)=TEMP1(MREG1)
AMPCF2=(AMAI*TIME+(AMAIR-APILR)*TIMER)/(TIME+TIMER)
DX2=DISL2/FLOAT(NREG2)
AREA2=3.14159*DNOZL*DX2
GEOL2=3.14159*DNOZL**2/4./DX2
MREG2=NREG2+1
C WRITE(7,1230)
GHN1=(APIL*FIA2*TIME+APILR*FIA2*TIMER)/(TIME+TIMER)/1000.
GHN2=(APIL*VA*TIME+APILR*VA*TIMER)/(TIME+TIMER)/1000.
SUMQ2=GHN1+PSIA*GHN2
DUCG=0.
DO 80 M=2,MREG2
  N=M-1
  XM=FLOAT(N)*DX2-DX2/2.
  DUDL2(N)=2000.
  QLOS2(N)=0.
  NN2=0
50 CONTINUE
  NN2=NN2+1
  IF(NN2.GT.200) THEN
    WRITE(*,*) ' Erro Stop      ENT3=',ENT3
    STOP
  ENDIF
  IF(NREG2.EQ.1) THEN
    ELOS2(N)=ELOS*TEMP2(N)*(APIL*TIME+APILR*TIMER)/(TIME+TIMER)
  ELSE IF(NREG2.NE.1.AND.N.EQ.1) THEN
    ELOS2(N)=ELOS*TEMP2(N)*APIL*TIME/(TIME+TIMER)
  ELSE IF(NREG2.NE.1.AND.N.EQ.NREG2) THEN
    ELOS2(N)=ELOS*TEMP2(N)*APILR*TIMER/(TIME+TIMER)
  ENDIF
  DP2=DUDL2(N)*DX2*AMPCF2/1000.+(1.-PSIA)*GHN2/FLOAT(NREG2)
  $ -ELOS2(N)-QLOS2(N)
  POW2(M)=POW2(N)+DP2
  ENT2(M)=POW2(M)/FMFL
  ENTCP=(ENT2(N)+ENT2(M))/2.
  CALL INSEP(TABIFL,TABTEM,ENTCP,TEMCP)
  CALL INSEP(TABTEM,TABKPL,TEMCP,AMD)
  CALL INSEP(TABTEM,TABCPL,TEMCP,CP)
  CALL INSEP(TABTEM,TABMPL,TEMCP,PLMH0)
  COEFC=2.*FMFL*CP/3.14159/AMD

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XPLUS=COEFC/XM
VNUX=0.2233*XPLUS**0.7455+3.66
ALFAX=VNUX*AMD/DNOZL
QLOS2(N)=ALFAX*AREA2*(ENTCP-HSUR2)/CF
OHM2=1./PLMHD/GEOL2
DUDL=AMP2*OHM2/DX2
DIFU=1.-DUDL/DUDL2(N)
IF (ABS(DIFU).GE.0.005) THEN
    DUDL2(N)=(DUDL+DUDL2(N))/2.
    GO TO 50
ENDIF
DUCG=DUCG+DUDL2(N)*DX2
SUMQ2=SUMQ2+QLOS2(N)+ELOS2(N)
CALL INSEP(TABIFL,TABTEM,ENT2(M),TEMP2(M))
80 CONTINUE
C    WRITE(7,1250) (POW2(I),I=1,MREG2)
C    WRITE(7,1260) (ENT2(I),I=1,MREG2)
C    WRITE(7,1270) (QLOS2(I),I=1,NREG2)
C    WRITE(7,1280) (TEMP2(I),I=1,MREG2)
C    WRITE(7,1290) (ELOS2(I),I=1,NREG2)
C    WRITE(7,1300) (DUDL2(I),I=1,NREG2)
C    WRITE(7,1310) SUMQ2,DUCG
C    WRITE(7,1320)
C-----
RO=DNOZL/2.
POW3(1)=POW2(MREG2)
MITER=0
90 CONTINUE
    MITER=MITER+1
    IF(MITER.GT.200) THEN
        WRITE(*,*) '      Error Stop      MITER.GT.200,DPP=',DPP
        STOP
    ENDIF
    ENT3(1)=POW3(1)/FMPL
    CALL INSEP(TABIFL,TABTEM,ENT3(1),TEMP3(1))
    DENSO=PAMBI*PLMOL/8315./TEMP3(1)
    UO=FMPL/DENSO/3.14159/RO**2
    ENERG(1)=FMPL*UO**2/2./1000.
    PFP=POW2(MREG2)-ENERG(1)
    DPP=ABS(1.-PFP/POW3(1))
    POW3(1)=PFP
    IF(DPP.GE.0.005) GO TO 90
    COEFM=UH/UO
C    WRITE(7,1340) UH,UO,COEFM
    VMID1=(1.-COEFM)/(1.+COEFM)
    VMID3=1.+0.8*COEFM-0.45*COEFM**2
    DX3=DISL3/FLOAT(NREG3)
    MREG3=NREG3+1
    SUMQ3=0.
    DUGE=0.
    R1(1)=RO
    R2(1)=RO
    FLWPL(1)=FMPL
    FLWSD(1)=0.

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AMPCP3=(AMAI*TIME+AMAIR*TIMER)/(TIME+TIMER)
DO 190 M=2,MREG3
  N=M-1
  X3=FLOAT(N)*DX3
  VMID2=0.27*X3
  VMID4=VMID1*(0.416+0.134*COEFM+0.021*VMID2*VMID1*VMID3/RO)
  R1(M)=RO-VMID2*VMID4
  VMIDA=0.021*VMID3/RO
  VMIDB=0.416+0.134*COEFM
  VMIDC=R1(M)-RO
  VMIDD=(-VMIDB+SQRT(VMIDB**2-4.*VMIDA*VMIDC))/2./VMIDA
  R2(M)=R1(M)+VMIDD
  NOM=0
  TBEGI=TEMP3(1)
  DENBEG=DENSO
  DR=(R2(M)-R1(M))/10.
  DUDL2(N)=2000.
  GEOL3=3.14159*R2(M)**2/DX3
120  CONTINUE
  NOM=NOM+1
  IF(NOM.GT.200) THEN
    WRITE(*,*)'      Erro Stop      ITER.IN STANDOFF EXCEED 200'
    STOP
  ENDIF
  FLWFL(M)=3.14159*R1(M)**2*UO*DENBEG
  FLWSD(M)=0.
  ENERG(M)=FLWFL(M)*UO**2/2./1000.
  CALL INSEP(TABTEM,TABIFL,TBEGI,EBEGI)
  POWER=FLWFL(M)*EBEGI
DO 150 K=1,10
  RMID=FLOAT(K)*DR-DR/2.+R1(M)
  ATA=(R2(M)-RMID)/(R2(M)-R1(M))
  UMID=UO-(UO-UH)*(1.-ATA**1.5)**2
  TMID=TBEGI-(TBEGI-TAMBI)*(1.-ATA)
  PGFL=PAMBI/(1.+(1./ATA-1.)*PLMOL/SDMOL)
  PGSD=PAMBI-PGFL
  DENFL=PGFL*PLMOL/8315./TMID
  DENSD=PGSD*SDMOL/8315./TMID
  VOLUM=2.*3.14159*RMID*DR*UMID
  FLWFL(M)=FLWFL(M)+VOLUM*DENFL
  FLWSD(M)=FLWSD(M)+VOLUM*DENSD
  ENERG(M)=ENERG(M)+(DENFL+DENSD)*VOLUM*UMID**2/2./1000.
  IF(TMID.GE.3000.) THEN
    CALL INSEP(TABTEM,TABIFL,TMID,ENTPL)
    CALL INSEP(TABTEM,TABISD,TMID,ENTSD)
  ELSE
    ENTPL=TABCPL(1)*TMID
    ENTSD=TABCS(1)*TMID
  ENDIF
  POWER=POWER+VOLUM*(DENFL*ENTPL+DENSD*ENTSD)
150  CONTINUE
  POWRCF=(POWER+POW3(N))/2.
  PLCF=(FLWFL(M)+FLWFL(N))/2.
  SDCP=(FLWSD(M)+FLWSD(N))/2.

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CALL AVERT (FLCP,SDCP,POWRCP,TABTEM,TABIPL,TABISD,TCF)
VRADI=3.14159*(R2(M)+R2(N))*2/4.*DX3
QLOS3(N)=VRADI*4.*1.E7*(TCP/15000.)*16/(1.+(TCP/15000.)*16)
CALL INSEP (TABTEM,TABMPL,TCF,PLMHO)
CALL INSEP (TABTEM,TABMSD,TCF,SDMHO)
CFMHO=((FLWPL(M)+FLWPL(N))*PLMHO+(FLWSD(M)+FLWSD(N))*SDMHO)/
$      (FLWPL(M)+FLWPL(N)+FLWSD(M)+FLWSD(N))
OHM3=1./CFMHO/GEOL3
DUDL3(N)=OHM3*AMP3/DX3
DP3=OHM3*AMP3**2/1000.
POW3(M)=POW3(N)+DP3-QLOS3(N)+(FLWSD(M)-FLWSD(N))*CPSD*TAMBI-
$      (ENERG(M)-ENERG(N))
PMP=1.-POWER/POW3(M)
IF (ABS(PMP).GE.0.010) THEN
  TBEGI=TBEGI*(1.+PMP/10.)
  DENBEG=PAMBI*PLMOL/8315./TBEGI
  UO=UO*FMPL/FLWPL(M)
  GO TO 120
ENDIF
WRITE(*,1390) N,NOM,PMP
SUMQ3=SUMQ3+QLOS3(N)
CALL AVERT (FLWPL(M),FLWSD(M),POWER,TABTEM,TABIPL,TABISD,
$      TEMP3(M))
ENT3(M)=POW3(M)/(FLWPL(M)+FLWSD(M))
DUGE=DUGE+DUDL3(N)*DX3
190 CONTINUE
WRITE(*,1480) (FLWPL(I),I=1,MREG3)
WRITE(7,1480) (FLWPL(I),I=1,MREG3)
WRITE(7,1490) (FLWSD(I),I=1,MREG3)
PAID=FLWSD(MREG3)*CPSD*TAMBI
C-----
RBOUND=R0
ITWID=1
DO 191 N=1,NREG4
  Bhole(N)=RBOUND
191 CONTINUE
195 CONTINUE
ATARB=(R2(MREG3)-RBOUND)/(R2(MREG3)-R1(MREG3))
TBOUND=TBEGI-(1.-ATARB)*(TBEGI-TAMBI)
WRITE(7,1540) TBOUND
DR=(R2(MREG3)-RBOUND)/10.
FLLOS=0.
SDLOS=0.
QLOSJ=0.
QGETJ=0.0
SDGET=0.0
DO 220 K=1,10
  RMID=FLOAT(K)*DR-DR/2.+RBOUND
  ATA=(R2(MREG3)-RMID)/(R2(MREG3)-R1(MREG3))
  UMID=UO-(UO-UH)*(1.-ATA**1.5)**2
  TMID=TBEGI-(TBEGI-TAMBI)*(1.-ATA)
  PGPL=PAMBI/(1.+(1./ATA-1.)*PLMOL/SDMOL)
  PGSD=PAMBI-PGPL
  DENPL=PGPL*PLMOL/8315./TMID

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DENSD=PGSD*SDMDL/8315./TMID
VOLUM=2.*3.14159*RMID*DR*UMID
FLLOS=FLLOS+VOLUM*DENFL
SDLOS=SDLOS+VOLUM*DENSD
IF (TMID.GE.3000.) THEN
    CALL INSEP (TABTEM,TABIFL,TMID,ENTFL)
    CALL INSEP (TABTEM,TABISD,TMID,ENTSD)
ELSE
    ENTFL=TABCPL(1)*TMID
    ENTSD=TABCSD(1)*TMID
ENDIF
QLOSJ=QLOSJ+VOLUM*(DENFL*ENTFL+DENSD*ENTSD)
220 CONTINUE
C-----
    GHK1=(AMAI*FIA3*TIME+AMAIR*(UR-FIA3)*TIMER)/(TIME+TIMER)/1000.
    GHK2=(AMAI*VA*TIME+AMAIR*VC*TIMER)/(TIME+TIMER)/1000.
C-----
225 CONTINUE
    POWER=POW3(MREG3)-QLOSJ+QGETJ
    PLM=FMPL-FLLOS
    SDM=FLWSD(MREG3)-SDLOS+SDGET
    POW4(1)=POWER+(1.-PSIA)*GHK2
    ENT4(1)=POW4(1)/(PLM+SDM)
    CALL AVERT(PLM,SDM,POW4(1),TABTEM,TABIFL,TABISD,TEMP4(1))
    SUMQ4=0.
    DP4=0.
    ELOSS=ELOS*TEMP4(1)*AMAI*TIME/(TIME+TIMER)
    GHK12=GHK1+PSIA*GHK2
C    WRITE(7,1555)
    DL=DISL4/FLOAT(NREG4)
    MREG4=NREG4+1
    DO 230 I=2,MREG4
        J=I-1
        XSOUR(J)=FLOAT(J)*DL-DL/2.
        AREA(J)=3.14159*BHOLE(J)*DL
230 CONTINUE
C    WRITE(7,1560) (XSOUR(K),K=1,NREG4)
C    WRITE(7,1570) RBOUND
C    WRITE(7,1580) (AREA(K),K=1,NREG4)
    WRITE(7,1590) PLM,SDM,TEMP4(1)
    DO 240 M=2,MREG4
        N=M-1
        QSEGM(N)=3.*GHK12*(1.-XSOUR(N)/DISL4)**2*DL/DISL4
        ELOS4(N)=3.*ELOSS*(1.-XSOUR(N)/DISL4)**2*DL/DISL4
        CALL CONV4(XSOUR(N),AREA(N),DP4,POW4(N),POW4(M),ENT4(M),
$           QLOS4(N),HSUR4,ELOS4(N),BHOLE(N))
        CALL AVERT(PLM,SDM,POW4(M),TABTEM,TABIFL,TABISD,TEMP4(M))
        QSOUR(N)=QLOS4(N)+ELOS4(N)+QSEGM(N)
        SUMQ4=SUMQ4+QSOUR(N)
240 CONTINUE
    CALL WIDTH(SUMQ4,QSOUR,XSOUR,NREG4,DISL4,ALFA,VWELD,BHOLE0,ITWID)
    ITWID=ITWID+1
    WRITE(*,*) 'RO=',RO,' RBOUND=',RBOUND,' R2(MREG3)=' ,R2(MREG3)
    DRB=0.0

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DO 250 J=1,NREG4
  DRB=AMAX1(DRB,ABS(BHOLE0(J)-BHOLE(J))/BHOLE(J))
250 CONTINUE
  IF(DRB.GE.0.002) THEN
    DO 260 J=1,NREG4
      BHOLE(J)=BHOLE(J)+.5*(BHOLE0(J)-BHOLE(J))
260 CONTINUE
      RBOUND=BHOLE(1)
      IF(RBOUND.GE.R2(MREG3)) THEN
        DENSD=PAMBI*SDMOL/8315./TAMBI
        QLOSJ=0.0
        PLLOS=0.0
        SDLOS=0.0
        SDGET=3.14159*(RBOUND**2-R2(MREG3)**2)*UH*DENSD
        QGETJ=SDGET*TAMBI*CPSD
        GO TO 225
      ELSE
        GO TO 195
      ENDIF
    ENDIF
  ENDIF
C   WRITE(7,1600) QIMPIN
C   WRITE(7,1610) (POW4(I),I=1,MREG4)
C   WRITE(7,1620) (ENT4(I),I=1,MREG4)
C   WRITE(7,1630) (TEMP4(I),I=1,MREG4)
C   WRITE(7,1640) (QLOS4(I),I=1,NREG4)
C   WRITE(7,1650) (ELOS4(I),I=1,NREG4)
C   WRITE(7,1660) (QSEGM(I),I=1,NREG4)
C   WRITE(7,1670) (QSOUR(I),I=1,NREG4)
  WRITE(7,1680) SUMQ4
  PTOTOU=CONDW+SUMQ1+SUMQ2+SUMQ3+SUMQ4+POW4(MREG4)
$   +QLOSJ+ENERG(MREG3)
  PTOTIN=GHW+(AMPCP1*DUBC+AMPCP2*DUCG+AMPCP3*DUGE)/1000.
$   +GHN1+GHN2+GHK1+GHK2+PAID
  WRITE(7,1690) PTOTIN,PTOTOU
  PERCQW=CONDW/PTOTIN
  PERQG=SUMQ1/PTOTIN
  PERQN=SUMQ2/PTOTIN
  PERQSR=SUMQ3/PTOTIN
  PERQSC=QLOSJ/PTOTIN
  PERQW=SUMQ4/PTOTIN
  PERQD=POW4(MREG4)/PTOTIN
  PERSUM=PERCQW+PERQG+PERQN+PERQSR+PERQSC+PERQW+PERQD
  WRITE(7,1700) CONDW,PERCQW
  WRITE(7,1710) SUMQ1,PERQG
  WRITE(7,1720) SUMQ2,PERQN
  WRITE(7,1730) SUMQ3,PERQSR
  WRITE(7,1740) QLOSJ,PERQSC
  WRITE(7,1750) SUMQ4,PERQW
  WRITE(7,1760) POW4(MREG4),PERQD
  WRITE(7,1770) PERSUM
  WRITE(7,1780) AMPCP1,AMPCP2,AMPCP3
  DUBE=DUBC+DUCG+DUGE
  DUAF=DUBE+VA+VC+FIA3-FIA1
  DUAFR=DUBE+VA+VC-FIA3+FIA1+UR

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WRITE(7,1790) DUBE,DUAF,DUAFR
DUFF=DUBC+VA+VC+FIA2-FIA1
DUPR=FIA2-FIA1-DUBC-DUCG
PTOTAL=((AMAI*DUAF+APIL*DUFF)*TIME+(AMAIR*DUAFR+APILR*DUPR)*
$   TIMER)/(TIME+TIMER)/1000.
C   PTOTAL=(AMAI*DUAF*TIME+AMAIR*DUAFR*TIMER)/(TIME+TIMER)/1000.
ATAQ4=SUMQ4/PTOTAL
WRITE(7,1800) DUFF,DUPR
WRITE(7,1810) PTOTAL,SUMQ4,ATAQ4
WRITE(7,*) ' CROWN WIDTH=',2.*BHOLE(1),' (mm)'
WRITE(7,*) ' ROOT WIDTH=',2.*BHOLE(NREG4),' (mm)'
STOP

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C-----
1000  FORMAT(///5X,'INPUT DATA:')
1010  FORMAT(/2X,'PLSMA (kg/s)',E12.5,2X,'SHIELD (kg/s)',E12.5)
1020  FORMAT(/5X,'TW OF W,NOZZLE,HOLE,INITIAL SOLID',3F8.1,/
$     5X,'ENT. OF ARC IN TW OF NOZZLE,HOLE',2E12.5)
1030  FORMAT(/5X,'L1,L2,L3,L4 (m)',2X,4F10.8)
1040  FORMAT(/5X,'PILOT I(+)=' ,F8.2,5X,'PILOT I(-)=' ,F8.2,/
$     5X,'MAIN I(+)=' ,F8.2,5X,'MAIN I(-)=' ,F8.2)
1050  FORMAT(/5X,'t(+)=' ,E11.4,5X,'t(-)=' ,E11.4)
1060  FORMAT(/5X,'WORK FUNCTION 1,2,3 =' ,3F5.2)
1070  FORMAT(/5X,'ANODE DROP=' ,F5.2,
$     2X,'CATHOD DROP=' ,F5.2)
1080  FORMAT(/5X,'e=' ,E12.5,5X,'k=' ,E12.5)
1090  FORMAT(/5X,'NREG1=' ,I3,2X,'NREG2=' ,I3,2X,'NREG3=' ,I3,
$     2X,'NREG4=' ,I3)
1100  FORMAT(/5X,'NOZZLE DIAM.(m)' ,F8.6,2X,'SHIELD DIAM.(m)' ,F8.6)
1110  FORMAT(/5X,'LENGTH OF POLARITY W =' ,E12.5,
$     /5X,'ENVIRONMENT TEMP. =' ,F6.1,2X,'AREA OF W POLARITY' ,
$     E12.5,/5X,'AMD OF POLARITY W =' ,E12.5)
1120  FORMAT(/5X,'ITMAX,DHMAX,DTMAX=' ,I4,E12.5,F6.4)
1125  FORMAT(/5X,'PSIA=' ,F6.4,2X,'PAMBI(N/m**2)=' ,F10.1,/
$     2X,'CF. OF HE IN AMBIENT (kJ/kg)=' ,E12.5,
$     2X,' (m/s)' ,E12.5)
1130  FORMAT(/5X,'PLASMA MOL.WEIGHT (kg/kmol)=' ,F8.4,2X,
$     /5X,'SHIELD MOL.WEIGHT (kg/kmol)=' ,F8.4,
$     /5X,'UR=' ,F5.1)
1140  FORMAT(/2X,'GHW,CONDW,ELOS1(kw)' ,3E12.5)
1150  FORMAT(//5X,'BEGINING OF SEGMENT ONE')
1170  FORMAT(/2X,'POW1=' ,4E12.5,/7X,4E12.5)
1180  FORMAT(/2X,'ENT1=' ,4E12.5,/7X,4E12.5)
1190  FORMAT(/1X,'QLOS1=' ,4E12.5,/7X,4E12.5)
1200  FORMAT(/2X,'TEMP1=' ,4E12.5,/8X,4E12.5)
1210  FORMAT(/2X,'TOTAL LOSS IN GAP I' ,E12.5,2X,'DUBC(v)' ,F6.2)
1220  FORMAT(/2X,'DUDL1' ,4E12.5,/7X,4E12.5)
1230  FORMAT(//5X,'NOZZLE COMPUTATION')
1240  FORMAT(/5X,'NN2.GT.100')
1250  FORMAT(/5X,'POW2=' ,4E12.5/10X,4E12.5)
1260  FORMAT(/5X,'ENT2=' ,4E12.5/10X,4E12.5)
1270  FORMAT(/4X,'QLOS2=' ,4E12.5/10X,4E12.5)
1280  FORMAT(/2X,'TEMP2' ,4E12.5,/7X,4E12.5)
1290  FORMAT(/2X,'ELOS2' ,4E12.5,/7X,4E12.5)
1300  FORMAT(/2X,'DUDL2' ,4E12.5,/7X,4E12.5)

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1310 FORMAT(/5X,'TOTAL LOSS IN NOZZLE =' ,E12.5,2X,'DUCG(v)' ,F6.2)
1320 FORMAT(/5X,'STANDOFF COMPUTATION')
1340 FORMAT(/5X,'UH,UO,COEFM',3E12.5)
1350 FORMAT(/2X,'LINE 285 TBEGI',E12.4)
1370 FORMAT(/1X,'ATA,TBEGI,TAMBI,TMID',4E11.4)
C1360 FORMAT(1X,'M,R1,R2,DR,RMID,ATA',I2,2E12.5,/5X,3E12.5)
1380 FORMAT(/2X,'IN MAIN,NOM,MAR,MHE,POWER',I4,2X,3E10.3)
1390 FORMAT(/2X,'ITER.IN STANDOFF,SEG.=' ,I2,2X,'NOM=' ,I4,
$      2X,'PMP=' ,F10.6)
1450 FORMAT(/2X,'TOTAL LOSS IN STANDOFF =' ,E12.5,2X,'DUGE(v)' ,F6.2)
1410 FORMAT(/5X,'POW3=' ,4E12.5,/10X,4E12.5)
1430 FORMAT(/4X,'QLOS3=' ,4E12.5,/10X,4E12.5)
1440 FORMAT(/4X,'TEMP3=' ,4E12.5,/10X,4E12.5)
1460 FORMAT(/5X,'R1(m)=' ,4F10.8,/11X,4F10.8)
1470 FORMAT(/5X,'R2(m)=' ,4F10.8,/11X,4F10.8)
1480 FORMAT(/5X,'FLWPL=' ,4E12.5,/11X,4E12.5)
1490 FORMAT(/5X,'FLWSD=' ,4E12.5,/11X,4E12.5)
1500 FORMAT(/5X,'ENERG=' ,4E12.5,/11X,4E12.5)
1510 FORMAT(/2X,'DUDL3',4E12.5,/7X,4E12.5)
1520 FORMAT(/5X,'POWER AID FROM SHIELD, PAID(kw)=' ,E12.5)
1530 FORMAT(/2X,'VELOC.,TEMP.IN CORE AT LAST',2E12.5)
1540 FORMAT(/5X,'T OF BOUNDARY, TBOUND=' ,E12.5)
1550 FORMAT(/5X,'CONVECTIVE LOSS OF JET (kw)' ,E12.5)
1555 FORMAT(/10X,'WORKPIECE COMPUTATION')
1560 FORMAT(/2X,'XSOUR',2X,5F8.6)
1570 FORMAT(/5X,'RADIUS OF KEYHOLE (m)=' ,E12.5)
1580 FORMAT(/2X,'AREA(m**2)' ,4E12.5,/12X,4E12.5)
1590 FORMAT(/4X,'FLM,SDM,TEMP4(1)' ,3E14.5)
1600 FORMAT(/5X,'IMPINGE LOSS (kw)' ,F8.5)
1610 FORMAT(/2X,'POW4=' ,4E12.5,/7X,4E12.5)
1620 FORMAT(/2X,'ENT4=' ,4E12.5,/7X,4E12.5)
1630 FORMAT(/2X,'TEMP4=' ,4E12.5,/8X,4E12.5)
1640 FORMAT(/2X,'QLOS4=' ,4E12.5,/8X,4E12.5)
1650 FORMAT(/2X,'ELOS4=' ,4E12.5,/8X,4E12.5)
1660 FORMAT(/2X,'QSEGM=' ,4E12.5,/8X,4E12.5)
1670 FORMAT(/2X,'QSOUR=' ,4E12.5,/8X,4E12.5)
1680 FORMAT(/5X,'TOTAL LOSS IN WORKPIECE =' ,E12.5)
1690 FORMAT(5X,'TOTAL POWER INCLUDING HELIUM, PTOTIN=' ,E12.5,/
$      5X,'TOTAL POWER FROM LOSS, PTOTOU=' ,E12.5)
1700 FORMAT(/2X,'POLARITY CONDUCT. LOSS AND PERCENT.' ,2E12.5)
1710 FORMAT(/2X,'GAP LOSS AND PERCENTAGE' ,2E12.5)
1720 FORMAT(/2X,'NOZZLE LOSS AND PERCENTAGE' ,2E12.5)
1730 FORMAT(/2X,'RADIAT.IN STANDOFF AND PERCENTAGE' ,2E12.5)
1740 FORMAT(/2X,'CONVEC.IN STANDOFF AND PERCENTAGE' ,2E12.5)
1750 FORMAT(/2X,'WORKPIECE LOSS AND PERCENTAGE' ,2E12.5)
1760 FORMAT(/2X,'DISCHARGE LOSS AND PERCENTAGE' ,2E12.5)
1770 FORMAT(/5X,'SUM. PERCENTAGE' ,F8.5)
1780 FORMAT(/5X,'AMPFCP1,2,3' ,3E12.5)
1790 FORMAT(/5X,'DUBE,DUAF,DUAFR' ,3E12.5)
1800 FORMAT(/4X,'DUPF=' ,E12.4,4X,'DUPR=' ,E12.4)
1810 FORMAT(/2X,'POWER,Q4,ATAQ4=' ,3E14.5)
      END

```

C

C-----

C

```

SUBROUTINE CONV4(XMID,AMID,DP,PA,PB,HB,PCONV,HW,QELOS,RHOLE)
COMMON MMM
COMMON TABTEM(26),TABIFL(26),TABCPL(26),TABKPL(26),TABISD(26)
COMMON ITMAX,DHMAX,DTMAX
COMMON TAMBI,DNOZL,FMPL
COMMON TABCSD(26),TABKSD(26)
COMMON TW4,MREG4,NREG4
COMMON PLM,SDM
PB=PA
NOM=0
200 CONTINUE
  NOM=NOM+1
  IF(NOM.GT.ITMAX) THEN
    WRITE(*,*)'  Erro Stop  ITERATIONS EXCEED ITMAX IN CONV4'
    STOP
  ENDIF
  PCP=(PA+PB)/2.
  HCP=PCP/(PLM+SDM)
  CALL AVERT(PLM,SDM,PCP,TABTEM,TABIFL,TABISD,TCP)
  CALL INSEP(TABTEM,TABKPL,TCP,FLAMD)
  CALL INSEP(TABTEM,TABKSD,TCP,SDAMD)
  AMD=(FLAMD*PLM+SDAMD*SDM)/(PLM+SDM)
  CALL INSEP(TABTEM,TABCPL,TCP,PLCP)
  CALL INSEP(TABTEM,TABCSD,TCP,SDCP)
  CP=(PLCP*PLM+SDCP*SDM)/(PLM+SDM)
  COEFC=2.*(PLM+SDM)*CP/3.14159/AMD
  XPLUS=COEFC/XMID
  VNUX=0.2233*XPLUS**0.7455+3.66
  ALFAX=VNUX*AMD/RHOLE/2.
  PCONV=ALFAX*AMID*(HCP-HW)/CP
  POU=PA-PCONV+DP-QELOS
  HB=POU/(PLM+SDM)
  DIFF=ABS(POU-PB)/PB
  PB=POU
  IF(DIFF.GE.DHMAX) GO TO 200
END

```

C

C-----

C

```

SUBROUTINE AVERT(FLOPL,FLOSD,PSUM,TABT,TABPL,TABSD,TVERA)
DIMENSION TABT(26),TABPL(26),TABSD(26)
COMMON MMM
C WRITE(7,3000) FLOPL,FLOSD,PSUM
NN=0
TVERA=10000.
10 CONTINUE
  NN=NN+1
  IF(NN.GT.200) THEN
    WRITE(*,*)'  Erro Stop  ITER.EXCEED 200 IN AVERT, THEN STOP'
    STOP
  ENDIF
  CALL INSEP(TABT,TABPL,TVERA,EPL)
  CALL INSEP(TABT,TABSD,TVERA,ESD)

```



```

PCOMP=FLOFL*EFL+FLOSD*ESD
DPOWR=1.-PCOMP/PSUM
IF (ABS(DPOWR).GE.0.010) THEN
TVERA=TVERA*(1.+DPOWR/10.)
GO TO 10
ENDIF
RETURN
END

```

C
C-----
C

```

SUBROUTINE INSEP(A,B,C,D)
DIMENSION A(26),B(26)
COMMON MMM
IF(C.LT.A(1).OR.C.GT.A(MMM)) THEN
WRITE(*,*)'  Erro Stop      INDEP. IS BEYOND SCOPE'
WRITE(*,*)'  C=',C,'A(1)=' ,A(1),'A(MMM)=' ,A(MMM)
STOP
ENDIF
DO 30 K=2,MMM
    IF((C.LE.A(K).AND.C.GE.A(K-1)).OR.
$    (C.GE.A(K).AND.C.LE.A(K-1))) THEN
        D=B(K-1)+(B(K)-B(K-1))/(A(K)-A(K-1))*(C-A(K-1))
        GO TO 40
    ENDIF
30  CONTINUE
40  CONTINUE
    RETURN
4010 FORMAT(/5X,' INDEP. C=',E12.4,5X,'DEPEND. D=',E12.4)
END

```

C
C-----
C

```

SUBROUTINE WIDTH(QORIG,QSOUR,HH,NHH,H,ALPHA,VWELD,RMAX,ITWID)
DIMENSION ZZ(34),TEMP(25,15,11),TEMPO(10,25,15,11)
DIMENSION BEAD(30,10),QSOUR(10),QMOLT(10),HH(10),Q4K(10),QS(10),
$    Z(11),RMAXO(11),RMAX(11)
COMMON/DAT10/NX,NY,NZ,X(25),Y(20),TM,TO,THK,EPSL,DENS,HFUSI
IF(ITWID.GT.1) GO TO 66
IF(NX.GT.1) THEN
    DO 1 I=1,NX
        X(I)=X(1)+FLOAT(I-1)*(X(NX)-X(1))/FLOAT(NX-1)
1    CONTINUE
    ENDIF
IF(NY.GT.1) THEN
    DO 5 J=1,NY
        Y(J)=Y(1)+FLOAT(J-1)*(Y(NY)-Y(1))/FLOAT(NY-1)
5    CONTINUE
    ENDIF
NZ=NHH
IF(NZ.GT.1) THEN
    DO 6 K=1,NZ
        Z(K)=FLOAT(K-1)*H/FLOAT(NZ-1)
6    CONTINUE

```

```

ENDIF
NOM=1
DO 8 L=1,NHH
  HH(L)=FLOAT(L-1)*H/FLOAT(NHH-1)
8 CONTINUE

```

C-----

```

  TMOLT=TM-TO
  V=VWELD*0.0254/60.
  V2A=-V/(2.*ALPHA)
  NITER=0
  NZ=NHH+1
  QTOTAL=QORIG
DO 10 I=1,NZ
  RMAX(I)=0.0
  Z(I)=FLOAT(I-1)*H/FLOAT(NZ-1)
10 CONTINUE
  DO 40 N=1,NHH
    QS(N)=QSOOR(N)
    DO 30 L=1,NZ
      DO 25 K=1,NY
        DO 20 J=1,NX
          TEMPO(N,J,K,L)=0.
20      CONTINUE
25      CONTINUE
30      CONTINUE
40      CONTINUE
    DO 65 N=1,NHH
      HHH=HH(N)
      ZZ(1)=-16.*H-HHH
      ZZ(2)=-16.*H+HHH
      DO 50 K=3,34,2
        ZZ(K)=ZZ(K-2)+2.*H
        ZZ(K+1)=ZZ(K-1)+2.*H
50      CONTINUE
      DO 64 K=1,NX
        DO 63 L=1,NY
          DO 62 J=1,NZ
            DO 60 M=1,34
              ZZZ=Z(J)-ZZ(M)
              XXX=X(K)
              YYY=Y(L)
              R=SQRT(XXX**2+YYY**2+ZZZ**2)
              RX=R+XXX
              RX=V2A*RX
              TEMPO(N,K,L,J)=TEMPO(N,K,L,J)+EXP(RX)/R
60          CONTINUE
62          CONTINUE
63          CONTINUE
64          CONTINUE
65          CONTINUE

```

C-----

```

66 CONTINUE
  NITER=NITER+1
  IF(NITER.GT.200) THEN

```

```

        WRITE(*,*) ' Erro Stop          NITER.GT.200 IN WIDTH, THEN STOP'
        STOP
    ENDIF
    DO 68 N=1,NHH
        Q4K(N)=QS(N)/(4.*3.14159*THK)
        QMOLT(N)=(RMAX(N)+RMAX(N+1))*H/FLOAT(NHH)*V*DENS*HFUSI
        Q4K(N)=(QS(N)-QMOLT(N))/(4.*3.14159*THK)
68    CONTINUE
        DO 75 K=1,NX
            DO 74 L=1,NY
                DO 73 J=1,NZ
                    TEMP(K,L,J)=0.0
                    DO 72 N=1,NHH
                        TEMP(K,L,J)=TEMP(K,L,J)+Q4K(N)*TEMPO(N,K,L,J)
72                CONTINUE
73            CONTINUE
74        CONTINUE
75    CONTINUE
        DO 95 K=1,NZ
            RMAXO(K)=0.0
            DO 90 I=1,NX
                DO 80 J=2,NY
                    L=J-1
                    IF((TEMP(I,L,K).LT.TMOLT.AND.TEMP(I,J,K).GE.TMOLT).OR.
$                     (TEMP(I,L,K).GT.TMOLT.AND.TEMP(I,J,K).LE.TMOLT)) THEN
                        YMOLT=Y(L)+(Y(J)-Y(L))/(TEMP(I,J,K)-TEMP(I,L,K))*
$                     (TMOLT-TEMP(I,L,K))
                        GO TO 85
                    ENDIF
80                CONTINUE
85            RMAXO(K)=AMAX1(RMAXO(K),YMOLT)
90        CONTINUE
95    CONTINUE
        DRMAX=0
        DO 100 N=1,NZ
            DRMAX=AMAX1(DRMAX,ABS(RMAX(N)-RMAXO(N)))
            WRITE(*,*) ' N= ',N, ' 2*RMAX(N)= ',2.*RMAX(N),
$                   ' 2*RMAXO(N)= ',2.*RMAXO(N)
100    CONTINUE
        WIDTHC=2.*RMAXO(1)
        WIDTHR=2.*RMAXO(NZ)
        write(*,*) ' ROOT WIDTH= ',WIDTHR, ' CROWN WIDTH= ',WIDTHC
        write(7,*) ' ROOT WIDTH= ',WIDTHR, ' CROWN WIDTH= ',WIDTHC
        QRCRO=0.
        QRRRO=0.
        DO 120 I=2,NX
            I1=I-1
            DO 110 J=2,NY
                J1=J-1
                TRMID=(TEMP(I1,J,1)+TEMP(I1,J1,1)+TEMP(I,J1,1)
$                     +TEMP(I,J,1))/4.
                TCMID=(TEMP(I1,J,NZ)+TEMP(I1,J1,NZ)+TEMP(I,J1,NZ)
$                     +TEMP(I,J,NZ))/4.
                DX=X(I1)-X(I)

```

```

        DY=Y(J)-Y(J1)
        DAREA=2.*ABS(DX*DY)
        QRCRO=QRCRO+ABS(DAREA)*EPSL*0.00567*((TCMID+TO)/100.)**4
        QRR00=QRR00+ABS(DAREA)*EPSL*0.00567*((TRMID+TO)/100.)**4
110    CONTINUE
120    CONTINUE
        QSQS=QORIG-QRCRO-QRR00
C      QSQS=QORIG
        DQS=1.-QSQS/QTOTAL
        DB=DRMAX/WIDTHC
        IF (ABS(DQS).GE.0.005.OR.DB.GE.0.002) THEN
            WRITE(*,*)' DQS=',DQS,' DB=',DB
            QTOTAL=0.0
            DO 130 N=1,NHH
                QS(N)=QS(N)*(1.-DQS/QORIG)
                QTOTAL=QTOTAL+QS(N)
130        CONTINUE
            DO 140 N=1,NZ
                RMAX(N)=RMAX(N)+.5*(RMAX0(N)-RMAX(N))
140        CONTINUE
            GO TO 66
        ENDIF
        RETURN
        END

```

Appendix B

***** COMPUTER PROGRAM FOR VFPA PENETRATION *****

PROGRAM WELDO.FOR, COMPILED ON MARCH 16, 1993

Point and Line Source Models are Combined to Estimate Whether
a Keyhole Can be Formed.

Impinging Convective Heat Transfer on the Surface of Workpiece
Is Taken as Convection before Keyhole Formed.

```
DIMENSION POW1(5), POW2(5), POW3(5), POW4(10)
DIMENSION ENT1(5), ENT2(5), ENT3(5), ENT4(10), TABMPL(20)
DIMENSION QLOS1(10), QLOS2(10), QLOS3(10), QLOS4(10), TABMSD(20)
DIMENSION TEMP1(5), TEMP2(5), TEMP3(5), TEMP4(10)
DIMENSION ELOS2(10), ELOS4(10), QSEGM(10), XSOUR(10)
DIMENSION AREA(10), TEMPG(11), DUDL1(10), DUDL2(10), DUDL3(10)
DIMENSION QSOUR(5), QNET(5)
DIMENSION R1(11), R2(11), FLWPL(11), FLWSD(11), ENERG(11)
common/dat10/NX, NY, X(25), Y(15), TM, TO, THK, EPSL, DENS, HFUSI
COMMON MMM
COMMON TABTEM(20), TABIPL(20), TABCPL(20), TABKPL(20), TABISD(20)
COMMON ITMAX, DHMAX, DTMAX
COMMON TAMBI, DNOZL, FMPL
COMMON TABCSD(20), TABKSD(20), TABNPL(20), TABNSD(20)
COMMON TW4, MREG4, NREG4
COMMON PLM, SDM
OPEN(5, FILE='C:WELDTAB.DAT')
OPEN(6, FILE='C:WELDIN.USE')
OPEN(7, FILE='C:WELDOU.USE')
READ(5, *) MMM
READ(5, *) (TABTEM(I), I=1, MMM)
READ(5, *) (TABIPL(I), I=1, MMM)
READ(5, *) (TABCPL(I), I=1, MMM)
READ(5, *) (TABKPL(I), I=1, MMM)
READ(5, *) (TABISD(I), I=1, MMM)
READ(5, *) (TABCSD(I), I=1, MMM)
READ(5, *) (TABKSD(I), I=1, MMM)
READ(5, *) (TABMPL(I), I=1, MMM)
READ(5, *) (TABMSD(I), I=1, MMM)
READ(5, *) (TABNPL(I), I=1, MMM)
READ(5, *) (TABNSD(I), I=1, MMM)
READ(6, *) NREG1, NREG2, NREG3, NREG4
READ(6, *) VA, VC
READ(6, *) FIA1, FIA2, FIA3
READ(6, *) TIME, TIMER
READ(6, *) DISL1, DISL2, DISL3, DISL4
READ(6, *) VVE, VVK
READ(6, *) APIL, APILR, AMAI, AMAIR
READ(6, *) DNOZL, DSHID, VPL, VSD
READ(6, *) PLMOL, SDMOL, UR
READ(6, *) ITMAX, DHMAX, DTMAX
READ(6, *) TW1, TW2, TW4, HSUR2, HSUR4
```

```
READ(6,*) DXW,TAMBI,DFOLAR,AMDW  
READ(6,*) PSIA,PAMBI,CFSD  
READ(6,*) ALFA,VWELD  
READ(6,*) NX,NY  
READ(6,*) X(1),X(NX)  
READ(6,*) Y(1),Y(NY)  
READ(6,*) TM,TO  
READ(6,*) THK,EPSL  
READ(6,*) DENS,HFUSI
```

C-----

```
WRITE(7,1000)  
WRITE(7,1001)MMM  
WRITE(7,1002)  
WRITE(7,1003)  
WRITE(7,1004)  
WRITE(7,1005)  
WRITE(7,1006)  
WRITE(7,1007)  
WRITE(7,1008)  
WRITE(7,1009)  
WRITE(7,1010)  
WRITE(7,1011)  
WRITE(7,1012)  
WRITE(7,1013)NREG1  
WRITE(7,1014)NREG2  
WRITE(7,1015)NREG3  
WRITE(7,1016)NREG4  
WRITE(7,1017)VA  
WRITE(7,1018)VC  
WRITE(7,1019)FIA1  
WRITE(7,1020)FIA2  
WRITE(7,1021)FIA3  
WRITE(7,1022)TIME  
WRITE(7,1023)TIMER  
WRITE(7,1024)DISL1  
WRITE(7,1025)DISL2  
WRITE(7,1026)DISL3  
WRITE(7,1027)DISL4  
WRITE(7,1028)VVE  
WRITE(7,1029)VVK  
WRITE(7,1030)APIL  
WRITE(7,1031)APILR  
WRITE(7,1032)AMAI  
WRITE(7,1033)AMAIR  
WRITE(7,1034)DNOZL  
WRITE(7,1035)DSHID  
WRITE(7,1036)VPL  
WRITE(7,1037)VSD  
WRITE(7,1038)PLMOL  
WRITE(7,1039)SDMOL  
WRITE(7,1040)UR  
WRITE(7,1041)ITMAX  
WRITE(7,1042)DHMAX  
WRITE(7,1043)DTMAX
```

```

WRITE(7,1044)TW1
WRITE(7,1045)TW2
WRITE(7,1046)TW4
WRITE(7,1047)HSUR2
WRITE(7,1048)HSUR4
WRITE(7,1049)DXW
WRITE(7,1050)TAMBI
WRITE(7,1051)DPOLAR
WRITE(7,1052)AMDW
WRITE(7,1053)PSIA
WRITE(7,1054)FAMBI
WRITE(7,1055)CFSD
WRITE(7,1056)ALFA
WRITE(7,1057)VWELD
WRITE(7,1058)NX
WRITE(7,1059)NY
WRITE(7,1060)X(1)
WRITE(7,1061)X(NX)
WRITE(7,1062)Y(1)
WRITE(7,1063)Y(NY)
WRITE(7,1064)TM
WRITE(7,1065)TO
WRITE(7,1066)THK
WRITE(7,1067)EPSL
WRITE(7,1068)DENS
WRITE(7,1069)HFUSI

```

C-----

```

VOLPL=VPL/1.27133/1.E5
VOLSD=VSD/1.27133/1.E5
FMPL=VOLPL*FAMBI*PLMOL/8315./TAMBI
FMSD=VOLSD*FAMBI*SDMOL/8315./TAMBI
UH=VOLSD*4./3.14159/(DSHID**2-DNOZL**2)

```

C

C----- FIRST SEGMENT CALCULATION -----

C

```

AREAW=3.14159*DPOLAR**2/4.
ELOS=1.5*VVK/VVE/1.E10
GHW=((AMAI+APIL)*(VC-FIA1)*TIME+(AMAIR-APILR)*(VA+FIA1)*
$   TIMER)/(TIME+TIMER)/1000.
CONDW=AMDW*AREAW*(TW1-TAMBI)/DXW
POW1(1)=GHW-CONDW
ENT1(1)=POW1(1)/FMPL
CALL INSEP(TABIPL,TABTEM,ENT1(1),TEMP1(1))
ELOS1=ELOS*TEMP1(1)*(AMAIR-APILR)*TIMER/(TIME+TIMER)
AMPCP1=((AMAI+APIL)*TIME+(AMAIR-APILR)*TIMER)/(TIME+TIMER)
DX1=DISL1/FLOAT(NREG1)
GEOL1=3.14159*((DPOLAR+DNOZL)/2. )**2/4./DX1
VOLUM1=3.14159*((DNOZL+DPOLAR)/2. )**2/4.*DX1
MREG1=NREG1+1
SUMQ1=0.
DUBC=0.
DO 40 M=2,MREG1
  N=M-1
  DUDL1(N)=2000.

```

```

      QLOS1(N)=0.
      NN1=0
10  CONTINUE
      NN1=NN1+1
      IF(NN1.GT.200) THEN
        WRITE(*,*) '      NN1.GT.200.  Erro stop'
        STOP
      ENDIF
      DF1=DUDL1(N)*DX1*AMPCP1/1000.-QLOS1(N)
      POW1(M)=POW1(N)+DF1
      ENT1(M)=POW1(M)/FMPL
      ENTCP1=(ENT1(N)+ENT1(M))/2.
      CALL INSEP(TABIFL,TABTEM,ENTCP1,TEMCP1)
      QLOS1(N)=VOLUM1*4.*1.E7*(TEMCP1/15000.)**16/
$   (1.+(TEMCP1/15000.)**16)
      CALL INSEP(TABTEM,TABMPL,TEMCP1,PLMHO)
      OHM1=1./PLMHO/GEOL1
      DUDL=AMPCP1*OHM1/DX1
      DIFU=1.-DUDL/DUDL1(N)
      IF(ABS(DIFU).GE.0.005) THEN
        DUDL1(N)=(DUDL+DUDL1(N))/2.
        GO TO 10
      ENDIF
      DUBC=DUBC+DUDL1(N)*DX1
      SUMQ1=SUMQ1+QLOS1(N)
      CALL INSEP(TABIFL,TABTEM,ENT1(M),TEMP1(M))
40  CONTINUE
C    WRITE(7,1170) (POW1(I),I=1,MREG1)
C    WRITE(7,1180) (ENT1(I),I=1,MREG1)
C    WRITE(7,1190) (QLOS1(I),I=1,NREG1)
C    WRITE(7,1200) (TEMP1(I),I=1,MREG1)
C    WRITE(7,1220) (DUDL1(I),I=1,NREG1)
C    WRITE(7,1210) SUMQ1,DUBC
C
C----- SECOND SEGMENT CLCULATION -----
C
      POW2(1)=POW1(MREG1)
      ENT2(1)=ENT1(MREG1)
      TEMP2(1)=TEMP1(MREG1)
      AMPCP2=(AMAI*TIME+(AMAIR-APILR)*TIMER)/(TIME+TIMER)
      DX2=DISL2/FLOAT(NREG2)
      AREA2=3.14159*DNOZL*DX2
      GEOL2=3.14159*DNOZL**2/4./DX2
      MREG2=NREG2+1
C    WRITE(7,1230)
      GHN1=(APIL*FIA2*TIME+APILR*FIA2*TIMER)/(TIME+TIMER)/1000.
      GHN2=(APIL*VA*TIME+APILR*VA*TIMER)/(TIME+TIMER)/1000.
      SUMQ2=GHN1+PSIA*GHN2
      DUCG=0.
      DO 80 M=2,MREG2
        N=M-1
        XM=FLOAT(N)*DX2-DX2/2.
        DUDL2(N)=2000.
        QLOS2(N)=0.

```



```

NN2=0
50  CONTINUE
    NN2=NN2+1
    IF (NN2.GT.200) THEN
        WRITE(*,*) ' Erro Stop      ENT3=', ENT3
        STOP
    ENDIF
    IF (NREG2.EQ.1) then
        ELOS2(N)=ELOS*TEMP2(N)*(APIL*TIME+APILR*TIMER)/(TIME+TIMER)
    else IF (NREG2.NE.1.AND.N.EQ.1) then
        ELOS2(N)=ELOS*TEMP2(N)*APIL*TIME/(TIME+TIMER)
    else IF (NREG2.NE.1.AND.N.EQ.NREG2) then
        ELOS2(N)=ELOS*TEMP2(N)*APILR*TIMER/(TIME+TIMER)
    endif
    DP2=DUDL2(N)*DX2*AMFCP2/1000.+(1.-PSIA)*GHN2/FLOAT(NREG2)
$    -ELOS2(N)-QLOS2(N)
    POW2(M)=POW2(N)+DP2
    ENT2(M)=POW2(M)/FMPL
    ENTCP=(ENT2(N)+ENT2(M))/2.
    CALL INSEP(TABIPL,TABTEM,ENTCP,TEMCP)
    CALL INSEP(TABTEM,TABKPL,TEMCP,AMD)
    CALL INSEP(TABTEM,TABCPL,TEMCP,CP)
    CALL INSEP(TABTEM,TABMPL,TEMCP,PLMH0)
    COEFC=2.*FMPL*CP/3.14159/AMD
    XPLUS=COEFC/XM
    VNUX=0.2233*XPLUS**0.7455+3.66
    ALFAX=VNUX*AMD/DNOZL
    QLOS2(N)=ALFAX*AREA2*(ENTCP-HSUR2)/CP
    OHM2=1./PLMH0/GEOL2
    DUDL=AMFCP2*OHM2/DX2
    DIFU=1.-DUDL/DUDL2(N)
    IF (ABS(DIFU).GE.0.005) THEN
        DUDL2(N)=(DUDL+DUDL2(N))/2.
        GO TO 50
    ENDIF
    DUCG=DUCG+DUDL2(N)*DX2
    SUMQ2=SUMQ2+QLOS2(N)+ELOS2(N)
    CALL INSEP(TABIPL,TABTEM,ENT2(M),TEMP2(M))
80  CONTINUE
C    WRITE(7,1250) (POW2(I),I=1,MREG2)
C    WRITE(7,1260) (ENT2(I),I=1,MREG2)
C    WRITE(7,1270) (QLOS2(I),I=1,NREG2)
C    WRITE(7,1280) (TEMP2(I),I=1,MREG2)
C    WRITE(7,1290) (ELOS2(I),I=1,NREG2)
C    WRITE(7,1300) (DUDL2(I),I=1,NREG2)
C    WRITE(7,1310) SUMQ2, DUCG
C    WRITE(7,1320)
C
C----- THIRD SEGMENT CLCULATION -----
C
    RO=DNOZL/2.
    POW3(1)=POW2(MREG2)
    MITER=0
90  CONTINUE

```

```

MITER=MITER+1
IF (MITER.GT.200) THEN
  WRITE(*,*)'      Erro Stop      MITER.GT.200,DPP=',DPP
  STOP
ENDIF
ENT3(1)=POW3(1)/FMPL
CALL INSEP(TABIPL,TABTEM,ENT3(1),TEMP3(1))
DENS0=PAMBI*PLMOL/8315./TEMP3(1)
U0=FMPL/DENS0/3.14159/R0**2
ENERG(1)=FMPL*U0**2/2./1000.
PPP=POW2(MREG2)-ENERG(1)
DPP=ABS(1.-PPP/POW3(1))
POW3(1)=PPP
IF (DPP.GE.0.005) GO TO 90
COEFM=UH/U0
VMID1=(1.-COEFM)/(1.+COEFM)
VMID3=1.+0.8*COEFM-0.45*COEFM**2
DX3=DISL3/FLOAT(NREG3)
MREG3=NREG3+1
SUMQ3=0.
DUGE=0.
R1(1)=R0
R2(1)=R0
FLWPL(1)=FMPL
FLWSD(1)=0.
AMPCP3=(AMAI*TIME+AMAIR*TIMER)/(TIME+TIMER)
DO 190 M=2,MREG3
  N=M-1
  X3=FLOAT(N)*DX3
  VMID2=0.27*X3
  VMID4=VMID1*(0.416+0.134*COEFM+0.021*VMID2*VMID1*VMID3/R0)
  R1(M)=R0-VMID2*VMID4
  VMIDA=0.021*VMID3/R0
  VMIDB=0.416+0.134*COEFM
  VMIDC=R1(M)-R0
  VMIDD=(-VMIDB+SQRT(VMIDB**2-4.*VMIDA*VMIDC))/2./VMIDA
  R2(M)=R1(M)+VMIDD
  NOM=0
  TBEGI=TEMP3(1)
  DENBEG=DENS0
  DR=(R2(M)-R1(M))/10.
  DUDL2(N)=2000.
  GEOL3=3.14159*R2(M)**2/DX3
  CONTINUE
  NOM=NOM+1
  IF (NOM.GT.200) THEN
    WRITE(*,*)'      Erro Stop      ITER.IN STANDOFF EXCEED 200'
    STOP
  ENDIF
  FLWPL(M)=3.14159*R1(M)**2*U0*DENBEG
  FLWSD(M)=0.
  ENERG(M)=FLWPL(M)*U0**2/2./1000.
  CALL INSEP(TABTEM,TABIPL,TBEGI,EBEGI)
  POWER=FLWPL(M)*EBEGI

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120

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DO 150 K=1,10
  RMID=FLOAT(K)*DR-DR/2.+R1(M)
  ATA=(R2(M)-RMID)/(R2(M)-R1(M))
  UMID=UO-(UO-UH)*(1.-ATA**1.5)**2
  TMID=TBEGI-(TBEGI-TAMBI)*(1.-ATA)
  FGFL=PAMBI/(1.+(1./ATA-1.)*FLMOL/SDMOL)
  PGSD=PAMBI-FGFL
  DENPL=FGFL*FLMOL/8315./TMID
  DENS=PGSD*SDMOL/8315./TMID
  VOLUM=2.*3.14159*RMID*DR*UMID
  FLWPL(M)=FLWPL(M)+VOLUM*DENPL
  FLWSD(M)=FLWSD(M)+VOLUM*DENS
  ENERG(M)=ENERG(M)+(DENPL+DENS)*VOLUM*UMID**2/2./1000.
  IF(TMID.GE.3000.) THEN
    CALL INSEP(TABTEM,TABIPL,TMID,ENTPL)
    CALL INSEP(TABTEM,TABISD,TMID,ENTSD)
  ELSE
    ENTPL=TABCPL(1)*TMID
    ENTSD=TABCS(1)*TMID
  ENDIF
  POWER=POWER+VOLUM*(DENPL*ENTPL+DENS*ENTSD)
150 CONTINUE
  POWRCP=(POWER+POW3(N))/2.
  PLCP=(FLWPL(M)+FLWPL(N))/2.
  SDCP=(FLWSD(M)+FLWSD(N))/2.
  CALL AVERT(PLCP,SDCP,POWRCP,TABTEM,TABIPL,TABISD,TCF)
  VRADI=3.14159*(R2(M)+R2(N))*2/4.*DX3
  QLOS3(N)=VRADI*4.*1.E7*(TCF/15000.)*16/(1.+(TCF/15000.)*16)
  CALL INSEP(TABTEM,TABMPL,TCF,PLMHO)
  CALL INSEP(TABTEM,TABMSD,TCF,SDMHO)
  CPMHO=((FLWPL(M)+FLWPL(N))*PLMHO+(FLWSD(M)+FLWSD(N))*SDMHO)/
$   (FLWPL(M)+FLWPL(N)+FLWSD(M)+FLWSD(N))
  OHM3=1./CPMHO/GEOL3
  DUDL3(N)=OHM3*AMPCP3/DX3
  DP3=OHM3*AMPCP3**2/1000.
  POW3(M)=POW3(N)+DP3-QLOS3(N)+(FLWSD(M)-FLWSD(N))*CPSD*TAMBI-
$   (ENERG(M)-ENERG(N))
  PMP=1.-POWER/POW3(M)
  IF(ABS(PMP).GE.0.010) THEN
    TBEGI=TBEGI*(1.+PMP/10.)
    DENBEG=PAMBI*FLMOL/8315./TBEGI
    UO=UO*FMPL/FLWPL(M)
    GO TO 120
  ENDIF
  WRITE(*,1390) N,NOM,PMP
  SUMQ3=SUMQ3+QLOS3(N)
  CALL AVERT(FLWPL(M),FLWSD(M),POWER,TABTEM,TABIPL,TABISD,
$   TEMP3(M))
  ENT3(M)=POW3(M)/(FLWPL(M)+FLWSD(M))
  DUGE=DUGE+DUDL3(N)*DX3
190 CONTINUE
  PAID=FLWSD(MREG3)*CPSD*TAMBI
C
C-----

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      GHK1=(AMAI*FIA3*TIME+AMAIR*(UR-FIA3)*TIMER)/(TIME+TIMER)/1000.
      GHK2=(AMAI*VA*TIME+AMAIR*VC*TIMER)/(TIME+TIMER)/1000.
C      GHK1=(AMAI*FIA3*TIME-AMAIR*FIA3*TIMER)/(TIME+TIMER)/1000.
C      GHK2=(AMAI*VA*TIME+AMAIR*(UR+VC)*TIMER)/(TIME+TIMER)/1000.
C-----
      POWER=POW3(MREG3)
      PLM=FMPL
      SDM=FLWSD(MREG3)
      POW4(1)=POWER+(1.-FSIA)*GHK2
      ENT4(1)=POW4(1)/(PLM+SDM)
      CALL AVERT(PLM,SDM,POW4(1),TABTEM,TABIPL,TABISD,TEMP4(1))
      ELOSS=ELOS*TEMP4(1)*AMAI*TIME/(TIME+TIMER)
      GHK12=GHK1+FSIA*GHK2
      CALL CONVO(R2(MREG3),ENT4(1),TEMP4(1),PLM,SDM,HSUR4,QCONV)
      SUMQ4=QCONV+ELOSS+GHK12
      WRITE(*,*)'  SUMQ4=',SUMQ4,'  VWELD=',VWELD
      CALL DEPTH(SUMQ4,DISL4,NREG4,ALFA,VWELD)
C=====
      STOP
C+++++
1000 FORMAT(/3X,'SYMBOL  UNIT      DESCRIPTION      ',
      $'      DATA'/)
1001 FORMAT(/3X,'MMM          Number of point in table      ',
      $I5)
1002 FORMAT(/3X,'TABTEM  K      Temperaeture table      ',
      $'      Table attached')
1003 FORMAT(/3X,'TABIPL  kJ/kg   Enthalpy of plasma gas      ',
      $'      Table attached')
1004 FORMAT(/3X,'TABCPPL  kJ/kg.K Specific heat of plasma gas      ',
      $'      Table attached')
1005 FORMAT(/3X,'TABKPL  kW/M.K   Thermal conductivity of plasma gas ',
      $'      Table attached')
1006 FORMAT(/3X,'TABISD  kJ/kg   Enthalpy of shield gas      ',
      $'      Table attached')
1007 FORMAT(/3X,'TABCSO  kJ/kg.K Specific heat of shield gas      ',
      $'      Table attached')
1008 FORMAT(/3X,'TABKSD  kW/M.K   Thermal conductivity of shield gas ',
      $'      Table attached')
1009 FORMAT(/3X,'TABMPL  MHO/M    Elictric conductivity of plasma gas',
      $'      Table attached')
1010 FORMAT(/3X,'TABMSD  MHO/M    Electric conductivity of shield gas',
      $'      Table attached')
1011 FORMAT(/3X,'TABNPL  kg/M.S   Viscosity of plasma gas      ',
      $'      Table attached')
1012 FORMAT(/3X,'TABNSD  kg/M.S   Viscosity of shield gas      ',
      $'      Table attached')
1013 FORMAT(/3X,'NREG1          Segment number between electrode      ',
      $ /3X,'          and orifice      ',I5)
1014 FORMAT(/3X,'NREG2          Segment number of orifice      ',
      $I5)
1015 FORMAT(/3X,'NREG3          Segment number of standoff      ',
      $I5)
1016 FORMAT(/3X,'NREG4          Segment number of workpiece      ',
      $I5)

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1017	FORMAT(/3X,'VA \$e12.5)	V	Anode potential drop	','
1018	FORMAT(/3X,'VC \$e12.5)	V	Cathode potential drop	','
1019	FORMAT(/3X,'FIA1 \$e12.5)	V	Electrode work function	','
1020	FORMAT(/3X,'FIA2 \$e12.5)	V	Orifice work function	','
1021	FORMAT(/3X,'FIA3 \$e12.5)	V	Workpiece work function	','
1022	FORMAT(/3X,'TIME \$e12.5)	mS	Time duration for straight polarity	','
1023	FORMAT(/3X,'TIMER \$e12.5)	mS	Time duration for reverse polarity	','
1024	FORMAT(/3X,'DISL1 \$/3X,'	M	Distance between electrode and orifice	','E12.5)
1025	FORMAT(/3X,'DISL2 \$e12.5)	M	Axial length of orifice	','
1026	FORMAT(/3X,'DISL3 \$e12.5)	M	Distance of standoff	','
1027	FORMAT(/3X,'DISL4 \$e12.5)	M	Thickness of workpiece	','
1028	FORMAT(/3X,'VVE \$e12.5)	Coulomb	Electron charge	','
1029	FORMAT(/3X,'VVK \$e12.5)	erg/K	Boltzman constant	','
1030	FORMAT(/3X,'APIL \$/3X,'	A	Pilot electric current in straight polarity	','e12.5)
1031	FORMAT(/3X,'APILR \$/3X,'	A	Pilot electric current in reverse polarity	','e12.5)
1032	FORMAT(/3X,'AMAI \$/3X,'	A	Main electric current in straight polarity	','e12.5)
1033	FORMAT(/3X,'AMAIR \$/3X,'	A	Main electric current in reverse polarity	','e12.5)
1034	FORMAT(/3X,'DNOZL \$e12.5)	M	Orifice diameter	','
1035	FORMAT(/3X,'DSHID \$e12.5)	M	External diameter of shield	','
1036	FORMAT(/3X,'VPL \$e12.5)	scfh	Plasma gas flow rate	','
1037	FORMAT(/3X,'VSD \$e12.5)	scfh	Shield gas flow rate	','
1038	FORMAT(/3X,'PLMOL \$e12.5)	kg/kmol	Molecular weight of plasma gas	','
1039	FORMAT(/3X,'SDMOL \$e12.5)	kg/kmol	Molecular weight of shield gas	','
1040	FORMAT(/3X,'UR \$e12.5)	V	Reverse polarity voltage rise	','
1041	FORMAT(/3X,'ITMAX \$I5)		Maximum number of iteration	','
1042	FORMAT(/3X,'DHMAX \$e12.5)		Maximum relative error of enthalpy	','
1043	FORMAT(/3X,'DTMAX \$e12.5)	K	Maximum error of temperature	','

1044	FORMAT(/3X,'TW1 \$e12.5)	K	Electrode wall temperature	'
1045	FORMAT(/3X,'TW2 \$e12.5)	K	Orifice wall temperature	'
1046	FORMAT(/3X,'TW4 \$e12.5)	K	Workpiece wall temperature	'
1047	FORMAT(/3X,'HSUR2 \$e12.5)	KJ/kg	Plasma enthalpy correponding to TW2'	'
1048	FORMAT(/3X,'HSUR4 \$e12.5)	KJ/kg	Jet enthalpy correponding to TW4	'
1049	FORMAT(/3X,'DXW \$e12.5)	M	Electrode length	'
1050	FORMAT(/3X,'TAMBI \$e12.5)	K	Enviromental temperature	'
1051	FORMAT(/3X,'DPOLAR \$e12.5)	M	Electrode diameter	'
1052	FORMAT(/3X,'AMDW \$e12.5)	KW/M.K	Thermal conductivity of electrode	'
1053	FORMAT(/3X,'PSIA \$/3x,')		Fraction power loss due to anode and cathode drop	' ,e12.5)
1054	FORMAT(/3X,'PAMBI \$e12.5)	N/M2	Environmental pressure	'
1055	FORMAT(/3X,'CPSD \$/3x,')	KJ/kg.K	Specific heat of shield gas with environmental temperature	' ,e12.5)
1056	FORMAT(/3X,'ALFA \$e12.5)	KW/M.K	Thermal diffusivity of workpiece	'
1057	FORMAT(/3X,'VWELD \$e12.5)	ipm	Welding speed	'
1058	FORMAT(/3X,'NX \$/3x,')		Number of computing nodal in X coordinate	' ,I5)
1059	FORMAT(/3X,'NY \$/3x,')		Number of computing nodal in Y coordinate	' ,I5)
1060	FORMAT(/3X,'X(1) \$/3x,')	M	Beginning position of computed nodal in X coordinate	' ,e12.5)
1061	FORMAT(/3X,'X(NX) \$/3x,')	M	Ending position of computed nodal in X coordinate	' ,e12.5)
1062	FORMAT(/3X,'Y(1) \$/3x,')	M	Beginning position of computed nodal in Y coordinate	' ,e12.5)
1063	FORMAT(/3X,'Y(NY) \$/3x,')	M	Ending position of computed nodal in Y coordinate	' ,e12.5)
1064	FORMAT(/3X,'TM \$e12.5)	K	Melting temperature of workpiece	'
1065	FORMAT(/3X,'TO \$e12.5)	K	Initial temperature of workpiece	'
1066	FORMAT(/3X,'THK \$e12.5)	KW/M.K	Thermal conductivity of workpiece	'
1067	FORMAT(/3X,'EPSL \$e12.5)		Emissivity of workpiece	'
1068	FORMAT(/3X,'DENS \$e12.5)	kg/M3	Density of workpiece	'
1069	FORMAT(/3X,'HFUSI \$e12.5)	KJ/kg	Melting latent heat of workpiece	'
C+++++				
1170	FORMAT(/2X,'POW1=',4E12.5,/7X,4E12.5)			

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1180 FORMAT(/2X,'ENT1=',4E12.5,/7X,4E12.5)
1190 FORMAT(/2X,'QLOS1=',4E12.5,/7X,4E12.5)
1200 FORMAT(/2X,'TEMP1=',4E12.5,/7X,4E12.5)
1210 FORMAT(/2X,'TOTAL LOSS IN GAP 1',E12.5,2X,'DUBC(V)',F6.2)
1220 FORMAT(/2X,'DUDL1',4E12.5,/7X,4E12.5)
1300 FORMAT(/2X,'DUDL2',4E12.5,/7X,4E12.5)
1310 FORMAT(/5X,'TOTAL LOSS IN NOZZLE =',E12.5,2X,'DUCG(V)',F6.2)
1250 FORMAT(/5X,'POW2=',4E12.5/10X,4E12.5)
1260 FORMAT(/5X,'ENT2=',4E12.5/10X,4E12.5)
1270 FORMAT(/4X,'QLOS2=',4E12.5/10X,4E12.5)
1280 FORMAT(/2X,'TEMP2',4E12.5,/7X,4E12.5)
1290 FORMAT(/2X,'ELOS2',4E12.5,/7X,4E12.5)
1320 FORMAT(/5X,'STANDOFF COMPUTATION')
1230 FORMAT(/5X,'NOZZLE COMPUTATION')
1240 FORMAT(/5X,'NN2.GT.100')
1340 FORMAT(/5X,'UH,UO,COEFM',3E12.5)
1350 FORMAT(/2X,'LINE 285 TBEGI',E12.4)
1370 FORMAT(/1X,'ATA,TBEGI,TAMBI,TMID',4E11.4)
1360 FORMAT(1X,'M,R1,R2,DR,RMID,ATA',I2,2E12.5,/5X,3E12.5)
1380 FORMAT(/2X,'IN MAIN,NOM,MAR,MHE,POWER',I4,2X,3E10.3)
1390 FORMAT(/2X,'ITER.IN STANDOFF,SEG.=',I2,2X,'NOM=',I4,
$      2X,'PMP=',F10.6)
1510 FORMAT(/2X,'DUDL3',4E12.5,/7X,4E12.5)
1450 FORMAT(/2X,'TOTAL LOSS IN STANDOFF =',E12.5,2X,'DUGE(V)',F6.2)
1410 FORMAT(/5X,'POW3=',4E12.5,/10X,4E12.5)
1430 FORMAT(/4X,'QLOS3=',4E12.5,/10X,4E12.5)
1440 FORMAT(/4X,'TEMP3=',4E12.5,/10X,4E12.5)
1460 FORMAT(/5X,'R1(m)=' ,4F10.8,/11X,4F10.8)
1470 FORMAT(/5X,'R2(m)=' ,4F10.8,/11X,4F10.8)
1480 FORMAT(/5X,'FLWPL=' ,4E12.5,/11X,4E12.5)
1490 FORMAT(/5X,'FLWSD=' ,4E12.5,/11X,4E12.5)
1500 FORMAT(/5X,'ENERG=' ,4E12.5,/11X,4E12.5)
1520 FORMAT(/5X,'POWER AID FROM SHIELD, PAID(kW)=' ,E12.5)
1530 FORMAT(/2X,'VELOC.,TEMP.IN CORE AT LAST',2E12.5)
1540 FORMAT(/5X,'T OF BOUNDARY, TBOUND=' ,E12.5)
1550 FORMAT(/5X,'CONVECTIVE LOSS OF JET (kW)',E12.5)
1555 FORMAT(/10X,'WORKPIECE COMPUTATION')
1560 FORMAT(/2X,'XSOUR',2X,5F8.6)
1570 FORMAT(/5X,'RADIUS OF KEYHOLE (m)=' ,E12.5)
1580 FORMAT(/2X,'AREA(m**2)',4E12.5,/12X,4E12.5)
1590 FORMAT(/4X,'PLM,SDM,TEMP4(1)',3E14.5)
1600 FORMAT(/5X,'IMPINGE LOSS (kW)',F8.5)
1660 FORMAT(/2X,'QSEGM=' ,4E12.5,/8X,4E12.5)
1680 FORMAT(/5X,'TOTAL LOSS IN WORKPIECE =' ,E12.5)
1610 FORMAT(/2X,'POW4=' ,4E12.5,/7X,4E12.5)
1620 FORMAT(/2X,'ENT4=' ,4E12.5,/7X,4E12.5)
1630 FORMAT(/2X,'TEMP4=' ,4E12.5,/8X,4E12.5)
1640 FORMAT(/2X,'QLOS4=' ,4E12.5,/8X,4E12.5)
1650 FORMAT(/2X,'ELOS4=' ,4E12.5,/8X,4E12.5)
1670 FORMAT(/2X,'QSOUR=' ,4E12.5,/8X,4E12.5)
1690 FORMAT(5X,'TOTAL POWER INCLUDING HELIUM, PTOTIN=' ,E12.5,/
$      5X,'TOTAL POWER FROM LOSS, PTOTOU=' ,E12.5)
1700 FORMAT(/2X,'POLARITY CONDUCT. LOSS AND PERCENT.',2E12.5)
1710 FORMAT(/2X,'GAP LOSS AND PERCENTAGE',2E12.5)

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1720 FORMAT(/2X,'NOZZLE LOSS AND PERCENTAGE',2E12.5)
1730 FORMAT(/2X,'RADIAT.IN STANDOFF AND PERCENTAGE',2E12.5)
1740 FORMAT(/2X,'CONVEC.IN STANDOFF AND PERCENTAGE',2E12.5)
1750 FORMAT(/2X,'WORKPIECE LOSS AND PERCENTAGE',2E12.5)
1760 FORMAT(/2X,'DISCHARGE LOSS AND PERCENTAGE',2E12.5)
1770 FORMAT(/5X,'SUM. PERCENTAGE',F8.5)
1780 FORMAT(/5X,'AMPCP1,2,3',3E12.5)
1790 FORMAT(/5X,'DUBE,DUAF,DUAFR',3E12.5)
1800 FORMAT(/4X,'DUFF=',E12.4,4X,'DUPR=',E12.4)
      END
C
C-----
C
      SUBROUTINE AVERT(FLOPL,FLOSD,PSUM,TABT,TABPL,TABSD,TVERA)
      DIMENSION TABT(20),TABPL(20),TABSD(20)
      COMMON MMM
C      WRITE(7,3000) FLOPL,FLOSD,PSUM
      NN=0
      TVERA=10000.
10  CONTINUE
      NN=NN+1
      IF(NN.GT.200) THEN
        WRITE(*,*)' Erro Stop      ITER.EXCEED 200 IN AVERT, THEN STOP'
        STOP
      ENDIF
      CALL INSEP(TABT,TABPL,TVERA,EPL)
      CALL INSEP(TABT,TABSD,TVERA,ESD)
      PCOMP=FLOPL*EPL+FLOSD*ESD
      DPOWR=1.-PCOMP/PSUM
      IF(ABS(DPOWR).GE.0.010) THEN
        TVERA=TVERA*(1.+DPOWR/10.)
C      WRITE(*,3020) NN,DPOWR
        GO TO 10
      ENDIF
C      WRITE(7,3030) NN,DPOWR,TVERA
      RETURN
3000 FORMAT(/2X,'IN AVERT,MPL,MSD,PSUM',3E11.4)
3020 FORMAT(2X,'NN=',I3,2X,'DPOWR=',E12.5)
3030 FORMAT(/2X,'SUB.AVERT, NN,DPOWR,TVERA',I4,2E14.5)
      END
C
C-----
C
      SUBROUTINE INSEP(A,B,C,D)
      DIMENSION A(26),B(26)
      COMMON MMM
      IF(C.LT.A(1).OR.C.GT.A(MMM)) THEN
        WRITE(*,*)' Erro Stop      INDEP. IS BEYOND SCOPE'
        WRITE(*,*)' C=',C,'A(1)=' ,A(1),'A(MMM)=' ,A(MMM)
        STOP
      ENDIF
      DO 30 K=2,MMM
        IF((C.LE.A(K).AND.C.GE.A(K-1)).OR.
$      (C.GE.A(K).AND.C.LE.A(K-1))) THEN

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      D=B(K-1)+(B(K)-B(K-1))/(A(K)-A(K-1))*(C-A(K-1))
C      WRITE(*,4010) C,D
      GO TO 40
      ENDIF
30      CONTINUE
C      WRITE(*,4020)
40      CONTINUE
      RETURN
4020 FORMAT(/5X,'WRITE FROM FORMAT 31 IN SUB. INSEP')
4010 FORMAT(/5X,'INDEP. C=',E12.4,5X,'DEPEND. D=',E12.4)

      END

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```

C
C-----
C
SUBROUTINE DEPTH(QORIG,H,NHH,ALPHA,VWELD)
  DIMENSION Z(20),ZZ(34),HH(15),TEMP(25,10,10)
  DIMENSION XMOLT(50),YMOLT(50),ZMOLT(50),ZMY(50),DZ(15),
$  DHZ(15),XMOLTO(50),ZMOLTO(50),TEMPO(10,25,10,10)
  common/dat10/NX,NY,X(25),Y(15),TM,TO,THK,EPSL,DENS,HFUSI
  OPEN(8,FILE='C:WEL.OU1')
  OPEN(9,FILE='C:WEL.OU2')
  OPEN(10,FILE='C:WEL.OU3')
  IF(NX.GT.1)THEN
    DO 1 I=1,NX
      X(I)=X(1)+FLOAT(I-1)*(X(NX)-X(1))/FLOAT(NX-1)
1    CONTINUE
  ENDIF
  IF(NY.GT.1)THEN
    DO 5 J=1,NY
      Y(J)=Y(1)+FLOAT(J-1)*(Y(NY)-Y(1))/FLOAT(NY-1)
5    CONTINUE
  ENDIF
  NZ=NHH
  IF(NZ.GT.1)THEN
    DO 6 K=1,NZ
      Z(K)=FLOAT(K-1)*H/FLOAT(NZ-1)
6    CONTINUE
  ENDIF
  NOM=1
  DO 10 L=1,NHH
    HH(L)=FLOAT(L-1)*H/FLOAT(NHH-1)
10 CONTINUE

```

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C-----
  TMDLT=TM-TO
  V=VWELD*0.0254/60.
  V2A=-V/(2.*ALPHA)
  QS=QORIG
  Q4K=1./(4.*3.14159*THK)

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C-----
  DO 70 N=1,NHH
    HHH=HH(N)
    ZZ(1)=-16.*H-HHH
    ZZ(2)=-16.*H+HHH

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      DO 20 K=3,34,2
        ZZ(K)=ZZ(K-2)+2.*H
        ZZ(K+1)=ZZ(K-1)+2.*H
20    CONTINUE
      DO 60 K=1,NX
        DO 50 L=1,NY
          DO 40 J=1,NZ
            DO 30 M=1,34
              ZZZ=Z(J)-ZZ(M)
              XXX=X(K)
              YYY=Y(L)
              R=SQRT(XXX**2+YYY**2+ZZZ**2)
              RX=R+XXX
              IF(RX.GT.10.) GO TO 60
              RX=V2A*RX
              EXPAN=EXP(RX)
              TEMPO(N,K,L,J)=TEMPO(N,K,L,J)+Q4K*EXPAN/R
30          CONTINUE
40        CONTINUE
50      CONTINUE
60    CONTINUE
70  CONTINUE
      QM=0.0
C-----
110 CONTINUE
      DO 150 K=1,NZ
        DO 140 J=1,NY
          DO 130 I=1,NX
            TEMP(I,J,K)=0.0
130    CONTINUE
140    CONTINUE
150 CONTINUE
      DO 190 I=1,NX
        DO 180 J=1,NY
          DO 170 K=1,NZ
            IF(NOM.GT.1) THEN
              DO 160 N=1,NOH
                TEMP(I,J,K)=TEMP(I,J,K)+QS/ZMAXO*DHZ(N)*TEMPO(N,I,J,K)
160          CONTINUE
            ELSE
              TEMP(I,J,K)=QS*TEMPO(1,I,J,K)
            ENDIF
170        CONTINUE
180      CONTINUE
190 CONTINUE
      ZMAX=0.0
      M1=0
      M2=0
      M3=0
      DO 220 K=1,NZ
        YMOLT(K)=0.0
        DO 210 I=1,NX-1
          IF(TMOLT.GT.TEMP(I,1,K).AND.TMOLT.LE.TEMP(I+1,1,K)) THEN
            XM1=X(I)+(X(I+1)-X(I))*(TMOLT-TEMP(I,1,K))/

```

```

$          (TEMP(I+1,1,K)-TEMP(I,1,K))
          M1=M1+1
          XMOLT(M1)=-1000.*XM1
          ZMOLT(M1)=1000.*Z(K)
          ZMAX=AMAX1(ZMAX,Z(K))
          I1=I+1
        ENDIF
        IF(TMOLT.LE.TEMP(I,1,K).AND.TMOLT.GT.TEMP(I+1,1,K)) THEN
$          XM2=X(I)+(X(I+1)-X(I))*(TMOLT-TEMP(I,1,K))/(
          (TEMP(I+1,1,K)-TEMP(I,1,K))
$          M2=M2+1
          XMOLTO(M2)=-1000.*XM2
          ZMOLTO(M2)=1000.*Z(K)
          ZMAX=AMAX1(ZMAX,Z(K))
          I2=I
        ENDIF
        DO 200 J=1,NY-1
$          IF((TMOLT.GE.TEMP(I,J,K).AND.TMOLT.LT.TEMP(I,J+1,K)).OR.
          (TMOLT.LE.TEMP(I,J,K).AND.TMOLT.GT.TEMP(I,J+1,K))) THEN
$          YM=Y(J)+(Y(J+1)-Y(J))/(TEMP(I,J+1,K)-TEMP(I,J,K))*
          (TMOLT-TEMP(I,J,K))
          IF(YMOLT(K).LT.1000.*YM) JY=J
          YMOLT(K)=AMAX1(YMOLT(K),1000.0*YM)
          ZMY(K)=1000.0*Z(K)
          M3=K
        ENDIF
200      CONTINUE
210      CONTINUE
220      CONTINUE
C-----
        WRITE(*,*)' M1=',M1,' I1=',I1,' I2=',I2
        IF(M1.LT.NZ) THEN
          DO 240 I=I1,I2
            DO 230 IM=2,NZ
              IF(TMOLT.LE.TEMP(I,1,IM-1).AND.TMOLT.GT.TEMP(I,1,IM)) THEN
$                ZM1=Z(IM-1)+(Z(IM)-Z(IM-1))*(TMOLT-TEMP(I,1,IM-1))/
                (TEMP(I,1,IM)-TEMP(I,1,IM-1))
$                M1=M1+1
                XMOLT(M1)=-1000.*X(I)
                ZMOLT(M1)=1000.0*ZM1
                ZMAX=AMAX1(ZM1,ZMAX)
                GO TO 240
              ENDIF
230          CONTINUE
240          CONTINUE
            ENDIF
C-----
            DZ(1)=0.5*(HH(2)-HH(1))
            DZ(M2)=ZMAX-0.5*(HH(M2)+HH(M2-1))
C          WRITE(*,*)' DZ(1)=' ,DZ(1), ' DZ(M2)=' ,DZ(M2)
            DO 248 L=2,M2-1
              DZ(L)=0.5*(HH(L)+HH(L+1))-0.5*(HH(L-1)+HH(L))
C          WRITE(*,*)' DZ(L)=' ,DZ(L)
248          CONTINUE

```

```

QM=0.0
DO 250 K=1,M2
  QM=QM+2.*V*DZ(K)*YMOLT(K)*HFUSI*DENS*0.001
250 CONTINUE
QSQS=QORIG-QM
WRITE(*,*)'QSQS=',QSQS,'  QORIG=',QORIG,'  QM=',QM
DQS=1.-QSQS/QS
IF (ABS(DQS).GT.0.05) THEN
  QS=QS*(1.-0.2*DQS)
  GO TO 110
ENDIF
IF (NOM.EQ.1) THEN
  NOM=NOM+1
  NOH=M2
  ZMAXO=ZMAX
  DO 252 I=1,NOH
    DHZ(I)=DZ(I)
252 CONTINUE
  GO TO 110
ENDIF

```

C-----

```

WRITE(*,*)'      ZMAX=',ZMAX,'      ZMAXO=',ZMAXO
WRITE(*,*)'      ZMAX/H=',ZMAX/H
IF ((1.0-ZMAX/H).LT.1.E-6) THEN
  WRITE(*,*)'      A keyhole has been formed !!!'
ELSE
  WRITE(*,*)'      No keyhole !!!'
ENDIF
300 CONTINUE
MM=M1+M2
WRITE(8,*)'      MM=',MM
DO 310 I=1,M2
  XMOLT(I+M1)=XMOLTO(M2-I+1)
  ZMOLT(I+M1)=ZMOLTO(M2-I+1)
310 CONTINUE
DO 320 J=1,MM
  WRITE(8,*) XMOLT(J),ZMOLT(J)
320 CONTINUE

```

C-----

```

WRITE(*,*)'      M3=',M3,'      JY=',JY
IF (M3.LT.NZ) THEN
  DO 333 J=JY,1,-1
    ZM0=0.0
    DO 332 I=1,NX
      DO 331 K=2,NZ
        IF ((TMOLT.LE.TEMP(I,J,K-1).AND.TMOLT.GT.TEMP(I,J,K)).OR.
$          (TMOLT.GE.TEMP(I,J,K-1).AND.TMOLT.LT.TEMP(I,J,K))) THEN
          ZM3=Z(K-1)+(Z(K)-Z(K-1))*(TMOLT-TEMP(I,J,K-1))/
$          (TEMP(I,J,K)-TEMP(I,J,K-1))
          ZM0=AMAX1(ZM0,ZM3)
        GO TO 332
      ENDIF
    CONTINUE
331 CONTINUE
332 CONTINUE

```

```

        M3=M3+1
        YMOLT(M3)=1000.0*Y(J)
        ZMY(M3)=1000.0*ZMO
C        WRITE(*,*) ' J=',J,' YM=',YMOLT(M3),' ZM=',ZMY(M3)
333    CONTINUE
    ENDIF
    DO 335 J=1,M3
        WRITE(9,*) YMOLT(J),ZMY(J)
335    CONTINUE
C-----
    IF((1.0-ZMAX/H).LT.1.E-6) THEN
        WRITE(10,3000) QSQS,QORIG,QM
    ELSE
        WRITE(10,3005) QSQS,QORIG,QM,100*ZMAX/H
    ENDIF
    RETURN
3000    FORMAT(/3X,'      QSQS      QORIG      QM      Keyhole(Y/N)?',
$        //3X,3F10.3,'      Y')
3005    FORMAT(/3X,'      QSQS      QORIG      QM      Keyhole(Y/N)?',
$        //3X,3F10.3,'      N',F6.1,' %')
    END
C-----
C
C
SUBROUTINE CONVO(RJ,HJ,TJ,PLM,SDM,HW,PCONV)
COMMON MMM
COMMON TABTEM(20),TABIFL(20),TABCPL(20),TABKPL(20),TABISD(20)
COMMON ITMAX,DHMAX,DTMAX
COMMON TAMBI,DNOZL,FMPL
COMMON TABCSD(20),TABKSD(20),TABNPL(20),TABNSD(20)
COMMON TW4,MREG4,NREG4
NOM=0
200    CONTINUE
    NOM=NOM+1
    IF(NOM.GT.ITMAX) THEN
        WRITE(*,*) ' Erro Stop      ITERATIONS EXCEED ITMAX IN CONV4'
        STOP
    ENDIF
    VJM=PLM+SDM
    write(*,*) ' TJ=',TJ
    HM=.5*(HJ+HW)
    POW=VJM*HM
    CALL AVERT(PLM,SDM,POW,TABTEM,TABIFL,TABISD,TM)
    CALL INSEP(TABTEM,TABCPL,TJ,PLCP)
    CALL INSEP(TABTEM,TABCSD,TJ,SDCP)
    CF=(PLCP*PLM+SDCP*SDM)/VJM
    CALL INSEP(TABTEM,TABCPL,TM,PLCPM)
    CALL INSEP(TABTEM,TABCSD,TM,SDCPM)
    CPM=(PLCPM*PLM+SDCPM*SDM)/VJM
    CALL INSEP(TABTEM,TABKPL,TJ,PLAMD)
    CALL INSEP(TABTEM,TABKSD,TJ,SDAMD)
    AMD=(PLAMD*PLM+SDAMD*SDM)/VJM
    CALL INSEP(TABTEM,TABNPL,TJ,PLN)
    CALL INSEP(TABTEM,TABNSD,TJ,SDN)

```

```
VISC=(FLN*FLM+SDN*SDM)/VJM  
REN=2.*VJM/RJ/VISC/3.14159  
FRA=CF*VISC/AMD  
VNU=0.78*REN**0.5*FRA**0.33  
ALFAJ=.5*VNU*AMD/RJ  
PCONV=3.14159*RJ*RJ*ALFAJ*(HJ-Hw)/CFM  
RETURN  
END
```

Appendix C

*** INPUT DATA FOR ALUMINUM ***

SYMBOL	UNIT	DESCRIPTION	DATA
MMM		Number of point in table	18
TABTEM	K	Temperaeture table	Table attached
TABIPL	KJ/kg	Enthalpy of plasma gas	Table attached
TABCPL	KJ/kg.K	Specific heat of plasma gas	Table attached
TABKPL	KW/M.K	Thermal conductivity of plasma gas	Table attached
TABISD	KJ/kg	Enthalpy of shield gas	Table attached
TABCSO	KJ/kg.K	Specific heat of shield gas	Table attached
TABKSD	KW/M.K	Thermal conductivity of shield gas	Table attached
TABMPL	MHO/M	Electric conductivity of plasma gas	Table attached
TABMSD	MHO/M	Electric conductivity of shield gas	Table attached
TABNPL	kg/M.S	Viscosity of plasma gas	Table attached
TABNSD	kg/M.S	Viscosity of shield gas	Table attached
NREG1		Segment number between electrode and orifice	1
NREG2		Segment number of orifice	1
NREG3		Segment number of standoff	1
NREG4		Segment number of workpiece	7
VA	V	Anode potential drop	.30000E+01
VC	V	Cathode potential drop	.45000E+01
FIA1	V	Electrode work function	.30000E+01
FIA2	V	Orifice work function	.45000E+01
FIA3	V	Workpiece work function	.38000E+01
TIME	mS	Time duration for straight polarity	Variable
TIMER	mS	Time duration for reverse polarity	Variable
DISL1	M	Distance between electrode and orifice	Variable
DISL2	M	Axial length of orifice	Variable

DISL3	M	Distance of standoff	Variable
DISL4	M	Thickness of workpiece	.63500E-02
VVE	Coulomb	Electron charge	.16020E-18
VVK	erg/K	Boltzman constant	.13800E-15
APIL	A	Pilot electric current in straight polarity	Variable
APILR	A	Pilot electric current in reverse polarity	Variable
AMAI	A	Main electric current in straight polarity	Variable
AMAIR	A	Main electric current in reverse polarity	Variable
DNOZL	M	Orifice diameter	.31800E-02
DSHID	M	External diameter of shield	.18000E-01
VPL	scfh	Plasma gas flow rate	Variable
VSD	scfh	Shield gas flow rate	Variable
PLMOL	kg/kmol	Molecular weight of plasma gas	.39950E+02
SDMOL	kg/kmol	Molecular weight of shield gas	.40030E+01
UR	V	Reverse polarity voltage rise	.11480E+02
ITMAX		Maximum number of iteration	100
DHMAX		Maximum relative error of enthalpy	.50000E-02
DTMAX	K	Maximum error of temperature	.50000E+00
TW1	K	Electrode wall temperature	.25000E+04
TW2	K	Orifice wall temperature	.40000E+03
TW4	K	Workpiece wall temperature	.91600E+03
HSUR2	kJ/kg	Plasma enthalpy corresponding to TW2	.20800E+03
HSUR4	kJ/kg	Jet enthalpy corresponding to TW4	.47600E+03
DXW	M	Electrode length	Variable
TAMBI	K	Enviromental temperature	.29800E+03
DPOLAR	M	Electrode diameter	.39600E-02
AMDW	kW/M.K	Thermal conductivity of electrode	.23500E-01

PSIA		Fraction power loss due to anode and cathode drop	.20000E+00
PAMBI	N/M2	Environmental pressure	.10132E+06
CPSD	KJ/kg.K	Specific heat of shield gas with environmental temperature	.51930E+01
ALFA	M2/S	Thermal diffusivity of workpiece	.52410E-04
VWELD	ipm	Welding speed	.91000E+01
NX		Number of computing nodal in X coordinate	15
NY		Number of computing nodal in Y coordinate	7
X(1)	M	Beginning position of computed nodal in X coordinate	-.70000E-02
X(NX)	M	Ending position of computed nodal in X coordinate	.70000E-02
Y(1)	M	Beginning position of computed nodal in Y coordinate	.00000E+00
Y(NY)	M	Ending position of computed nodal in Y coordinate	.70000E-02
TM	K	Melting temperature of workpiece	.91600E+03
TO	K	Initial temperature of workpiece	.29800E+03
THK	KW/M.K	Thermal conductivity of workpiece	.12000E+00
EPSL		Emissivity of workpiece	.10000E+00
DENS	kg/M3	Density of workpiece	.26500E+04
HFUSI	KJ/kg	Melting latent heat of workpiece	.38700E+03

Attached Table for Aluminum

Temperature (K)

.3000E+04	.6000E+04	.7000E+04	.8000E+04	.9000E+04
.1000E+05	.1100E+05	.1200E+05	.1300E+05	.1400E+05
.1500E+05	.1600E+05	.1700E+05	.1800E+05	.1900E+05
.2000E+05	.2200E+05	.2400E+05		

Enthalpy of Plasma Gas (kJ/kg) (ARGON)

.1562E+04	.3138E+04	.3652E+04	.4229E+04	.4966E+04
.6125E+04	.8164E+04	.1183E+05	.1778E+05	.2613E+05
.3553E+05	.4384E+05	.4957E+05	.5372E+05	.5661E+05
.5945E+05	.6862E+05	.8667E+05		

Specific Heat of Plasma Gas (kJ/kg.K) (ARGON)

.5192E+00	.5192E+00	.5401E+00	.6280E+00	.8918E+00
.1511E+01	.2721E+01	.4677E+01	.7243E+01	.9253E+01
.9253E+01	.7159E+01	.4731E+01	.3211E+01	.2734E+01
.3136E+01	.6573E+01	.1122E+02		

Thermal Conductivity of Plasma Gas (kW/M.K) (ARGON)

.1440E-03	.1660E-03	.2030E-03	.2720E-03	.4020E-03
.6250E-03	.9610E-03	.1403E-02	.1901E-02	.2297E-02
.2417E-02	.2315E-02	.2252E-02	.2294E-02	.2436E-02
.2644E-02	.3094E-02	.3542E-02		

Enthalpy of Shield Gas (kJ/kg) (HELIUM)

.2597E+05	.3116E+05	.3635E+05	.4154E+05	.4674E+05
.5194E+05	.5728E+05	.6295E+05	.6935E+05	.7718E+05
.8773E+05	.1027E+06	.1245E+06	.1562E+06	.2011E+06
.2624E+06	.4322E+06	.6198E+06		

Specific Heat of Shield Gas (kJ/kg.K) (HELIUM)

.5193E+01	.5193E+01	.5193E+01	.5193E+01	.5229E+01
.5266E+01	.5453E+01	.5924E+01	.6952E+01	.8913E+01
.1232E+02	.1777E+02	.2588E+02	.3720E+02	.5183E+02
.6880E+02	.9526E+02	.8384E+02		

Thermal Conductivity of Shield Gas (kW/M.K) (HELIUM)

.9100E-03	.9300E-03	.9500E-03	.1028E-02	.1164E-02
.1300E-02	.1620E-02	.1940E-02	.3060E-02	.4980E-02
.6900E-02	.1174E-01	.1658E-01	.2260E-01	.2980E-01
.3700E-01	.3860E-01	.3420E-01		

Electric Conductivity of Plasma Gas (MHO/M) (ARGON)

.1030E+02	.1010E+03	.3610E+03	.9230E+03	.1770E+04
.2730E+04	.3730E+04	.4740E+04	.5740E+04	.6670E+04
.7490E+04	.8200E+04	.8810E+04	.9730E+04	.9880E+04
.1040E+05	.1080E+05	.1050E+05		

Electric Conductivity of Shield Gas (MHO/M) (HELIUM)

.4285E-01	.7852E+00	.2070E+01	.5458E+01	.1439E+02
.3793E+02	.1000E+03	.2512E+03	.6310E+03	.1261E+04
.2002E+04	.2887E+04	.3648E+04	.4368E+04	.5137E+04
.5720E+04	.7093E+04	.8794E+04		

Viscosity of Plasma Gas (kg/M.S) (ARGON)

.1290E-03	.2090E-03	.2330E-03	.2560E-03	.2770E-03
.2900E-03	.2840E-03	.2450E-03	.1810E-03	.1170E-03
.7110E-04	.4460E-04	.3150E-04	.2570E-04	.2380E-04
.2300E-04	.2100E-04	.1560E-04		

Viscosity of Shield Gas (kg/M.S) (HELIUM)

.1000E-03	.1400E-03	.1550E-03	.1620E-03	.1700E-03
.1840E-03	.1920E-03	.2000E-03	.2060E-03	.2120E-03
.2180E-03	.2200E-03	.2180E-03	.2110E-03	.2050E-03
.1950E-03	.1600E-03	.1000E-03		

Appendix D: Input Data in Program (I) (Mild Steel)

SYMBOL	DESCRIPTION	DATA
MMM	Number of point in table	26
TABTEM	Temperature table	Table Attached
TABIPL	Enthalpy of plasma gas (Argon)	Table Attached
TABCPL	Specific heat of plasma gas (Argon)	Table Attached
TABKPL	Thermal conductivity of plasma gas (Argon)	Table Attached
TABISD	Enthalpy of shield gas (Argon)	Table Attached
TABCSO	Specific heat of shield gas (Argon)	Table Attached
TABKSD	Thermal conductivity of shield gas (Argon)	Table Attached
TABMPL	Electric conductivity of plasma gas (Argon)	Table Attached
TABMSD	Electric conductivity of shield gas (Argon)	Table Attached
NREG1	Segment number between electrode and orifice	1-5
NREG2	Segment number of orifice	1-5
NREG3	Segment number of standoff	1-5
NREG4	Segment number of workpiece	1-5
VA	Anode potential drop	3V
VC	Cathode potential drop	4.5V
FIA1	Electrode work function	2.6V
FIA2	Orifice work function	4.5V
FIA3	Workpiece work function	4.2V
TIME	Time duration for straight polarity	19ms
TIMER	Time duration for reverse polarity	4ms
DISL1	Distance between electrode and orifice	1.1938mm

D: Input Data in Program (II)

SYMBOL	DESCRIPTION	DATA
DISL2	Vertical length of orifice	3.175mm
DISL3	Distance of standoff	Variable
DISL4	Thickness of workpiece	6.35mm
VVE	Electron charge	1.602×10^{-19} coulomb
VVK	Boltzman constant	1.38×10^{-16} erg/k
APIL	Pilot electric current in straight polarity	Variable
APILR	Pilot electric current in reverse polarity	Variable
AMAI	Main electric current in straight polarity	Variable
AMAIR	Main electric current in reverse polarity	Variable
DNOZL	Orifice diameter	3.175mm
DSHID	External diameter of shield gas	18mm
VPL	Plasma gas flow rate	Variable
VSD	Shield gas flow rate	Variable
PLMOL	Molecular weight of plasma gas (Argon)	39.5 kg/kmol
SDMOL	Molecular weight of shield gas (Argon)	39.5 kg/kmol
URA	Constant in computation of reverse polarity rise	12.2
URB	Constant in computation of reverse polarity rise	16
ITMAX	Maximum number of iteration	100
DHMAX	Maximum relative error of enthalpy	0.005
DTMAX	Maximum error of temperature	0.5K
TWI	Electrode wall temperature	2500K
TW2	Orifice wall temperature	353K
TW4	Workpiece wall temperature	1727K

D : Input Data in Program (III)

SYMBOL	DESCRIPTION	DATA
HSUR2	Plasma enthalpy corresponding to TW2 (Argon)	190 kJ/kg
HSUR4	Jet enthalpy corresponding to TW4 (Argon)	900 kJ/kg
DXW	Electrode length	68.072mm
TAMBI	Environmental temperature	298K
DPOLAR	Electrode diameter	3.9624mm
AMDW	Thermal conductivity of electrode	23.5 W/m.K
PSIA	Fraction of power loss due to anode and cathode drops	0.
PAMBI	Environmental pressure	101320 N/m ²
CPSD	Specific heat of shield gas with environmental temperature (Argon)	0.5205 kJ/kg.K
NX	Number of computing nodal in X coordinate	10
NY	Number of computing nodal in Y coordinate	20
NZ	Number of computing nodal in Z coordinate	2
NHH	Number of heat source	1
X	Position of computed nodal in X coordinate	Variable
Y	Position of computed nodal in Y coordinate	Variable
Z	Position of computed nodal in Z coordinate	0., 6.35mm
HH	Position of heat source	3.175mm
H	Workpiece thickness	6.35mm
V	Welding speed	Variable
ALPHA	Thermal diffusivity of workpiece	$5.45 \times 10^{-6} \text{ m}^2/\text{s}$

D : Input Data in Program (IV)

[illegible]

Appendix D: Attached Table for Mild Steel (I)

51,99L

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THERMAL CONDUCTIVITY OF PLASMA GAS (kW/m.K) (ARGON)

.1013E-03	.1057E-03	.1174E-03	.1432E-03	.1933E-03
.2820E-03	.4279E-03	.6550E-03	.9916E-03	.1463E-02
.2050E-02	.2563E-02	.2675E-02	.2480E-02	.2348E-02
.2374E-02	.2507E-02	.2697E-02	.3148E-02	.3632E-02
.4126E-02	.4623E-02	.5120E-02	.5618E-02	.6116E-02
.6365E-02				

ENTHALPY OF SHIELD GAS (kJ/kg) (ARGON)

.1562E+04	.2082E+04	.2603E+04	.3125E+04	.3654E+04
.4215E+04	.4894E+04	.5931E+04	.7892E+04	.1173E+05
.1823E+05	.2680E+05	.3549E+05	.4287E+05	.4874E+05
.5351E+05	.5762E+05	.6143E+05	.6988E+05	.8590E+05
.1112E+06	.1298E+06	.1441E+06	.1609E+06	.1831E+06
.1956E+06				

SPECIFIC HEAT OF SHIELD GAS (kJ/kg.K) (ARGON)

.5205E+00	.5205E+00	.5209E+00	.5238E+00	.5382E+00
.5972E+00	.7971E+00	.1370E+01	.2719E+01	.5115E+01
.7791E+01	.8973E+01	.8163E+01	.6531E+01	.5236E+01
.4370E+01	.3901E+01	.3771E+01	.5252E+01	.1139E+02
.1173E+02	.7515E+01	.7329E+01	.9700E+01	.1229E+02
.1265E+02				

D: Attached Table for Mild Steel (II)

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THERMAL CONDUCTIVITY OF PLASMA GAS (kW/m.K) (ARGON)					
.1013E-03	.1057E-03	.1174E-03	.1432E-03	.1933E-03	
.2320E-03	.4279E-03	.6550E-03	.9916E-03	.1463E-02	
.2050E-02	.2563E-02	.2675E-02	.2480E-02	.2348E-02	
.2374E-02	.2507E-02	.2697E-02	.3148E-02	.3632E-02	
.4126E-02	.4623E-02	.5120E-02	.5618E-02	.6116E-02	
.6365E-02					

ENTHALPY OF SHIELD GAS (kJ/kg) (ARGON)					
.1562E+04	.2082E+04	.2603E+04	.3125E+04	.3654E+04	
.4215E+04	.4394E+04	.5931E+04	.7892E+04	.1173E+05	
.1823E+05	.2680E+05	.3549E+05	.4287E+05	.4874E+05	
.5351E+05	.5762E+05	.6143E+05	.6988E+05	.8590E+05	
.1112E+06	.1298E+06	.1441E+06	.1609E+06	.1831E+06	
.1956E+06					

SPECIFIC HEAT OF SHIELD GAS (kJ/kg.K) (ARGON)					
.5205E+00	.5205E+00	.5209E+00	.5238E+00	.5382E+00	
.5972E+00	.7971E+00	.1370E+01	.2719E+01	.5115E+01	
.7791E+01	.8973E+01	.8163E+01	.6531E+01	.5238E+01	
.4370E+01	.3901E+01	.3771E+01	.5252E+01	.1139E+02	
.1173E+02	.7515E+01	.7329E+01	.9700E+01	.1229E+02	
.1265E+02					

D: Attached Table for Mild Steel (III)

100,147L

100:	THERMAL CONDUCTIVITY OF SHIELD GAS (KW/M.K) (ARGON)				
101:					
102:	.1013E-03	.1057E-03	.1174E-03	.1432E-03	.1933E-03
103:					
104:	.2820E-03	.4279E-03	.6550E-03	.9916E-03	.1463E-02
105:					
106:	.2050E-02	.2563E-02	.2675E-02	.2480E-02	.2348E-02
107:					
108:	.2374E-02	.2507E-02	.2697E-02	.3148E-02	.3632E-02
109:					
110:	.4126E-02	.4623E-02	.5120E-02	.5618E-02	.6116E-02
111:					
112:	.6365E-02				
113:					
114:					
115:					

116:	ELECTRIC CONDUCTIVITY OF PLASMA GAS (MHO/m) (ARGON)				
117:					
118:	.5960E-04	.1270E+00	.1030E+02	.1010E+03	.3610E+03
119:					
120:	.9230E+03	.1770E+04	.2730E+04	.3730E+04	.4740E+04
121:					
122:	.5740E+04	.6670E+04	.7490E+04	.8200E+04	.8810E+04
123:					
124:	.9730E+04	.9880E+04	.1040E+05	.1080E+05	.1050E+05
125:					
126:	.1020E+05	.1040E+05	.1090E+05	.1130E+05	.1160E+05
127:					
128:	.1170E+05				
129:					
130:					
131:					

132:	ELECTRIC CONDUCTIVITY OF SHIELD GAS (MHO/m) (ARGON)				
133:					
134:	.5960E-04	.1270E+00	.1030E+02	.1010E+03	.3610E+03
135:					
136:	.9230E+03	.1770E+04	.2730E+04	.3730E+04	.4740E+04
137:					
138:	.5740E+04	.6670E+04	.7490E+04	.8200E+04	.8810E+04
139:					
140:	.9730E+04	.9880E+04	.1040E+05	.1080E+05	.1050E+05
141:					
142:	.1020E+05	.1040E+05	.1090E+05	.1130E+05	.1160E+05
143:					
144:	.1170E+05				

Appendix E : Nomenclature

- A_c = Crown reinforcement area (m^2)
 A_E = Cross-sectional area of electrode (m^2)
 A_X = Orifice circumferential area (m^2)
 A_r = Root reinforcement area (m^2)
 C_p = Constant pressure specific heat ($J/kg \cdot K$)
 D = Orifice diameter (m)
 D_E = Electrode diameter (m)
 $D_{s,e}$ = External diameter of shielding gas (m)
 d_c = Crown bead width (m)
 d_r = Root bead width (m)
 $\frac{dv}{dL}$ = Voltage drop per unit length (V/m)
 d_w = Feed wire diameter (m)
 g = Gravitational acceleration (m/s^2)
 h_c = Crown height (m)
 h_{exit} = Plasma jet enthalpy at the exit of workpiece (J/kg)
 h_X = Plasma enthalpy corresponding to the orifice wall temperature (J/kg)
 h_{plasma} = Plasma enthalpy (J/kg)
 h_r = Root height (m)
 $h_{1,i}, h_{1,o}$ = Plasma enthalpy at entrance and exit ends, respectively, of gap between electrode and orifice (J/kg)
 $h_{2,i}, h_{2,o}$ = Plasma enthalpy at entrance and exit ends, respectively, of orifice (J/kg)
 $h_{3,i}, h_{3,o}$ = Plasma enthalpy at entrance and exit ends, respectively, of standoff column (J/kg)

$h_{4,1}, h_{4,0}$ = Plasma enthalpy at entrance and exit ends, respectively, of workpiece keyhole (J/kg)
 I_m^+, I_m^- = Main electric current in straight and reverse polarities, respectively (A)
 I_p^+, I_p^- = Pilot electric current in straight and reverse polarities, respectively (A)
 k = Thermal conductivity of plasma jet (W/m·k)
 k_E = Thermal conductivity of electrode (W/m·k)
 L_E = Length of electrode (m)
 L_1 = Distance between electrode and orifice (m)
 L_2 = Axial length of orifice (m)
 L_3 = Column distance of standoff (m)
 L_4 = Thickness of workpiece (m)
 $\dot{m}_{p,1}$ = Plasma gas mass flow rate (kg/s)
 $\dot{m}_{s,d}$ = Shielding gas mass flow rate (kg/s)
 $M_{p,1}$ = Molecular weight of plasma gas (kg/kmol)
 $M_{s,d}$ = Molecular weight of shielding gas (kg/kmol)
 n = Parabolic exponent of reinforcement shape
 \bar{P} = External pressure (N/m²)
 $P_{p,1}$ = Partial pressure of plasma gas (N/m²)
 P_E = Power input at electrode (W)
 P_H = Environment pressure (N/m²)
 $P_{s,d}$ = Partial pressure of shielding gas (N/m²)
 $P_{J,1}$ = Joule heating power input in the gap between electrode and orifice (W)
 $P_{J,2}$ = Joule heating power input in the orifice (W)
 $P_{J,3}$ = Joule heating power input in the standoff column (W)
 $P_{N,1}$ = Orifice work function induced power input (W)

$P_{X,2}$ = Orifice anode drop induced power input (W)
 $P_{V,1}$ = Workpiece work function induced power input (W)
 $P_{V,2}$ = Workpiece anode and cathode drops induced power input (W)
 $P_{1,1}, P_{1,0}$ = Plasma arc power at entrance and exit ends respectively, of gap between electrode and orifice (W)
 $P_{2,1}, P_{2,0}$ = Plasma arc power at entrance and exit ends respectively, of orifice (W)
 $P_{3,1}, P_{3,0}$ = Plasma arc power at entrance and exit ends respectively, of standoff column (W)
 $P_{4,1}, P_{4,0}$ = Plasma power at entrance and exit ends, respectively, of workpiece keyhole (W)
 Q_{dis} = Plasma arc discharged power loss (at exit end of keyhole) (W)
 Q_G = Power loss in the gap between electrode and orifice (W)
 Q_X = Total power loss in the orifice (W)
 $Q_{X,c}$ = Convective heat transfer power loss in the orifice (W)
 $Q_{X,e}$ = Free electron power loss in the orifice (W)
 $Q_{X,g}$ = Direct power loss from the surface of the orifice contributed by total power input to work function and part of power input to anode drop at orifice (W)
 $Q_{s,r}$ = Standoff column radiative power loss (W)
 $Q_{s,c}$ = Standoff column convective power loss (W)
 Q_s = Standoff column total power loss (W)
 $Q_{W,c}$ = Convective heat transfer workpiece power loss (W)
 $Q_{W,e}$ = Free electron power loss in workpiece (W)
 Q_W = Total power loss in workpiece (W)
 R = Universal gas constant (J/mol·K)
 R_E = Effective radius of plasma jet (m)
 R_0 = Orifice radius (m)
 R_i = Distant between source and point of computation at workpiece (m)

t_+ , t_- = Time duration for straight and reverse polarities, respectively (s)
 T_E = Effective temperature of plasma jet; Electrode temperature (K)
 T_H = Environment temperature (K)
 T_m = Melting temperature of workpiece (K)
 T_0 = Jet core temperature; Initial temperature of workpiece (K)
 u = Welding traveling speed; plasma jet velocity (m/s)
 u_H = Ambient flow velocity (m/s)
 u_0 = Jet core velocity (m/s)
 $V_A, V_B, V_C, V_D, V_E, V_F, V_G$ = Straight polarity electric voltage, shown in Figure 1, at points A, B, C, D, E, F, and G, respectively (V)
 $V_{A'}, V_{B'}, V_{C'}, V_{D'}, V_{E'}, V_{F'}, V_{G'}$ = Reverse polarity electric voltage, shown in Figure 1, at points A', B', C', D', E', F', and G', respectively (V)
 \dot{V}_G = Plasma volumetric flow rate in the gap between electrode and orifice (m^3/s)
 V_s = Plasma volume in the standoff column (m^3/s)
 V_w = Wire feeding speed (m/s)
 W_g = Initial gap distance between two workpieces (m)
 x_H = Distance of Jet Initial Region (m)
 y = Coordinate axis
 y_c = Coordinate to be used for spatial temperature distribution computation (m)
 z = Coordinate axis
 z_c = Coordinate to be used for spatial temperature distribution computation (m)
 z_{1-35} = Heat source spatial point of distribution (m)
 α = Angle (rad); workpiece thermal diffusivity (m^2/s)

- θ = Angle (rad)
 $\Delta V_a, \Delta V_c$ = Anode and cathode electric potential drops, respectively (V)
 $\Delta V_m^+, \Delta V_m^-$ = Main electric voltage drops in straight and reverse polarities, respectively (V)
 $\Delta V_p^+, \Delta V_p^-$ = Pilot electric voltage drops in straight and reverse polarities, respectively (V)
 ϵ = Emissivity of workpiece
 ϵ_R = Reverse polarity voltage rise (V)
 σ_s = Surface tension coefficient (N/m)
 ϕ = Fraction of heat source distributed in spatial coordinate
 ϕ_E = Electrode work function (V)
 ϕ_N = Orifice work function (V)
 ϕ_w = Workpiece work function (V)
 ψ = Fraction of orifice, or workpiece, power loss contributed by anode and cathode drops
 η = Dimensionless coordinate
 ρ_{p1} = Mass of plasma gas in unit volume of plasma jet (kg/m^3)
 ρ_{sd} = Mass of shielding gas in unit volume of plasma jet (kg/m^3)

Basic Input Parameters (I)

(Aluminum #2219-T87)

Symbol	Description	Data Input
L_1	Distance between electrode and nozzle	1.1176 mm
L_2	Vertical length of nozzle	3.2760 mm
L_4	Thickness of workpiece	6.35 mm
L_E	Length of electrode	69.6 mm
D	Nozzle diameter	3.175 mm
D_E	Electrode diameter	3.9624 mm
K_E	Thermal conductivity of electrode	23.5 kW/m·°K
\dot{m}	Argon gas mass flow rate	Variable
ϕ_E	Electrode work function	3.0 V
ϕ_N	Nozzle work function	4.5 V
ϕ_w	Workpiece work function	3.8 V
ΔV_a	Anode potential drop	3.0 V
ΔV_c	Cathode potential drop	4.5 V
I_m^+	Main electric current in straight polarity	Variable
I_m^-	Main electric current in reverse polarity	Variable
I_p^+	Pilot electric current in straight polarity	Variable
I_p^-	Pilot electric current in reverse polarity	Variable
t_+	Time duration for straight polarity	19 ms
t_-	Time duration for reverse polarity	4 ms
T_E	Electrode temperature	2500 °K
T_N	Nozzle temperature	400 °K
T_0	Environment temperature; Initial temperature of workpiece	298 °K

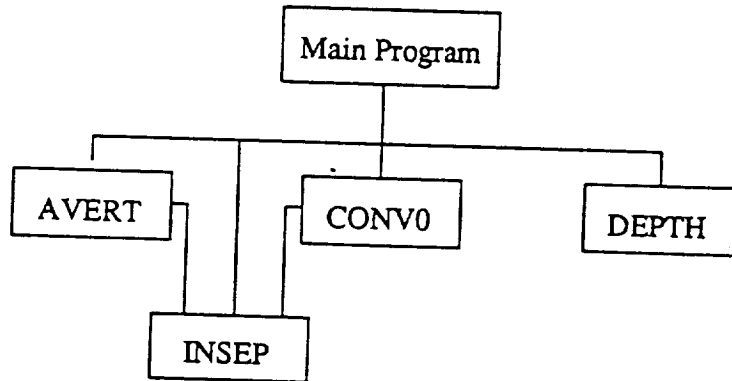
Basic Input Parameters (II)
(Aluminum #2219-T87)

Symbol	Description	Data Input
h_N	Plasma enthalpy corresponding to orifice wall temperature	0.208 $\frac{\text{kJ}}{\text{g}}$
h_K	Plasma enthalpy corresponding to keyhole temperature	0.476 $\frac{\text{kJ}}{\text{g}}$
ϕ	Fraction of power loss due to anode and cathode drops	0.0
ϕ	Location of welding heat source from back of workpiece in fraction of plate thickness	0.5 - 1.0
u	Welding traveling speed	Variable
k_w	Thermal conductivity of workpiece	0.13 $\frac{\text{kw}}{\text{m} \cdot ^\circ\text{K}}$
α	Thermal diffusivity of workpiece	$5.678 \times 10^{-5} \frac{\text{m}^2}{\text{s}}$
ρ_w	Density of workpiece	2650 kg/m^3
Q_f	Melting heat of workpiece	387 kJ/kg
ϵ	Emissivity of workpiece	0.1
T_m	Melting temperature of workpiece	916 $^\circ\text{K}$

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Appendix F Block Diagram of Penetration Depth Calculation

Structure Diagram of WELD0 Computer Program
(Computation of penetration depth)



Explanation of WELD0 Program Structure

1. Main Program

Input physical parameter tables of plasma and shield gas and initial parameters of welding process. Compute distribution of related physical parameters of plasma and shield gas, such as electric potential, power, power loss, enthalpy, etc., between torch and workpiece.

2. Subroutine AVERT

Compute mean temperature of plasma and shield gas mixture with given plasma and shield gas flow rate and power of the mixture.

3. Subroutine INSEP

Compute interpolatively temperature or enthalpy and their corresponding values of related physical parameters of plasma and shield gas with input values of plasma and shield gas material constants and given temperature or enthalpy of plasma and shield gas.

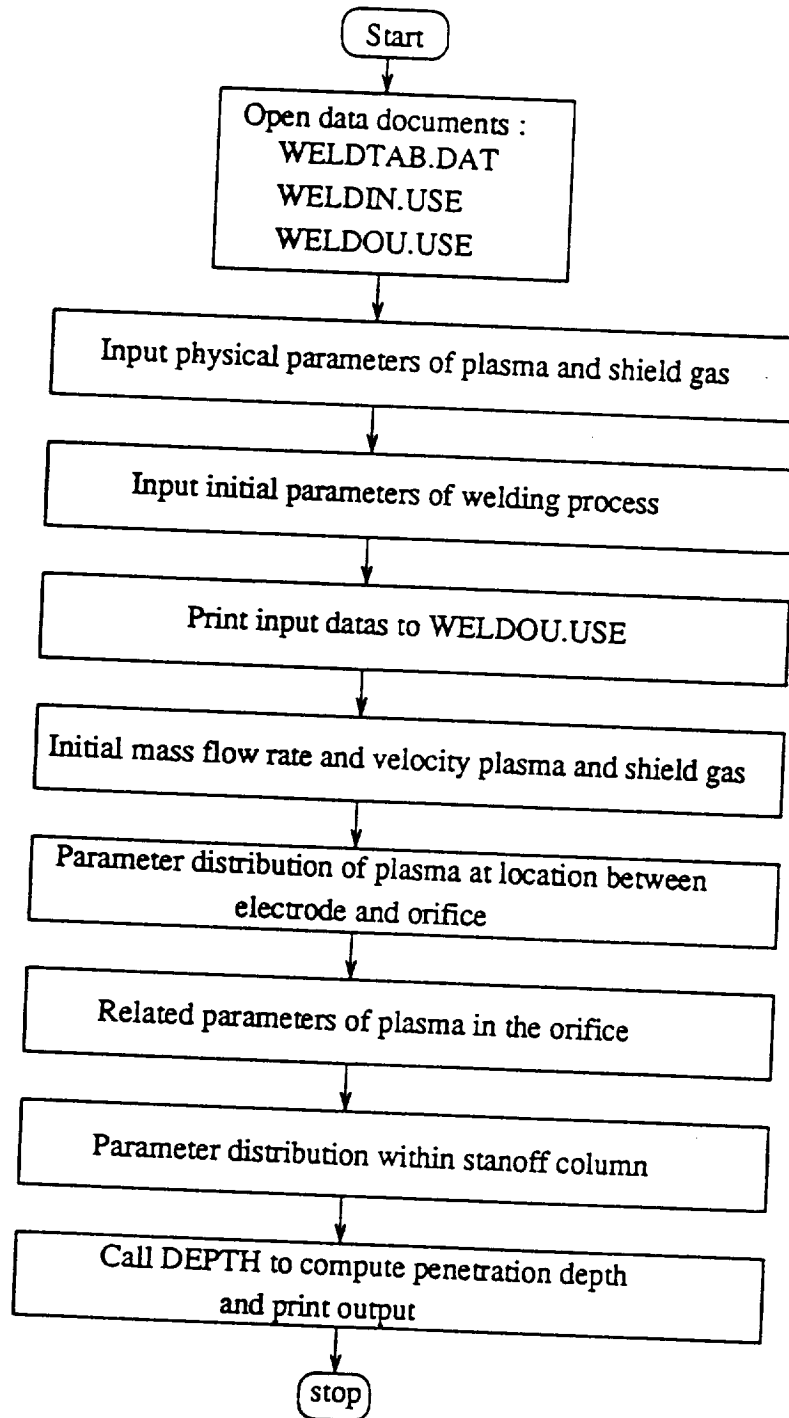
4. Subroutine CONV0

Compute power transmission from plasma jet to workpiece through heat process.

5. Subroutine DEPTH

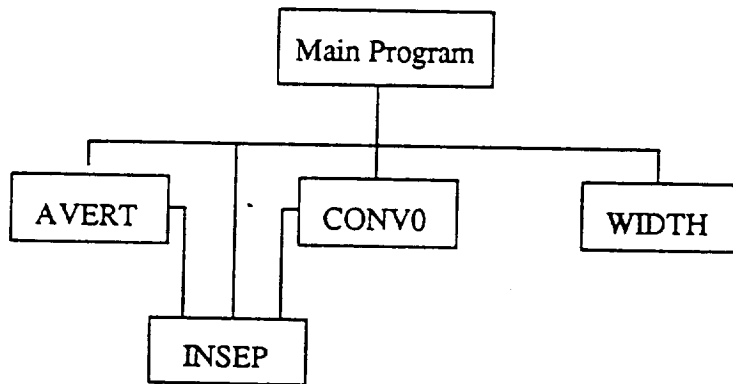
Compute temperature distribution, geometry of molten pool of workpiece and depth of partial penetration of welding process.

Flow Chart of WELD0 Computation Program



Appendix G Block Diagram of VPPA Modeling Structure

Structure Diagram of Diagram of WELDBOTH
(VPPA Modeling)



Explanation of WELDBOTH Program Structure

1. Main Program

Input physical parameter tables of plasma and shield gas and initial parameters of welding process. Compute distribution of related physical parameters of plasma and shield gas, such as electric potential, power, power loss, enthalpy, etc., between torch and workpiece.

2. Subroutine AVERT

Compute mean temperature of plasma and shield gas mixture with given plasma and shield gas flow rate and power of the mixture.

3. Subroutine INSEP

Compute interpolatively temperature or enthalpy and their corresponding values of related physical parameters of plasma and shield gas with input values of plasma and shield gas material constants and given temperature or enthalpy of plasma and shield gas.

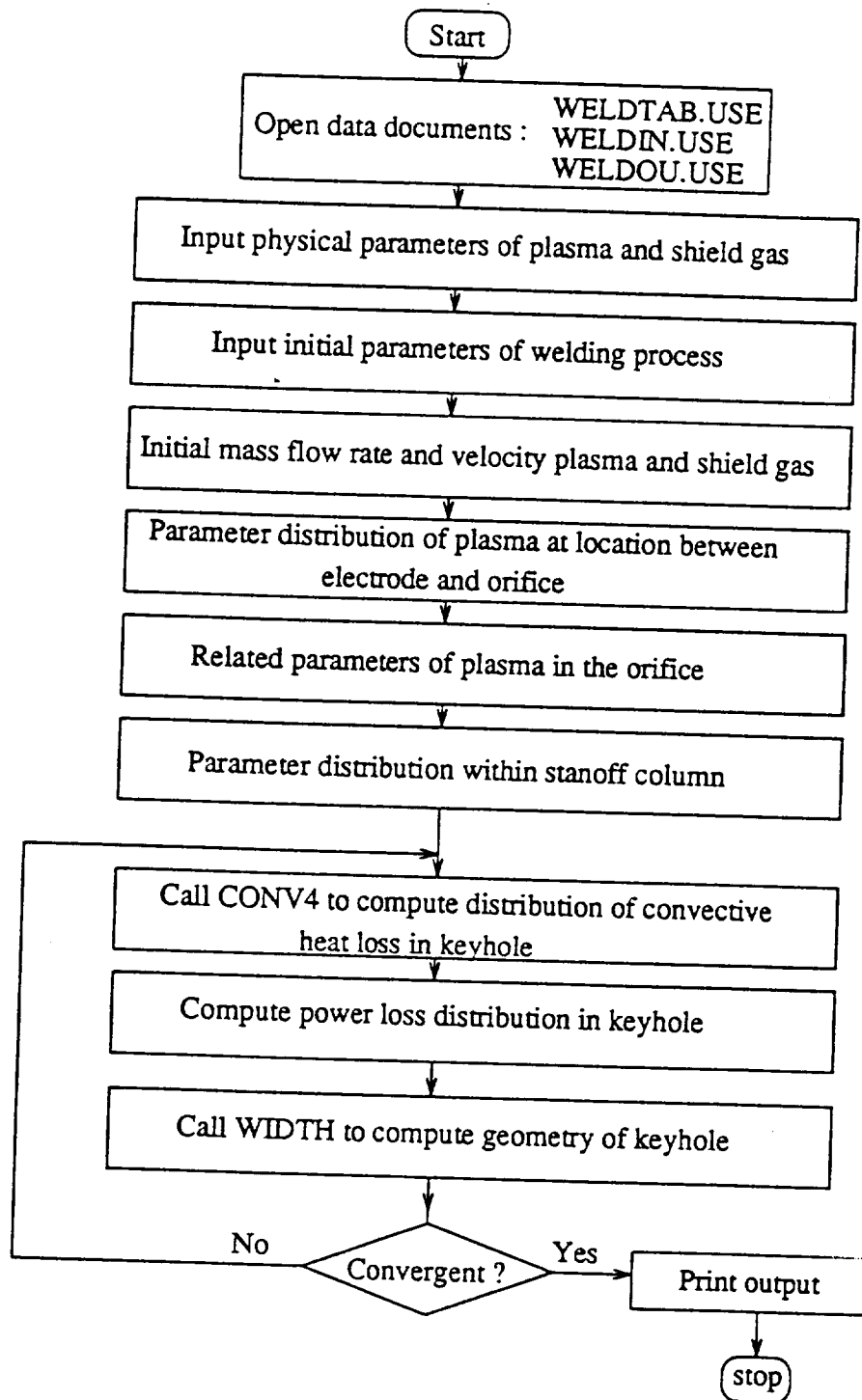
4. Subroutine CONV4

Compute power transmission from plasma jet to the wall of keyhole in workpiece through heat convection process.

5. Subroutine DEPTH

Compute crown and root widths based on temperature distribution of workpiece and geometry of keyhole.

Flow Chart of WELDBOTH Computation Program



Appendix H

Comparison Between Results of Model Computations and Experimental Measurements

Figures H-1 to H-63 show the comparison between the results of model computations and experimental measurements. Model computations are based on the mathematical formulations illustrated in this report, while experimental measurements are adopted from the experiments accomplished by Nichols Research Corporation (1992).

In Figures H-1 to H-31, comparisons are made between the model computed values of forward electric voltage and reversed electric voltage versus that of the values of experimental measurements. The results show that the tendency and magnitudes of the model computations are very much the same as that of the experimental measurements.

In Figures H-32 to H-38, comparisons are made for leading edge angle between model computed values and that of the values of experimental measurements. There are so many parameters which could be changed in the experimental measurements. It is very hard to choose a series of experimental measurement with one parameter as a variable and with the rest of the parameters unchanged. Comparisons made in Figures H-32 to H-38 follow the order of the sequence of experimental measurement of leading edge angle between model computation and experiment. The results also show that the tendency and magnitudes of the model computations are very much the same as that of the experimental measurements.

Figures H-39 to H-62 show the comparison for crown width and root width between model computed values and that of the values of experimental measurements. The results show that the model computation and the experimental measurement are relatively in good manners of agreement. It is noted that some parameters provide a great influence on the model computation of the crown and root widths. However, within the range of proper control of parameters, it can anticipate to predict a fairly reasonably good values of model computation in crown and root widths agreeable in comparison with the experimental measurements.

As to the problems of abnormal welding, model formulations illustrated in Section VII of this report have been adopted to calculate the probability of the keyhole full and partial penetrations of the welding workpiece. Table H-A shows the results of model computations for keyhole full and partial penetration of the workpiece in comparison to experimental measurements of ID Numbers 7A to 7P listed in the report accomplished by Nichols Research Corporation (1992), while Table H-B illustrates the results of the similar model computations in comparison to experimental measurements of ID Numbers 8A to 8N listed in the same report. It shows that the results of model computation are basically all agreeable with the experimental measurements based on the points of the possibility of keyhole full and partial penetrations of the welding workpiece.

For the purpose of making easier comparison for the possibility of keyhole full and partial penetrations of welding workpiece among so many different controlled parameters of welding

process between model computation and experimental measurements, a set of dimensionless parameters are proposed and illustrated in Figure H-63 with $V \cdot H / (2\alpha)$ as the horizontal coordinate and $Q / [4\pi \cdot H \cdot (k \cdot \Delta T_m + \alpha \rho L_f)]$ as the vertical coordinate. Here,

- V = Welding Speed
- H = Thickness of workpiece
- α = Thermal diffusivity of workpiece
- k = Thermal conductivity of workpiece
- ΔT_m = Temperature difference between molten and initial temperatures of workpiece
- ρ = Density of workpiece
- L_f = Latent heat of molten workpiece
- Q = Total power absorption of workpiece during the welding process.

Recall that there is no available experimental measurements of Q values because of the difficulty in accurate measurements of Q values experimentally. Q values adopted in Figure H-63 are calculated based on the physical model illustrated in Equation (7-3) of this report.

Figure H-63 shows the critical curve for keyhole full and partial penetrations of welding workpiece from the model computation. In this figure, the left-hand upper region shows the zone of keyhole full penetration while the right-hand lower region illustrates the zone of partial penetration. This curve is computed based on the condition of the bottom portion of the workpiece to attain molten temperature of the metal. Precise locations of each experimental measurements with experimental ID

numbers 7 and 8 from the Nichols report are also plotted. In these experiments, aluminum workpiece with thickness of 1/4" (6.35 mm) are used. The results show that the model computations predict the keyhole full and partial penetrations of welding completely agreeable with that of the experimental measurements.

Table H-A (a)

CALCULATION COMPARED WITH EXPERIMENT

ID#	QSQS	QORIG	QM	Keyhole(Y/N)?	
	(KW)	(KW)	(KW)	Cal.	Exp.
7A1	1.235	1.331	.143	Y	Y
7A2	1.306	1.474	.163	Y	Y
7A3	1.404	1.604	.199	Y	Y
7B1	1.241	1.390	.143	Y	Y
7B2	1.337	1.515	.173	Y	Y
7B3	1.444	1.657	.212	Y	Y
7C1	1.300	1.467	.167	Y	Y
7C2	1.394	1.590	.196	Y	Y
7C3	1.507	1.740	.233	Y	Y
7D1	1.377	1.567	.191	Y	Y
7D2	1.493	1.703	.225	Y	Y
7D3	1.534	1.853	.264	Y	Y
7E1	1.226	1.340	.115	N 51.4 %	N
7E2	1.347	1.479	.132	N 55.6 %	N
7E3	1.456	1.614	.153	N 63.0 %	N
7F1	1.257	1.373	.121	N 51.9 %	N
7F2	1.335	1.526	.141	N 59.3 %	N
7F3	1.502	1.673	.171	N 64.3 %	N
7G1	1.321	1.455	.134	N 53.6 %	N
7G2	1.432	1.585	.135	N 61.7 %	N
7G3	1.563	1.755	.183	N 66.2 %	N

Table H-A (b)

7H1	1.393	1.544	.145	N	60.2 %	N
7H2	1.516	1.691	.174	N	64.8 %	N
7H3	1.665	1.874	.209	N	75.0 %	N
7I1	0.981	1.087	.106	N	77.14%	INTERMIT
7I2	1.098	1.232	.134	Y		INTERMIT
7I3	1.231	1.385	.172	Y		INTERMIT
7J1	1.004	1.111	.107	N		INTERMIT
7J2	1.133	1.284	.151	Y		INTERMIT
7J3	1.246	1.426	.180	Y		INTERMIT
7K1	1.074	1.202	.128	N		INTERMIT
7K2	1.197	1.364	.167	Y		INTERMIT
7K3	1.305	1.501	.196	Y		INTERMIT
7L1	1.137	1.290	.153	Y		INTERMIT
7L2	1.261	1.444	.183	Y		INTERMIT
7L3	1.380	1.592	.212	Y		INTERMIT
7M1	0.961	1.071	.110	N	46.7%	N
7M2	1.111	1.248	.137	N	50.5%	N
7M3	1.228	1.384	.156	N	52.7%	N
7N1	1.011	1.123	.113	N	47.0%	N
7N2	1.155	1.299	.144	N	51.2%	N
7N3	1.280	1.444	.164	N	53.2%	N
7O1	1.072	1.202	.130	N	49.4%	N
7O2	1.216	1.370	.154	N	52.1%	N
7O3	1.345	1.519	.152	N	54.1%	N

Table H-A (c)

7P1	1.165	1.311	.148	N	51.2%	N
7P2	1.311	1.473	.169	N	53.6%	N
7P3	1.445	1.623	.184	N	59.1%	N

=====

Material : 1/4" (6.35mm) 2219-T97 Aluminum (7A-7H)
 1/4" (6.35mm) A36 Mild Steel (7I-7P)

QORIG = Power absorbed by workpiece.

QM = Latent power of workpiece.

QSQS = Conduction loss in workpiece (= QORIG-QM).

These values are calculated by the model

Table H-8

CALCULATION COMPARED WITH EXPERIMENT

Estimating whether keyhole can be formed

ID#	CALCULATION				EXPERIMENT RESULTS			
	QSQS (kW)	QORIG (kW)	QM (kW)	Keyhole? (Y/N)	Weld width/ Crown Root	Weld height/ Crown Root	Bead Ap- pearance	
8A	1.103	1.184	.089	N 85.7 %	9.86 *	1.24 *	PP,N	
8B	1.101	1.180	.070	N 85.2 %	9.45 *	1.30 *	PP,N	
8C	1.105	1.135	.080	N 85.9 %	9.40 *	1.31 *	PP,N	
8D	1.103	1.183	.080	N 85.6 %	9.41 *	1.08 *	PP,N	
8E	1.103	1.183	.080	N 85.6 %	9.58 *	1.52 *	PP,N	
8F	0.935	0.982	.046	N 61.6 %	5.74 *	1.70 *	PP,N	
8G	1.164	1.362	.198	Y	10.03 *	1.14 0.75	PP,PT,N	
8H	0.979	1.084	.105	N 76.1%	9.00 *	1.25 *	PP,N	
8I	0.976	1.081	.105	N 75.8%	8.38 *	1.85 *	PP,D	
8J	0.977	1.082	.105	N 75.9%	9.80 *	1.17 *	PP,D	
8K	0.977	1.082	.105	N 75.9%	9.32 *	1.02 *	PP,D	
8L	0.972	1.078	.104	N 76.5%	8.78 *	1.30 *	PP,N	
8M	0.889	0.973	.084	N 67.4%	7.87 *	1.11 *	PP,N	
8N	1.059	1.182	.123	N 87.0%	8.28 *	* *	PP,D	

Material : 1/4"(6.35mm) 2219-T87 Aluminum (8A-8G)
1/4"(6.35mm) A36 Mild Steel (8H-8N)

QORIG = Power absorbed by workpiece.

QM = Latent power of workpiece.

QSQS = Conduction loss in workpiece (= QORIG-QM).

These values are calculated by the model

VOLTAGE (1/4" AL. #F)

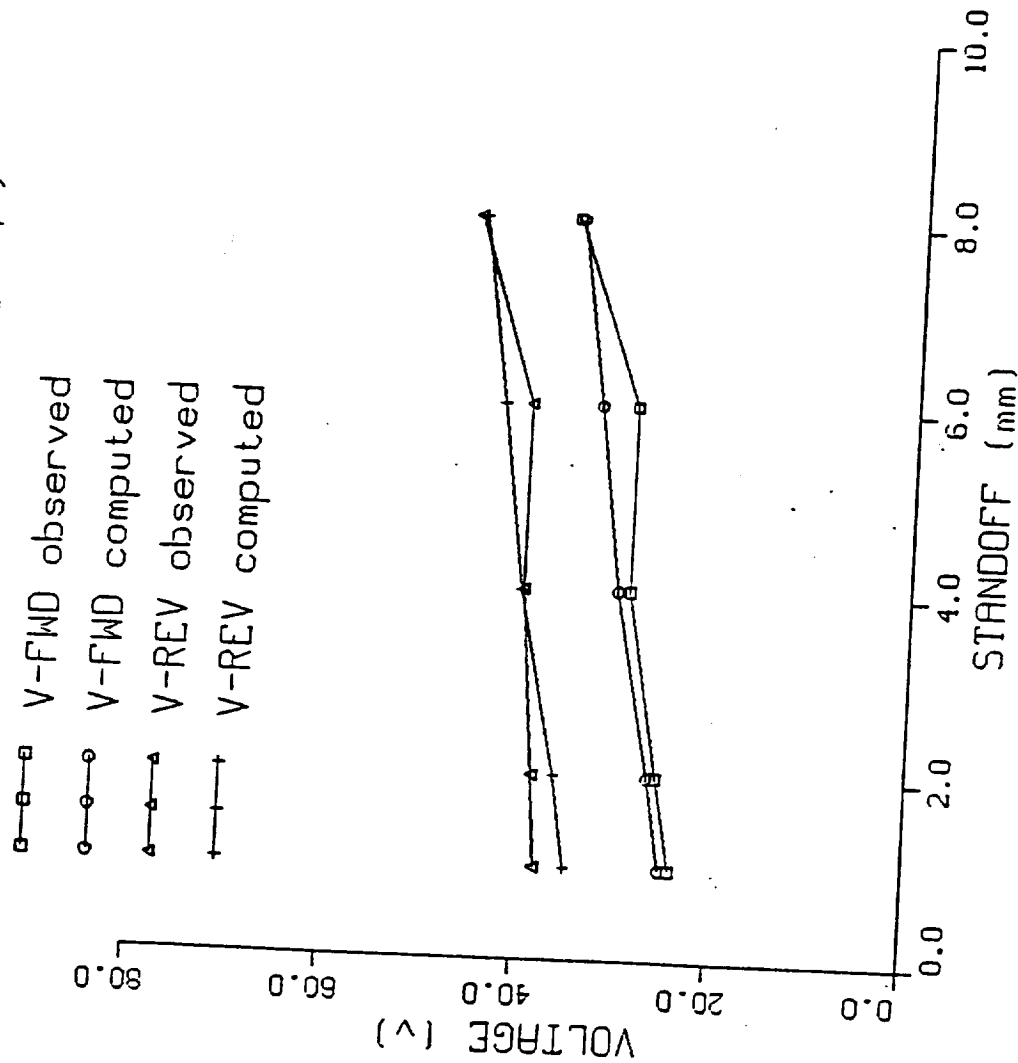


Fig. H-1

VOLTAGE (1/4' AL. #G1, L3=2mm)

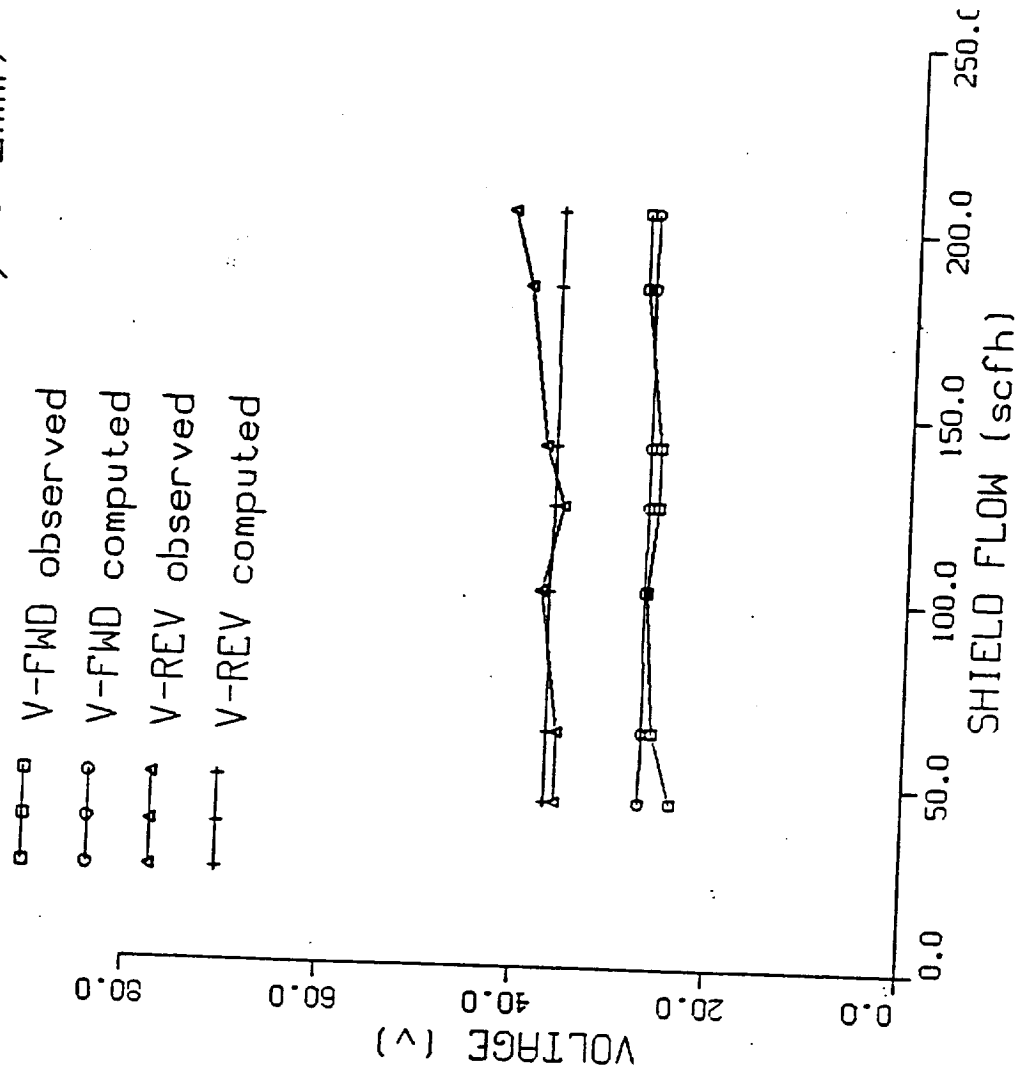


Fig. H-2

VOLTAGE (1/4" AL. #G1, L3=4mm)

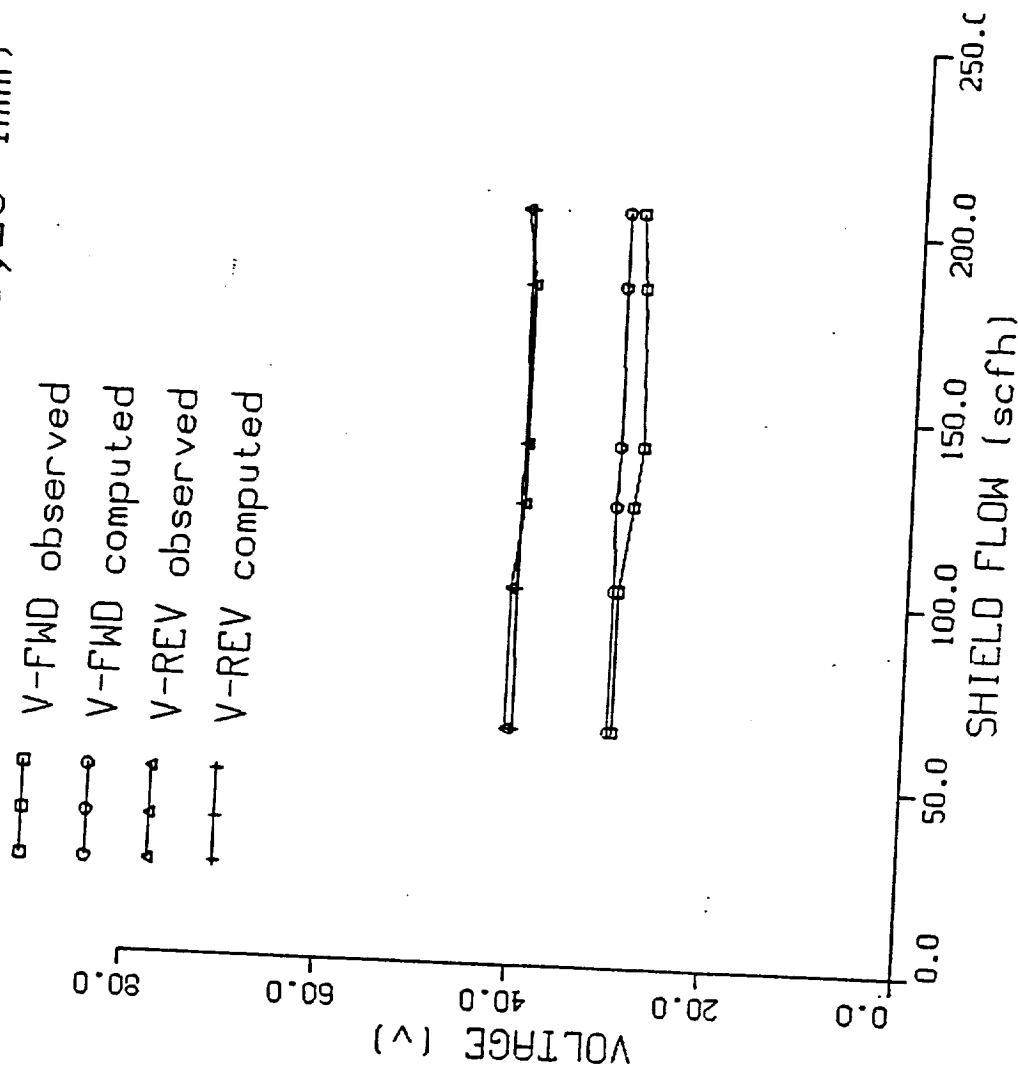


Fig. H-3.

VOLTAGE (1/4' AL. #G1, L3=8mm)

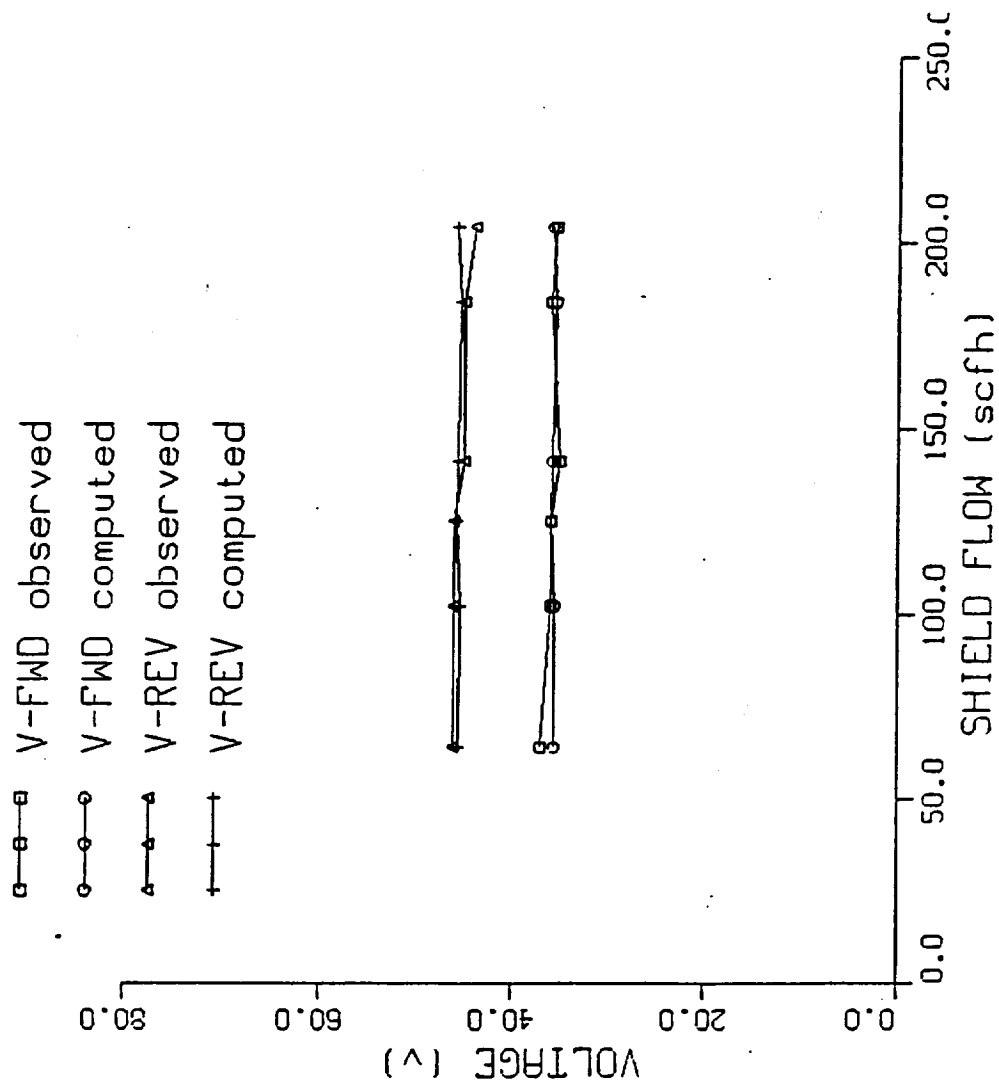


Fig H-4

VOLTAGE (1/4' AL. #H1, L3=2mm)

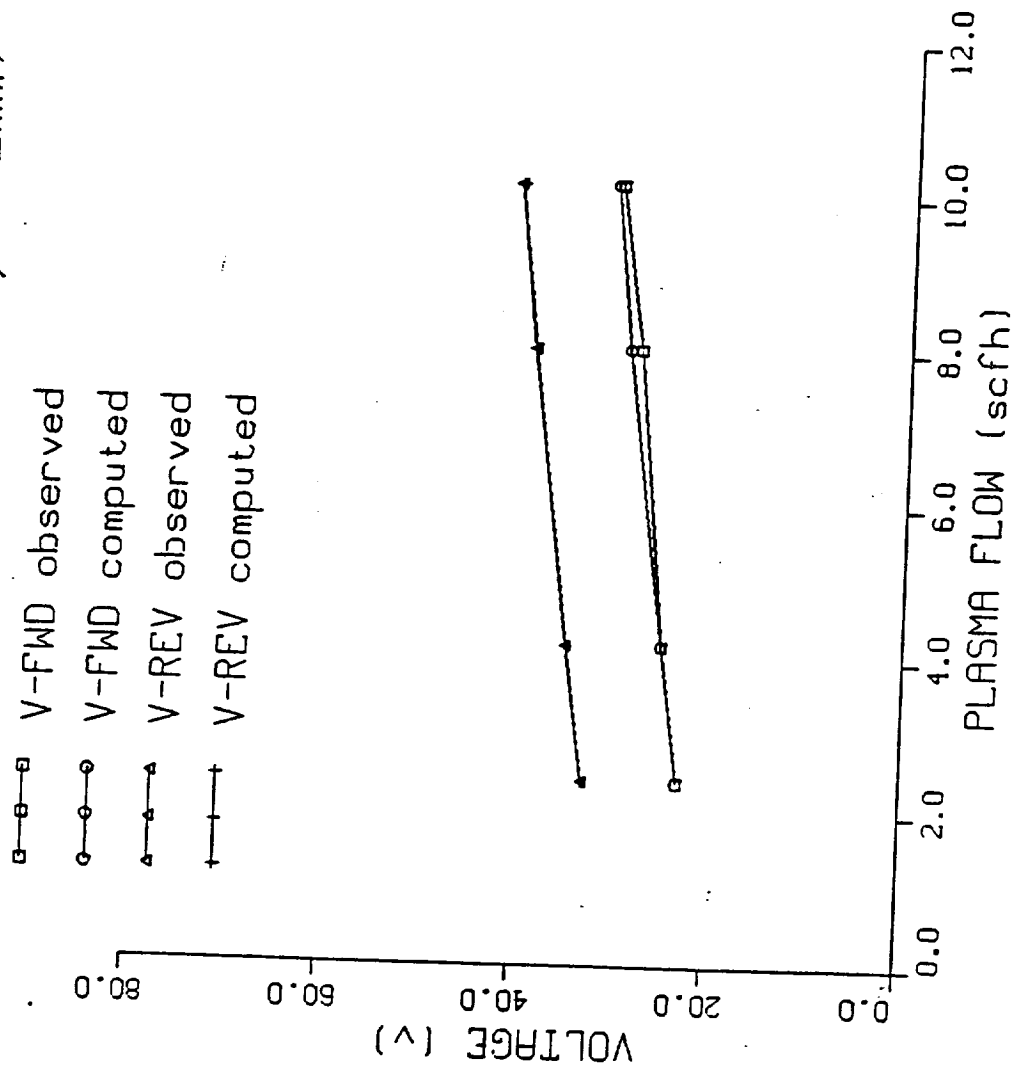


Fig. H-5

VOLTAGE (1/4" AL. #H1, L3=4mm)

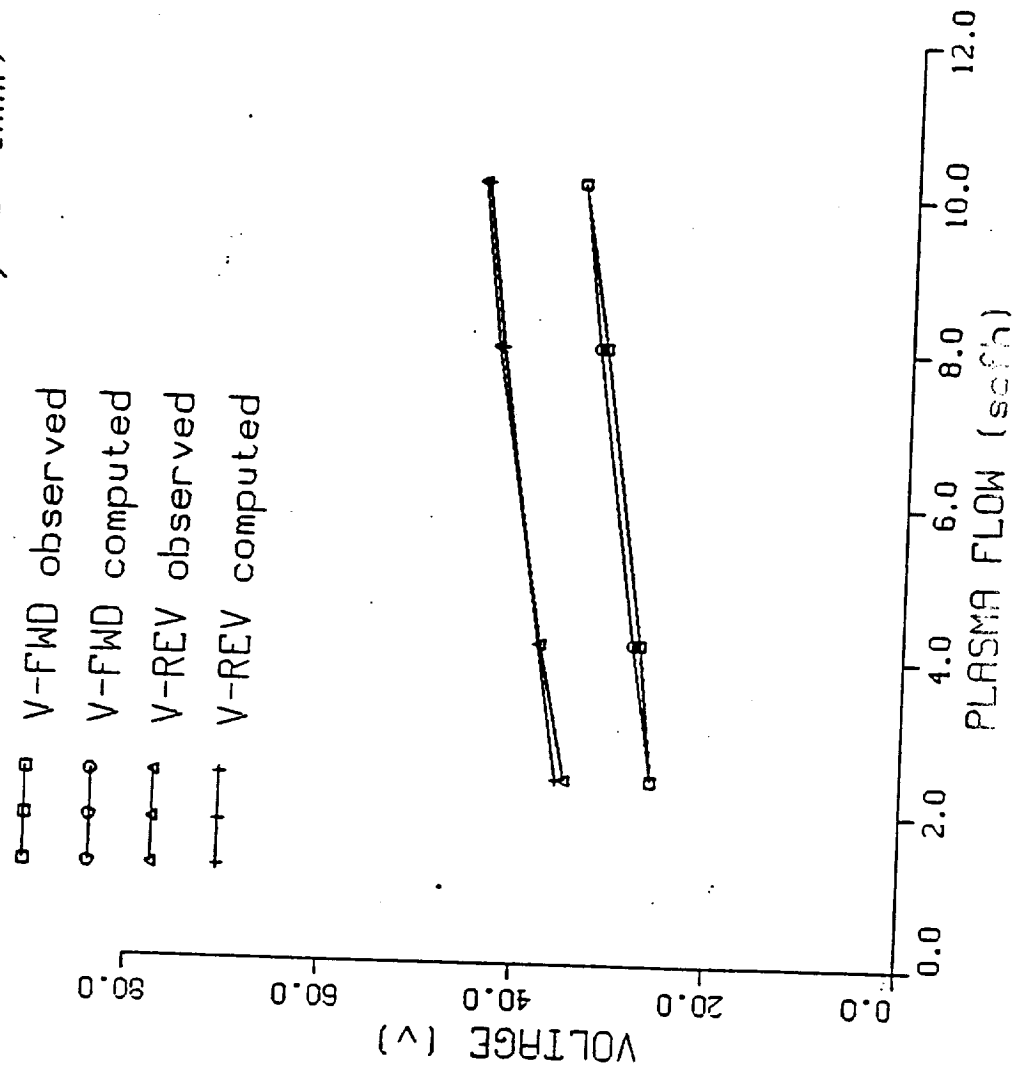


Fig. H-6

VOLTAGE (1/4' AL. #H1, L3=8mm)

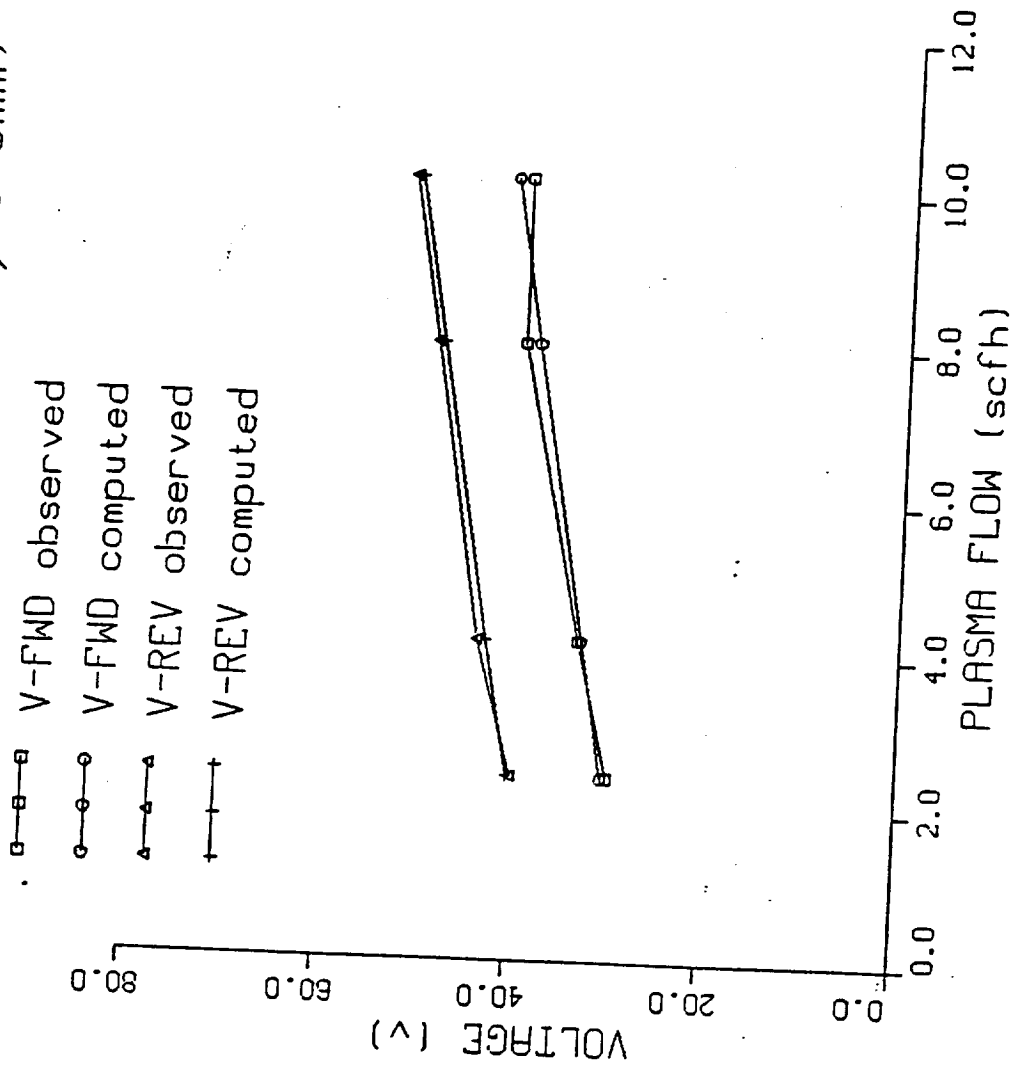


Fig. H-7

VOLTAGE (1/4" AL. #I1, L3=2mm)

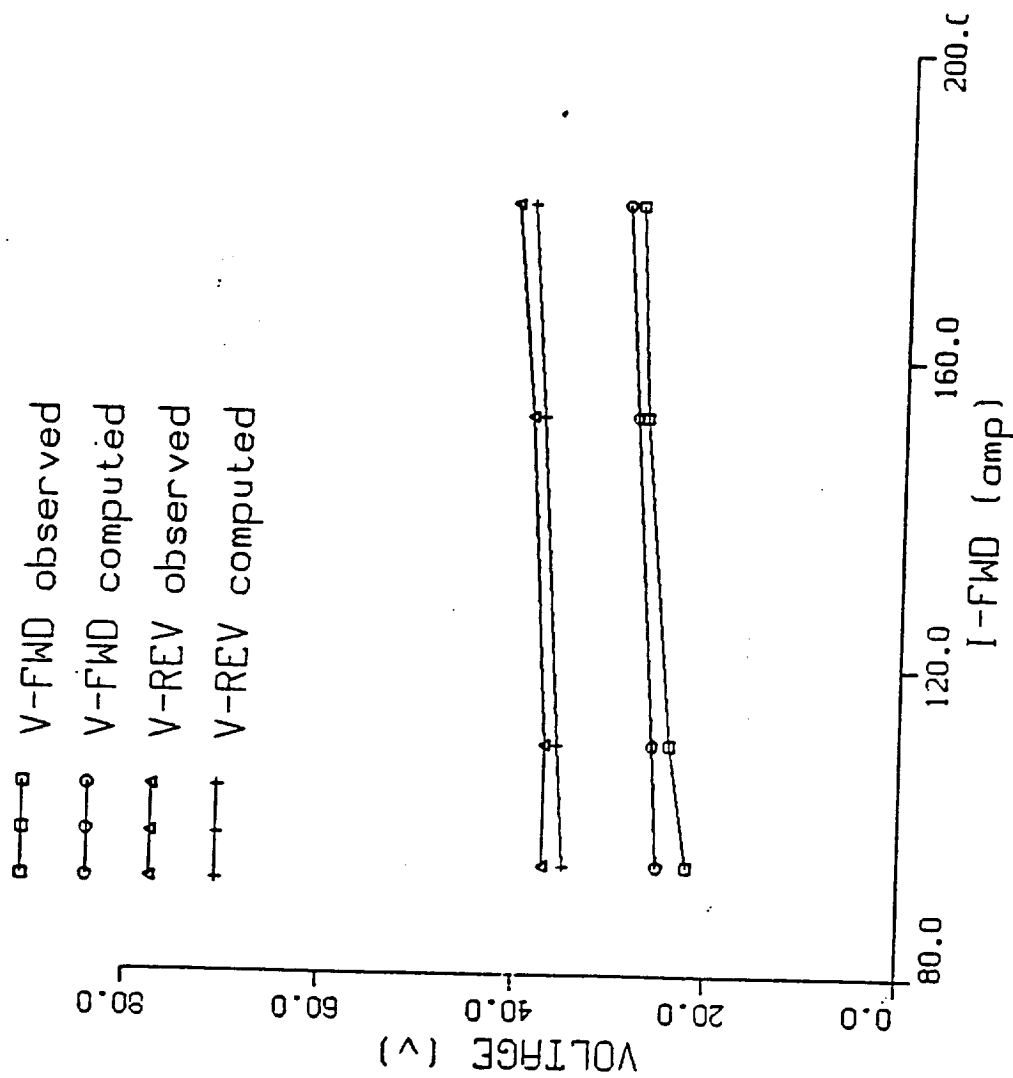
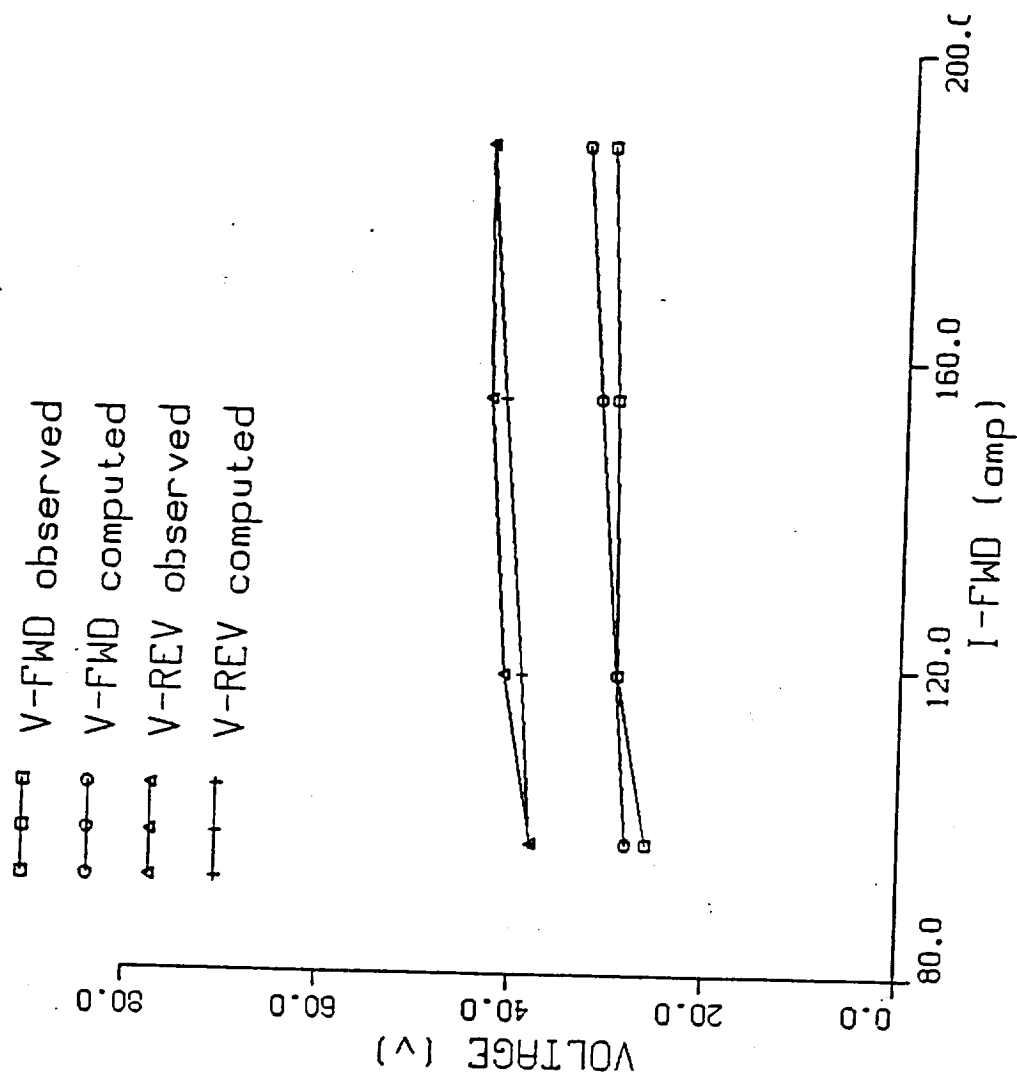


Fig. H-8

VOLTAGE (1/4" AL. #I1, L3=4mm)



Cut

Fig. H-9

VOLTAGE (1/4' AL. #I1, L3=8mm)

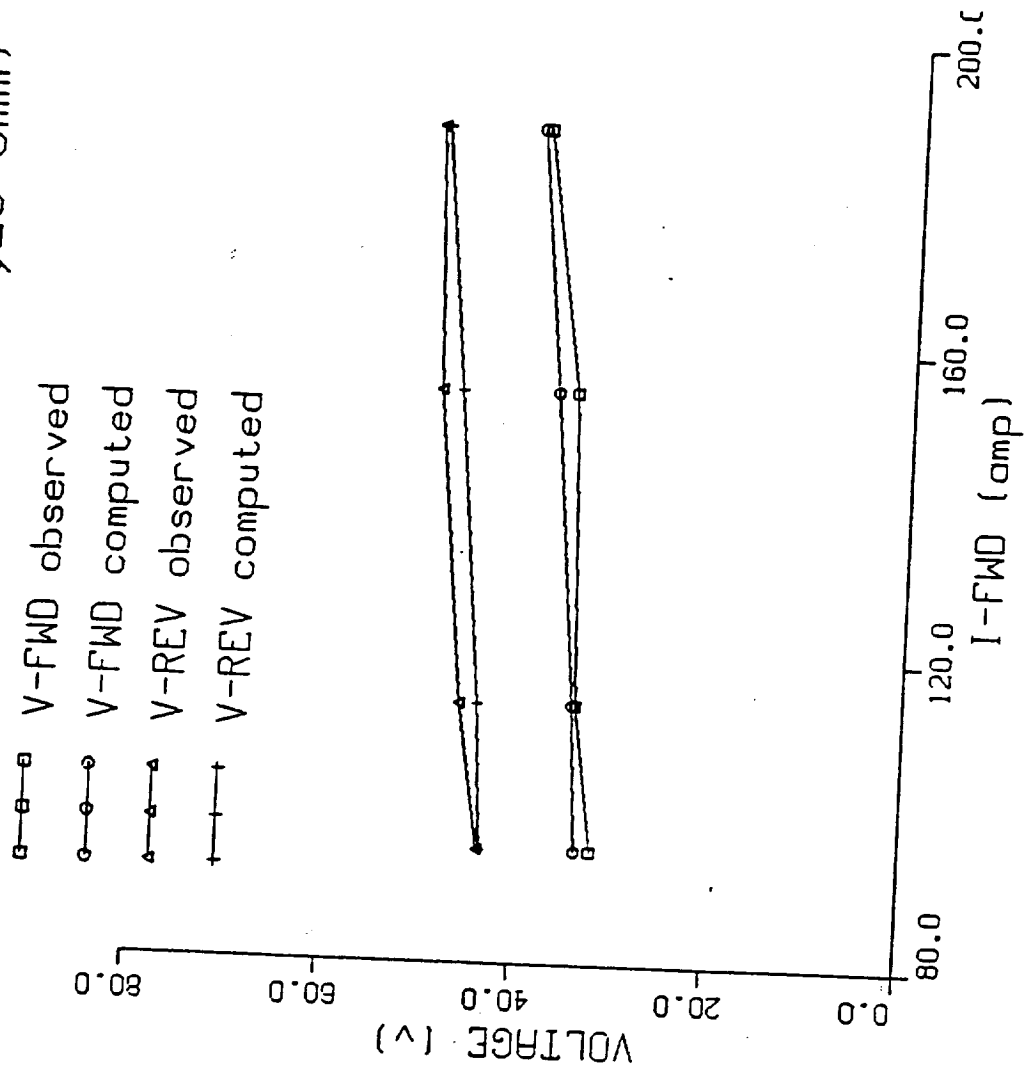


Fig. H-10

VOLTAGE (1/4' AL. #J1, L3=2mm)

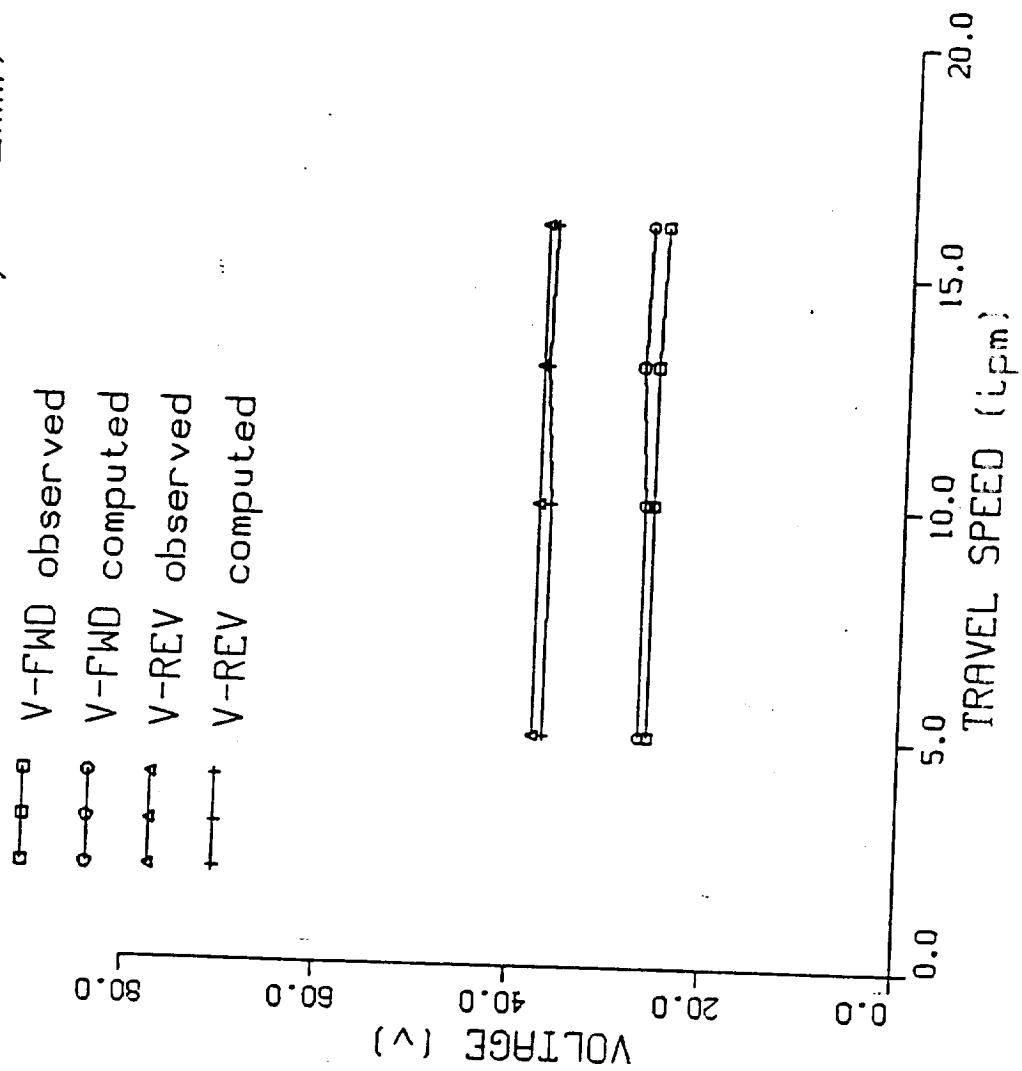


Fig. H-11

VOLTAGE (1/4" AL. #J1, L3=4mm)

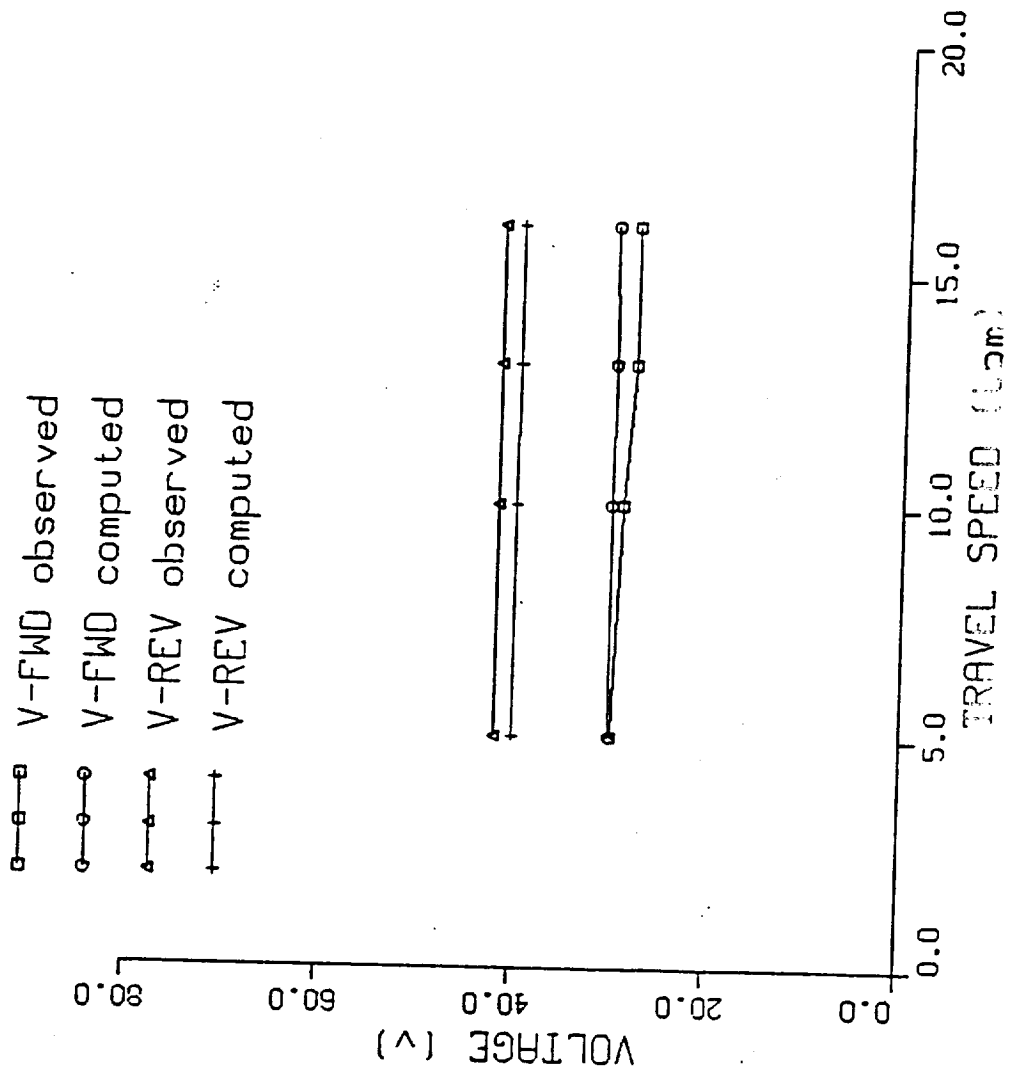
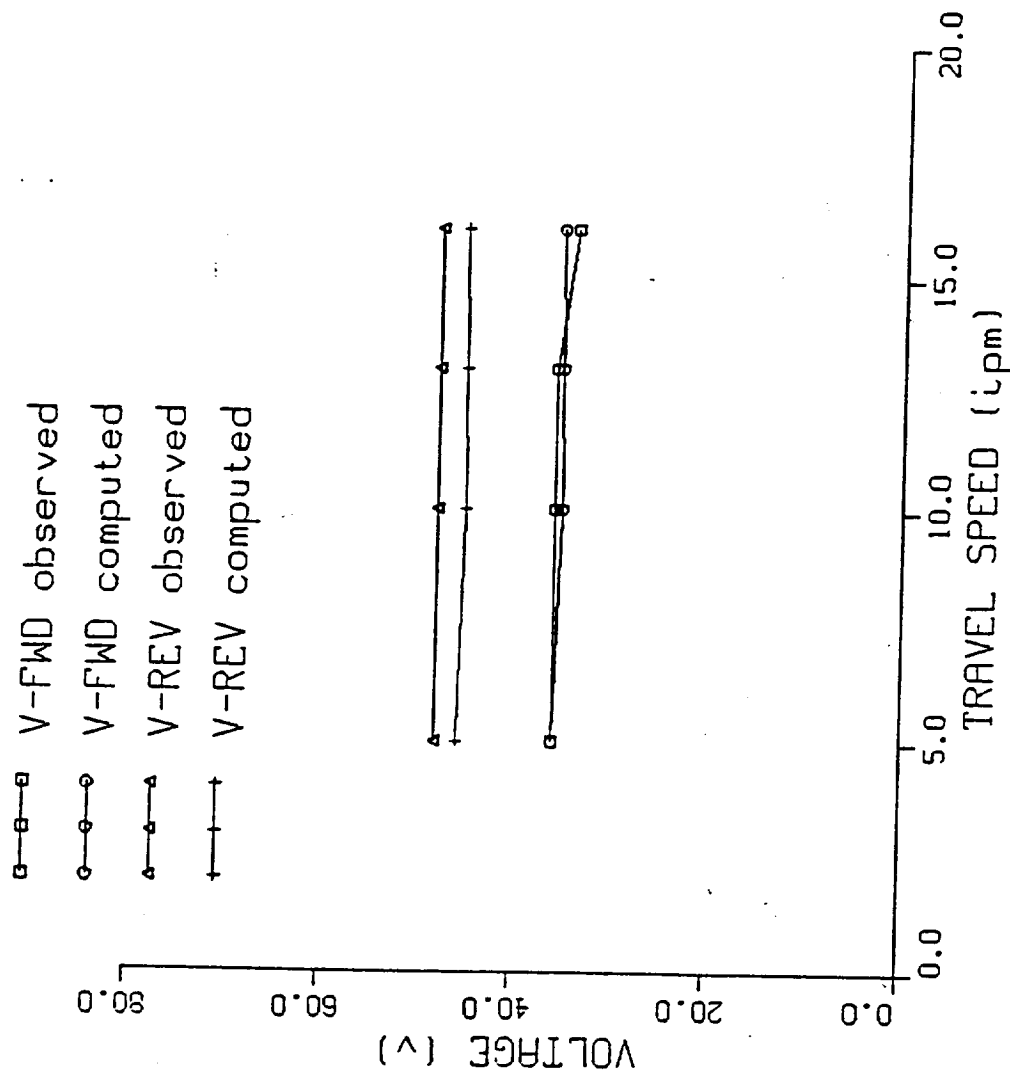


Fig. H-12

VOLTAGE (1/4' AL. #J1, L3=8mm)



RC
U
LU

Fig. H-13

VOLTAGE (1/4" AL. #K2, U=12.5 ipm)

- V-FWD observed
- V-FWD computed
- △ V-REV observed
- † V-REV computed

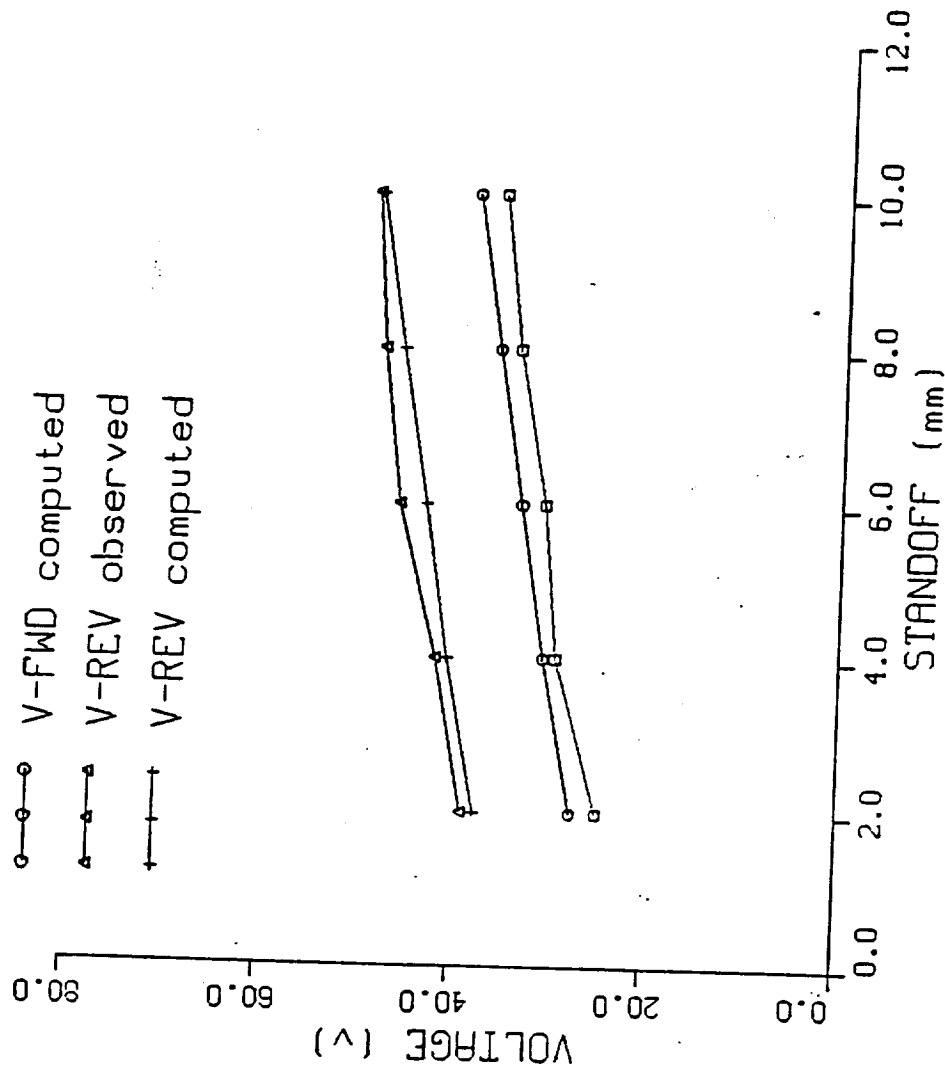


Fig. H-14

VOLTAGE (1/4' AL. #K2, U=16 ipm)

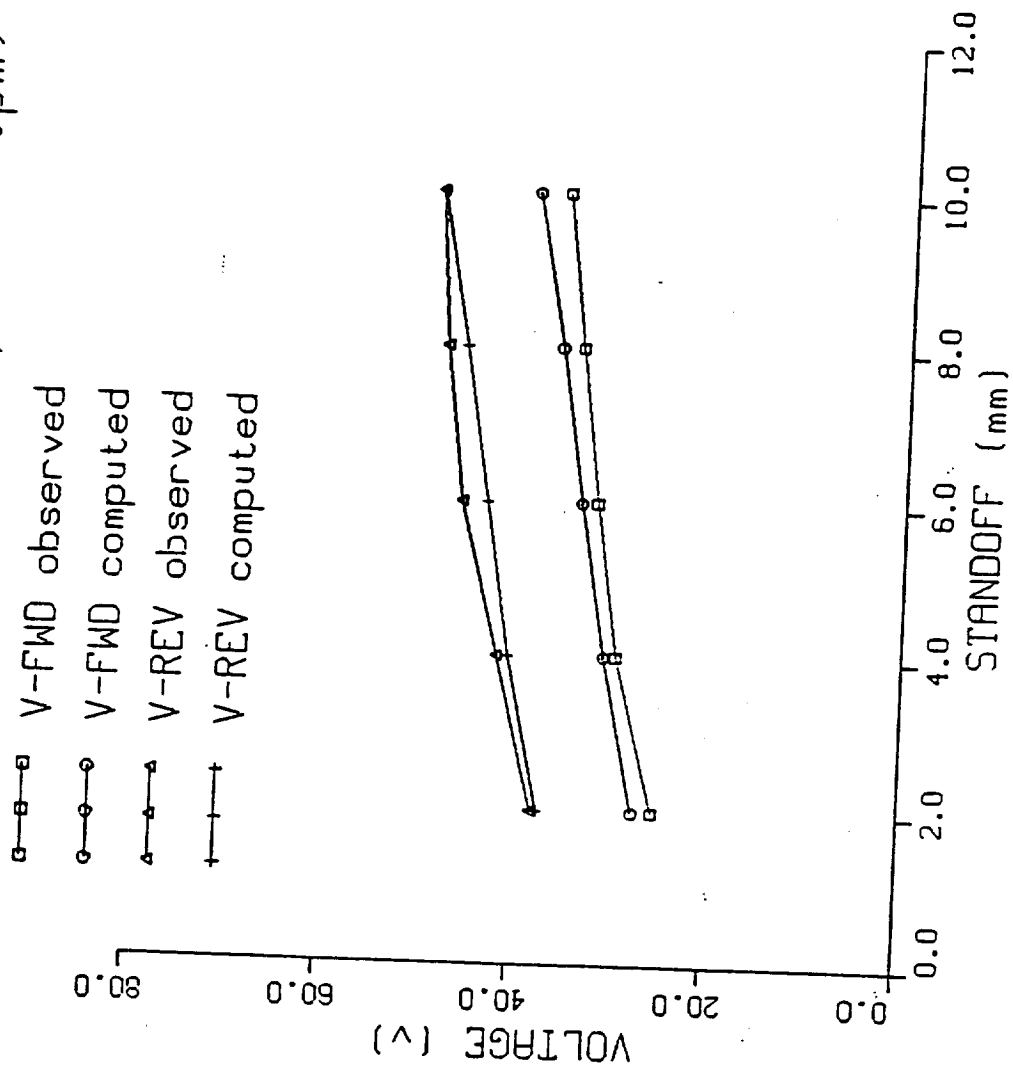


Fig. H-15

VOLTAGE (1/4" AL. L3=2mm)

- V-FWD observed
- V-FWD computed
- △-△-△ V-REV observed
- + + + V-REV computed

0101
0102
0103

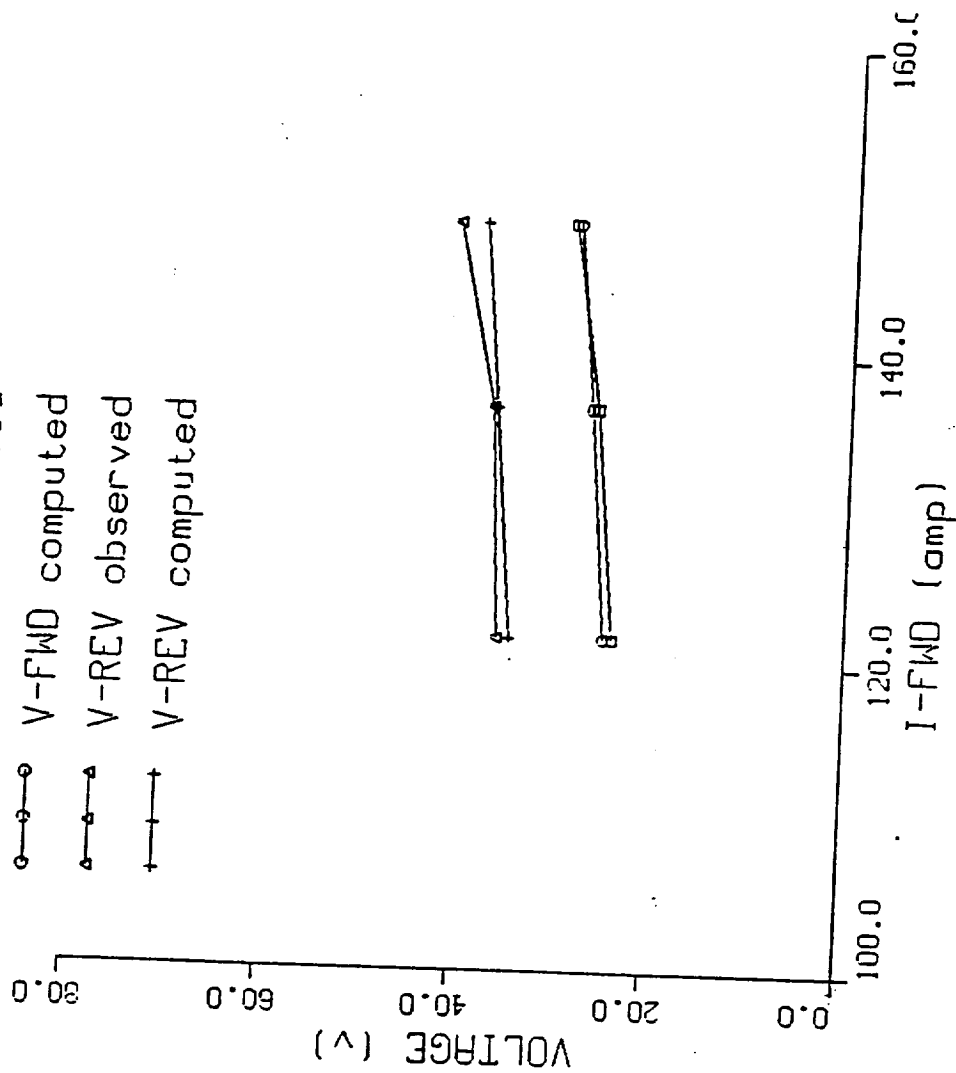


Fig. H-16

VOLTAGE (1/4" AL. L3=4mm)

- V-FWD observed
- V-FWD computed
- △-△-△ V-REV observed
- + + + V-REV computed

0104
0105
0106

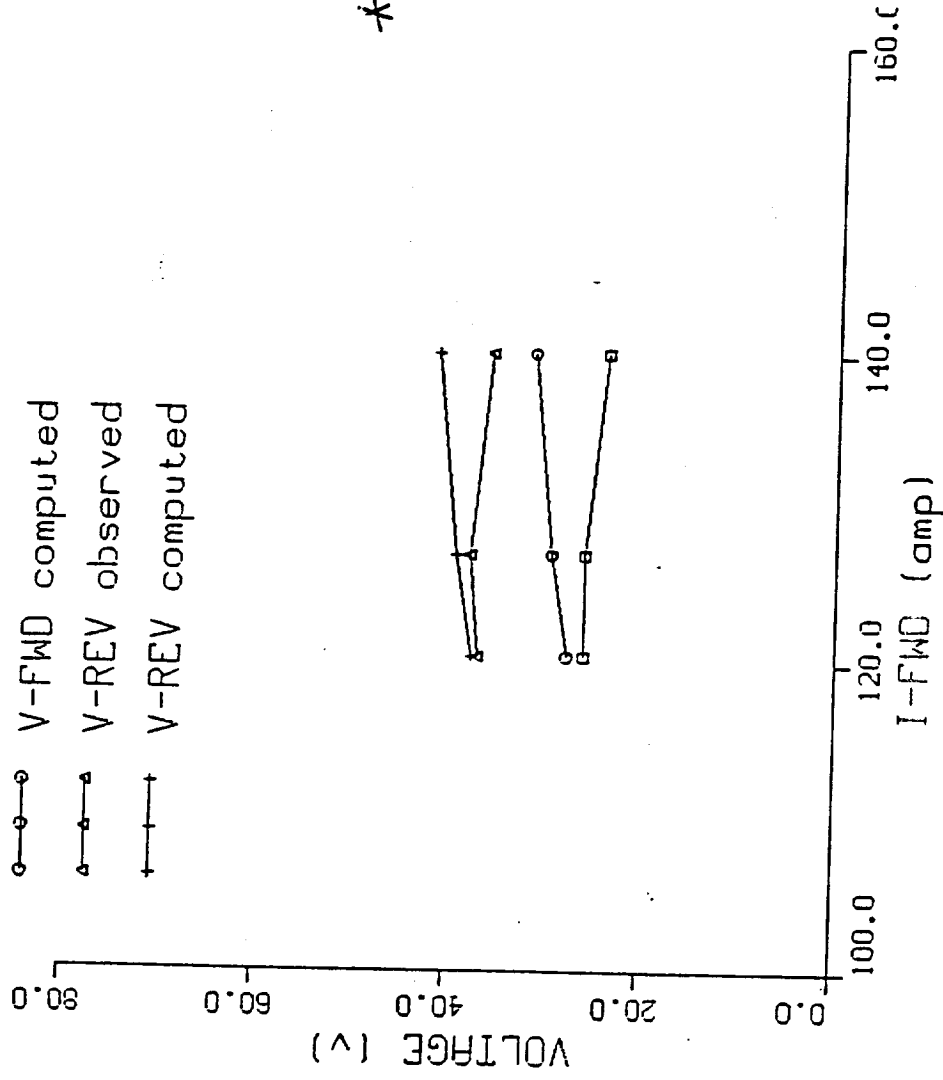
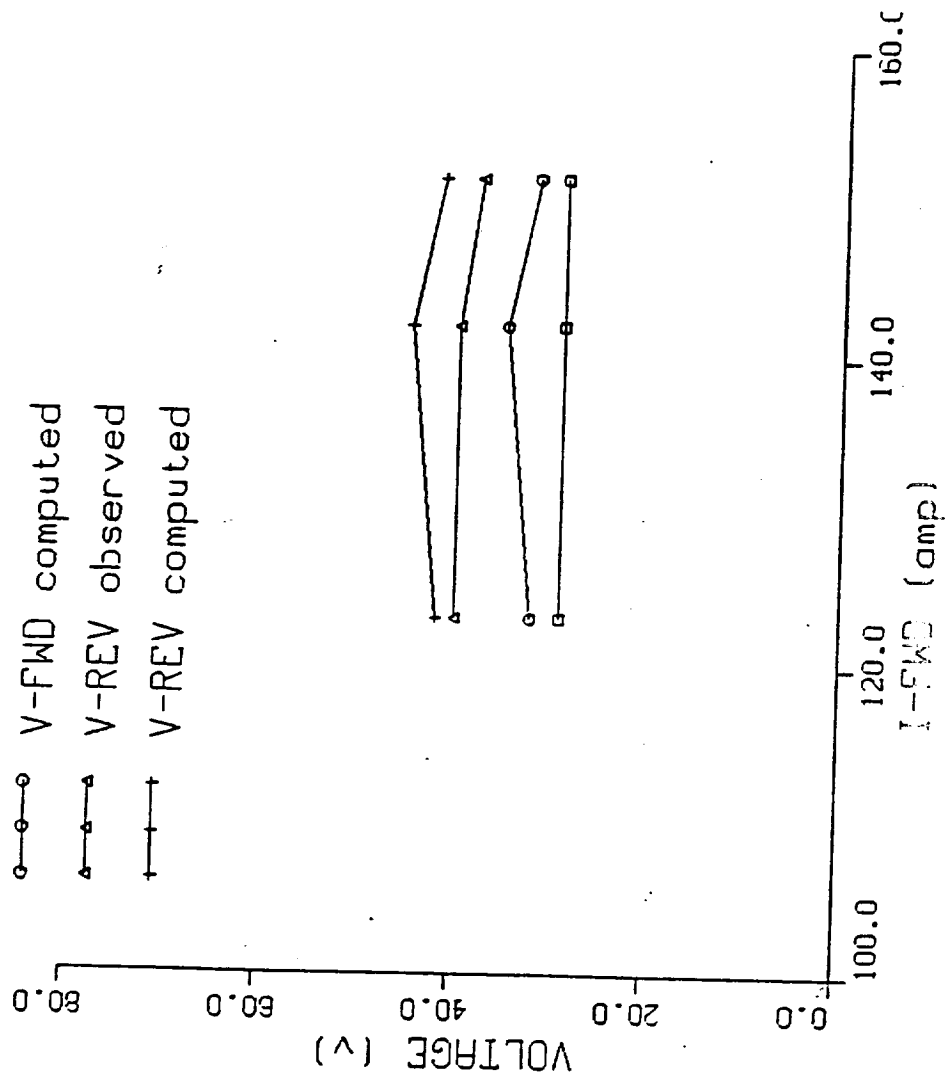


Fig. H-17

VOLTAGE (1/4" AL. L3=6mm)

- V-FWD observed
- V-FWD computed
- △-△-△ V-REV observed
- + + + V-REV computed



0107-2
0108
0109

RU

Fig. 1-13

VOLTAGE (1/4" AL. L3=2mm)

- V-FWD observed
- V-FWD computed
- △-△-△ V-REV observed
- + + + V-REV computed

0110-2
0111-2
0112

XU
ED

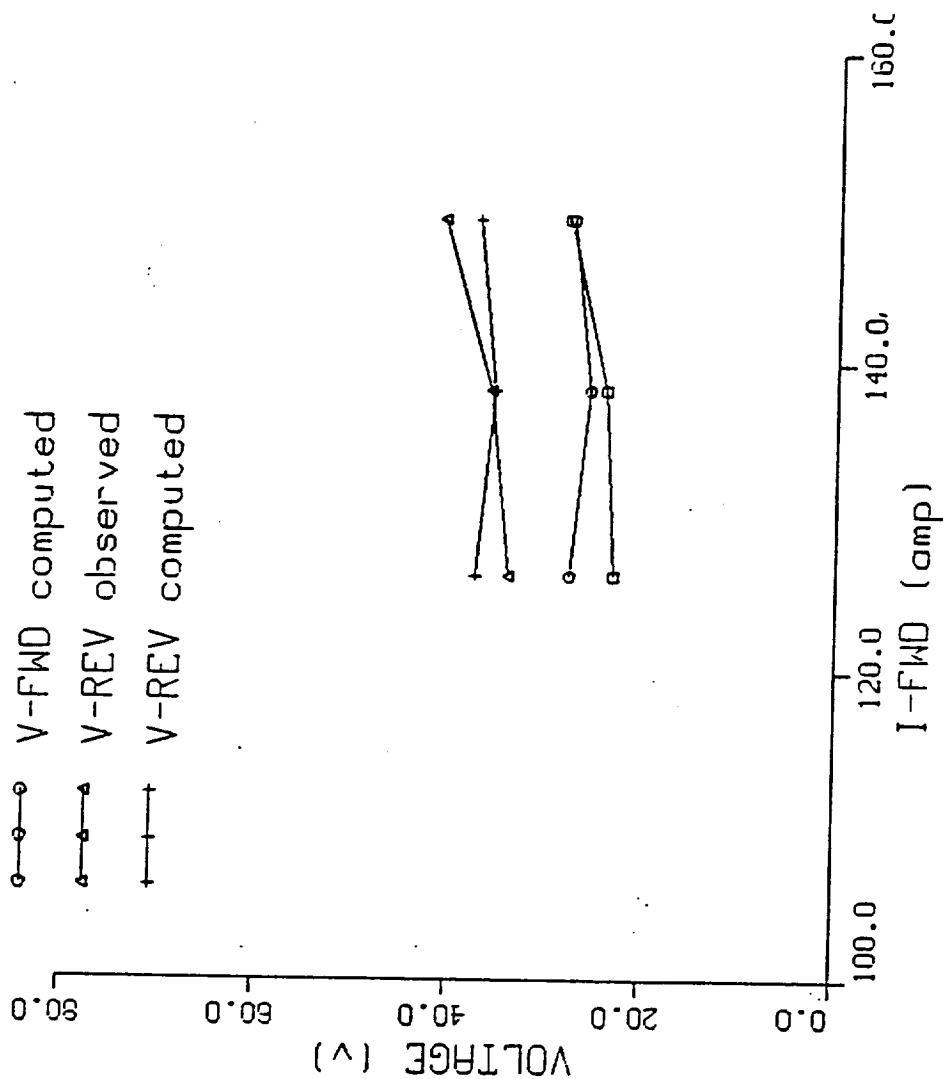


Fig. H-19

VOLTAGE (1/4" AL. L3=4mm)

- V-FWD observed
- V-FWD computed
- △-△-△ V-REV observed
- + + + V-REV computed

0113-2
0114-2
0115-

Ru
Lu

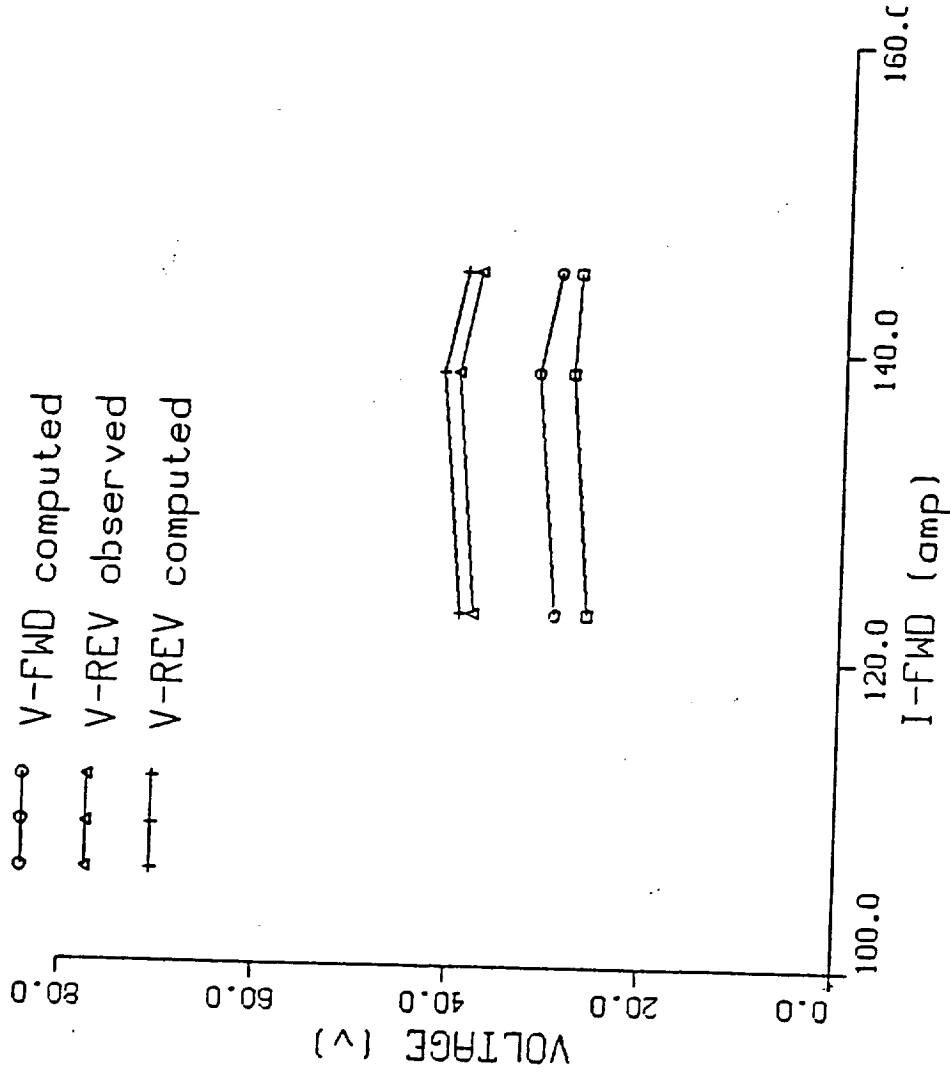


Fig. H-20

VOLTAGE (1/4" AL. L3=6mm)

□-□-□ V-FWD observed
 ○-○-○ V-FWD computed
 △-△-△ V-REV observed
 + + + V-REV computed

0116
 0117-3
 0118

* Bad strip
 Chart

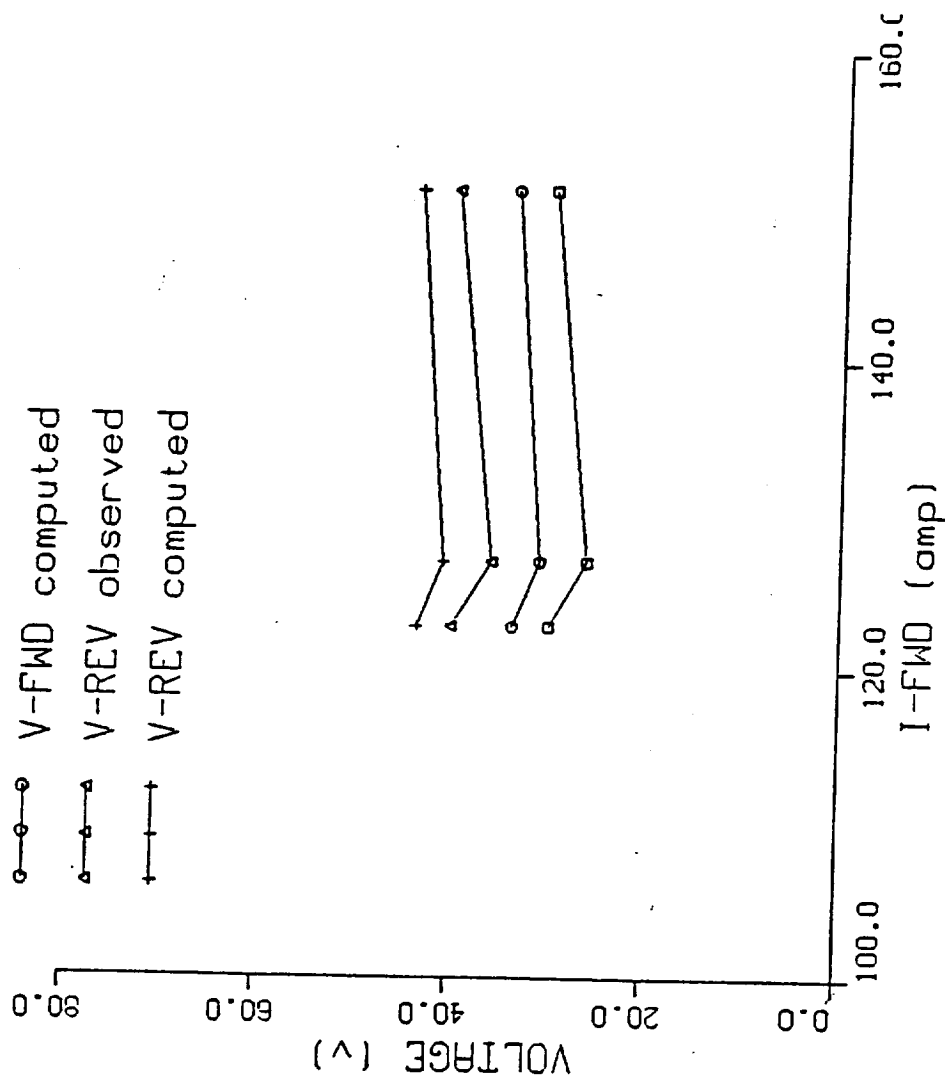
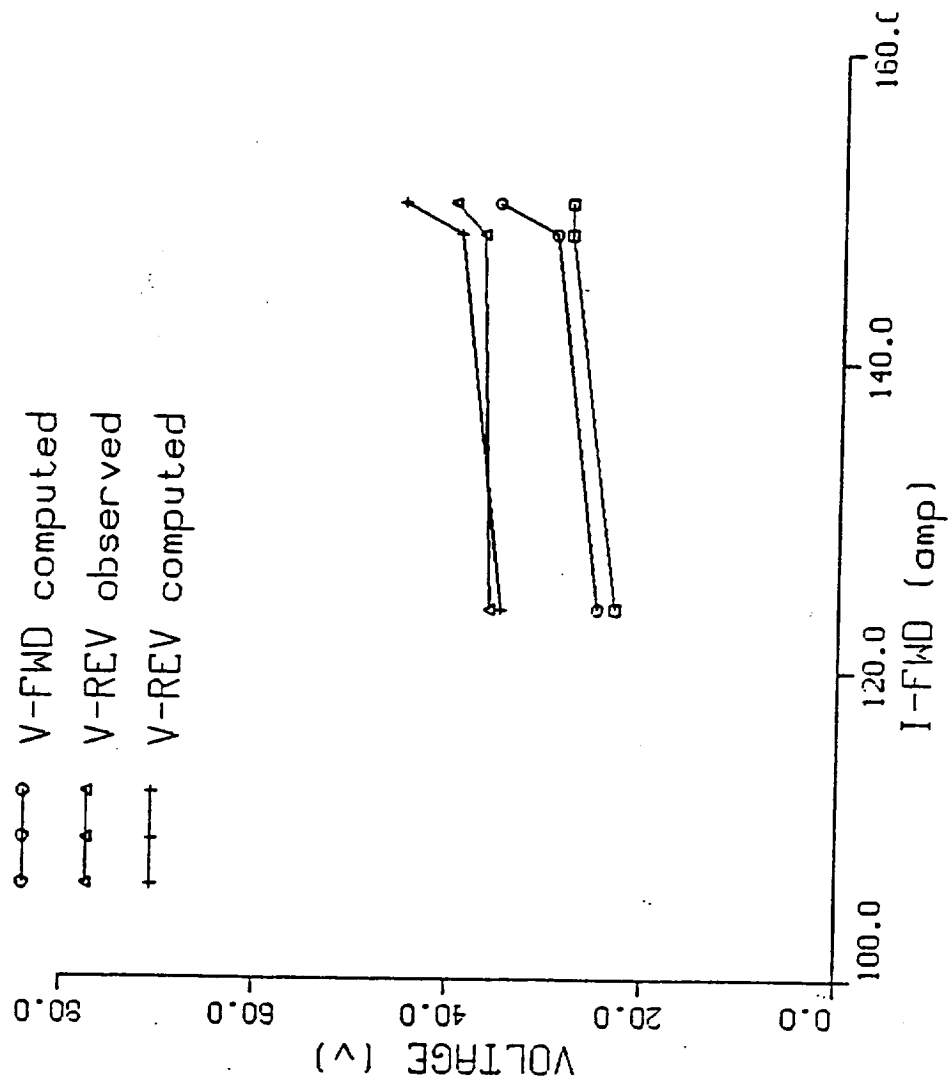


Fig. H-21

VOLTAGE (1/4' AL. CONFIRM. TEST)

- V-FWD observed
- V-FWD computed
- V-REV observed
- V-REV computed



0126
0119-A
0123

ED

Fig. H-22

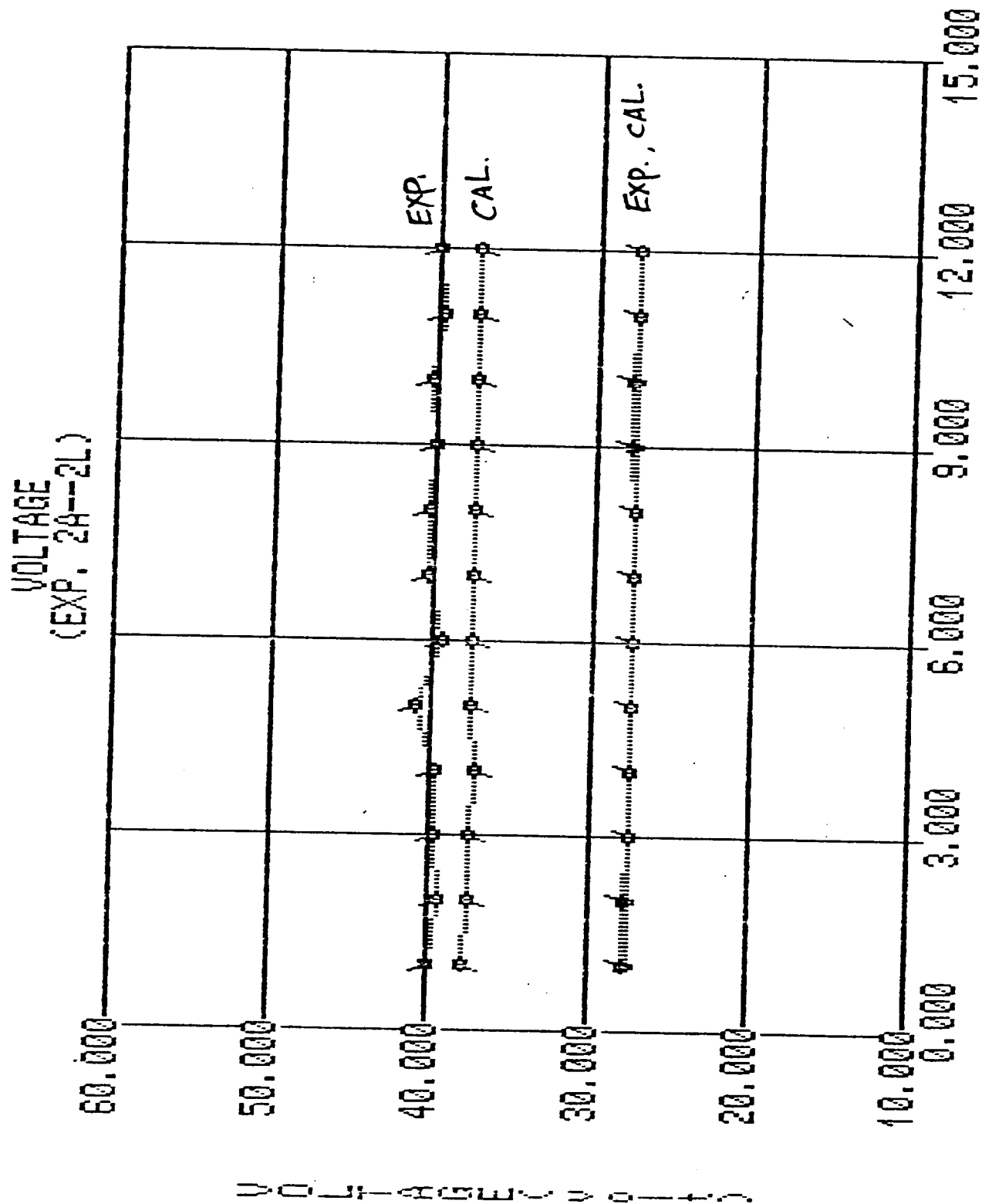


Fig. H-23

VOLTAGE
(EXP. 2M--2V)

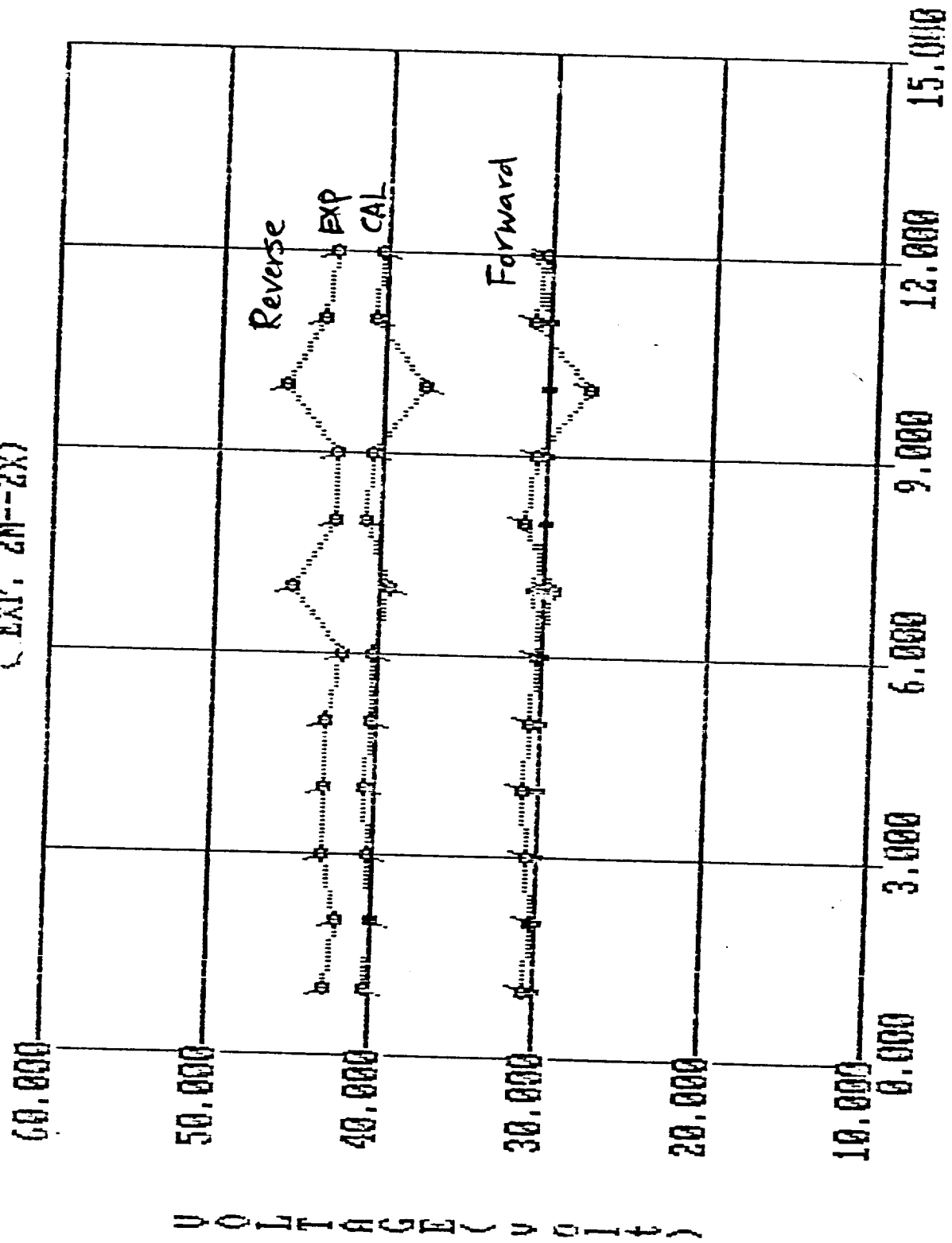


Fig. H-24

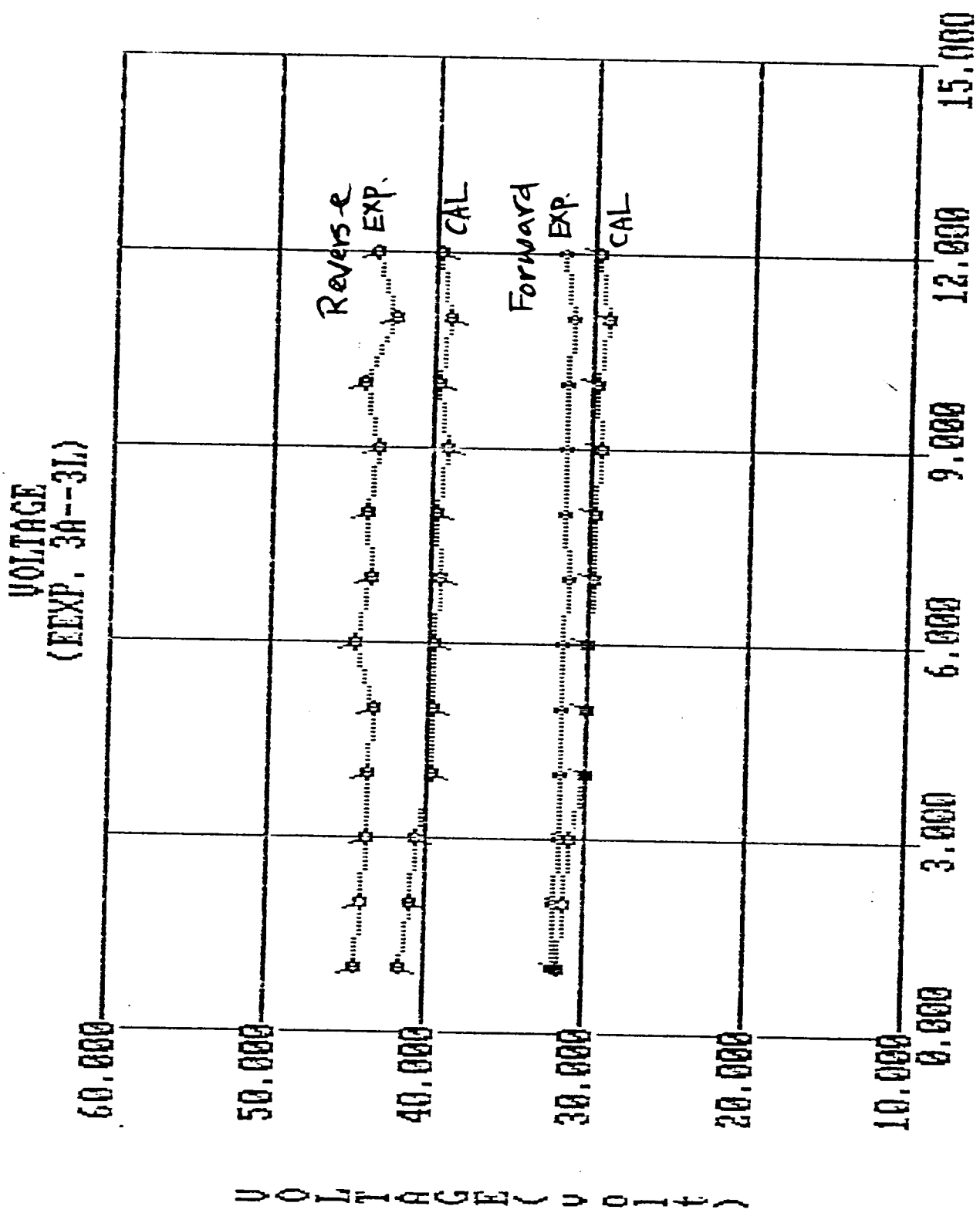


Fig. H-25

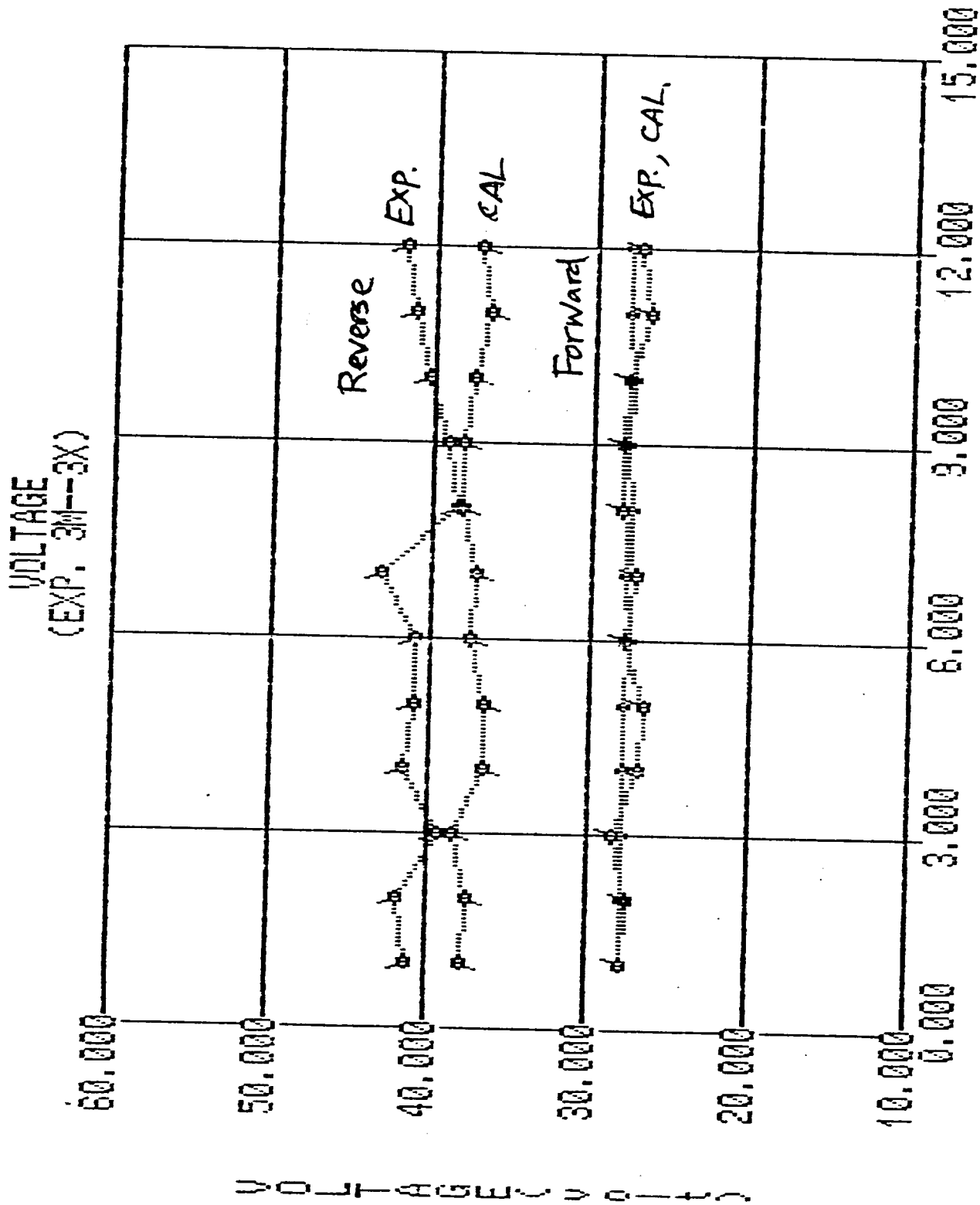


Fig. H-26

VOLTAGE (EXP. 4A--4C)

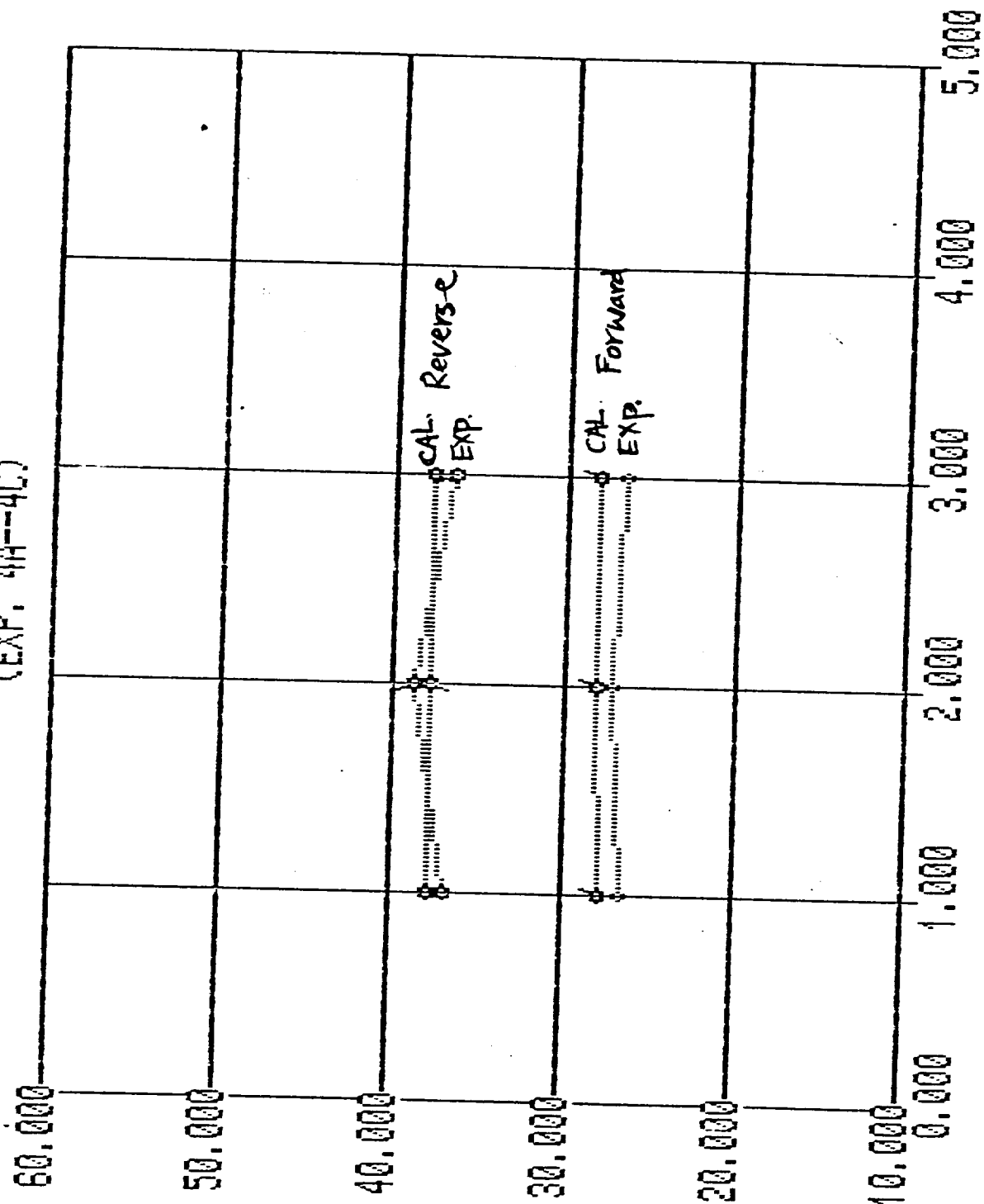


Fig. H-27

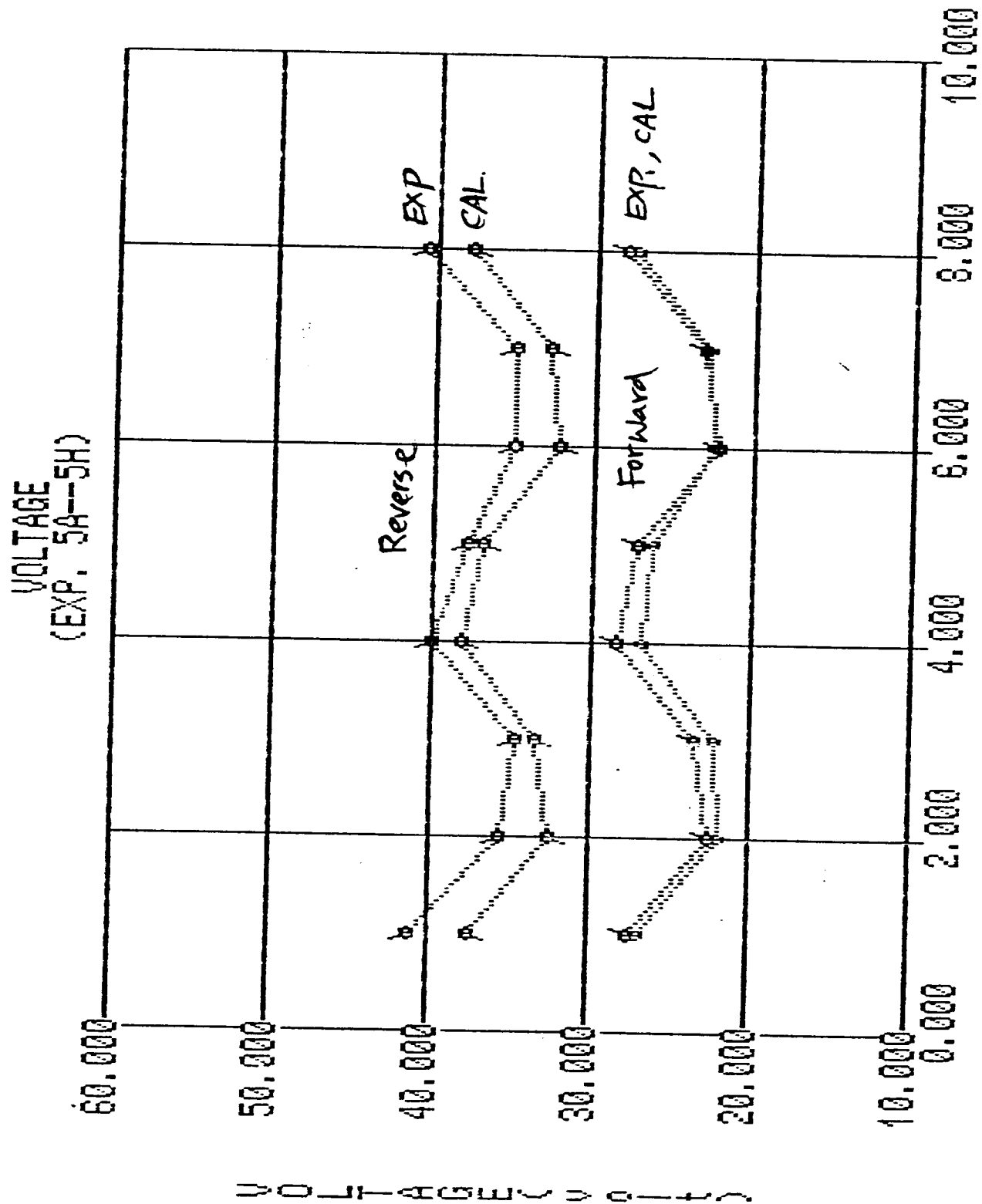


Fig. H-28

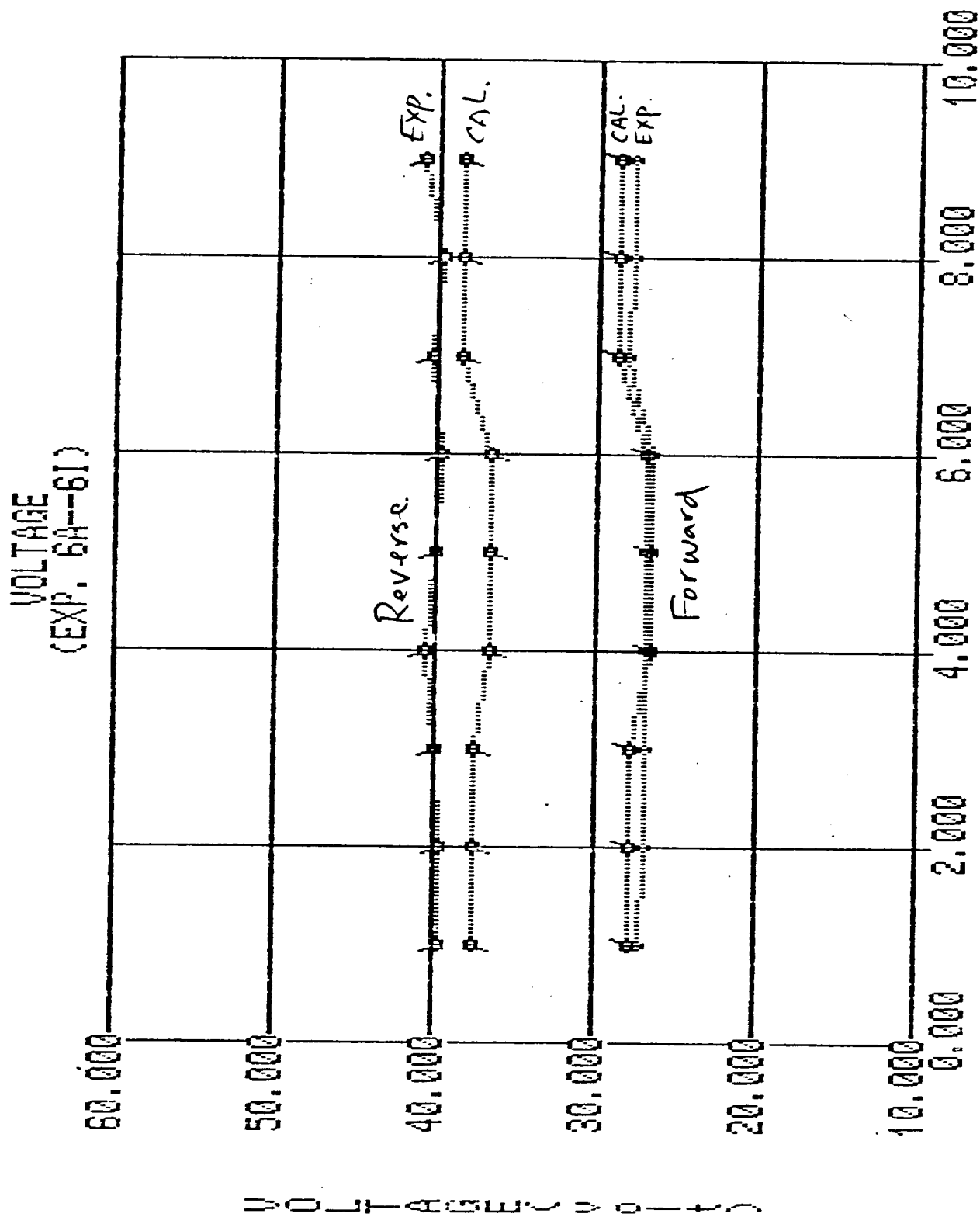


Fig. H-29

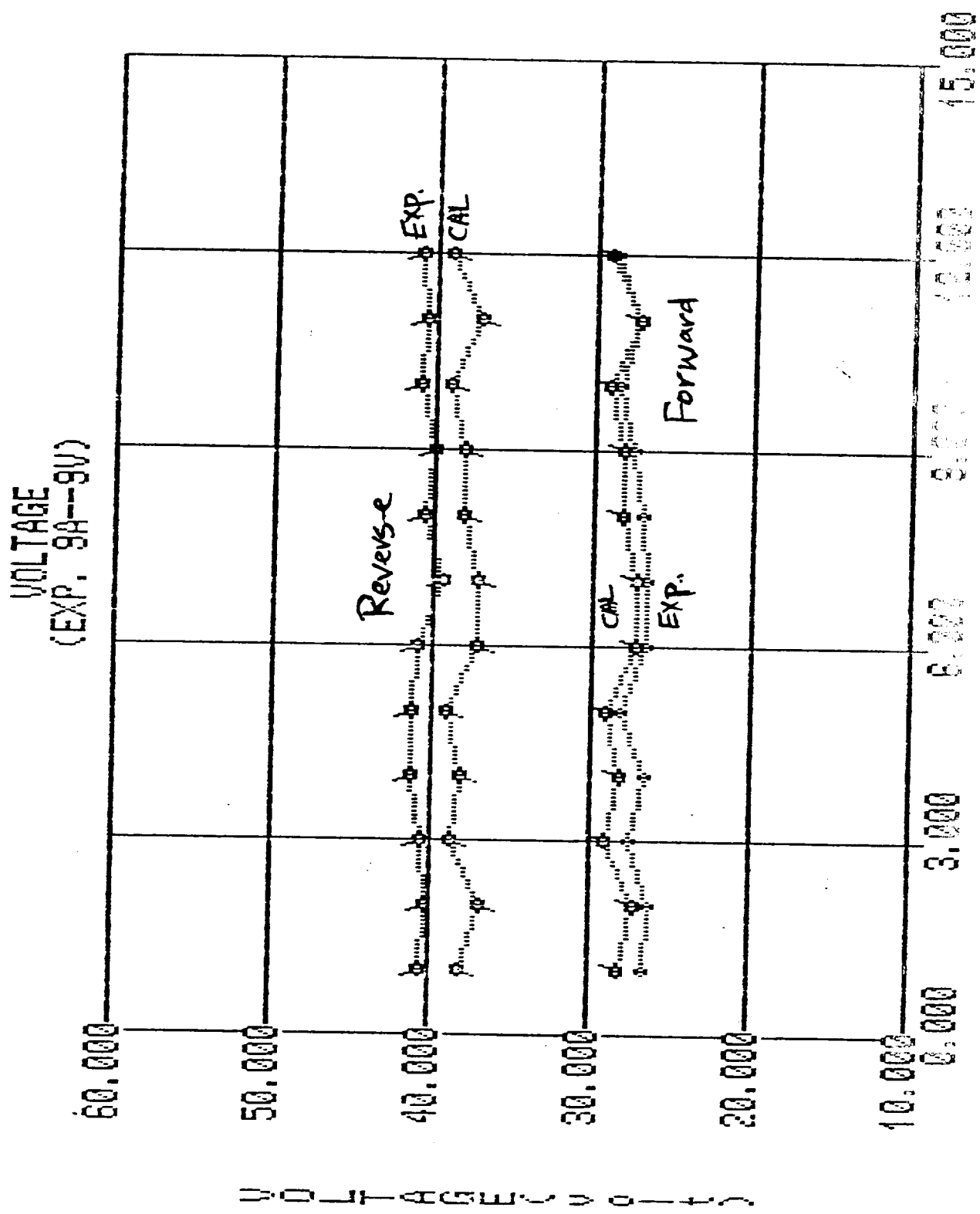


Fig. H-30

VOLTAGE (EXP. 9AA--9AV)

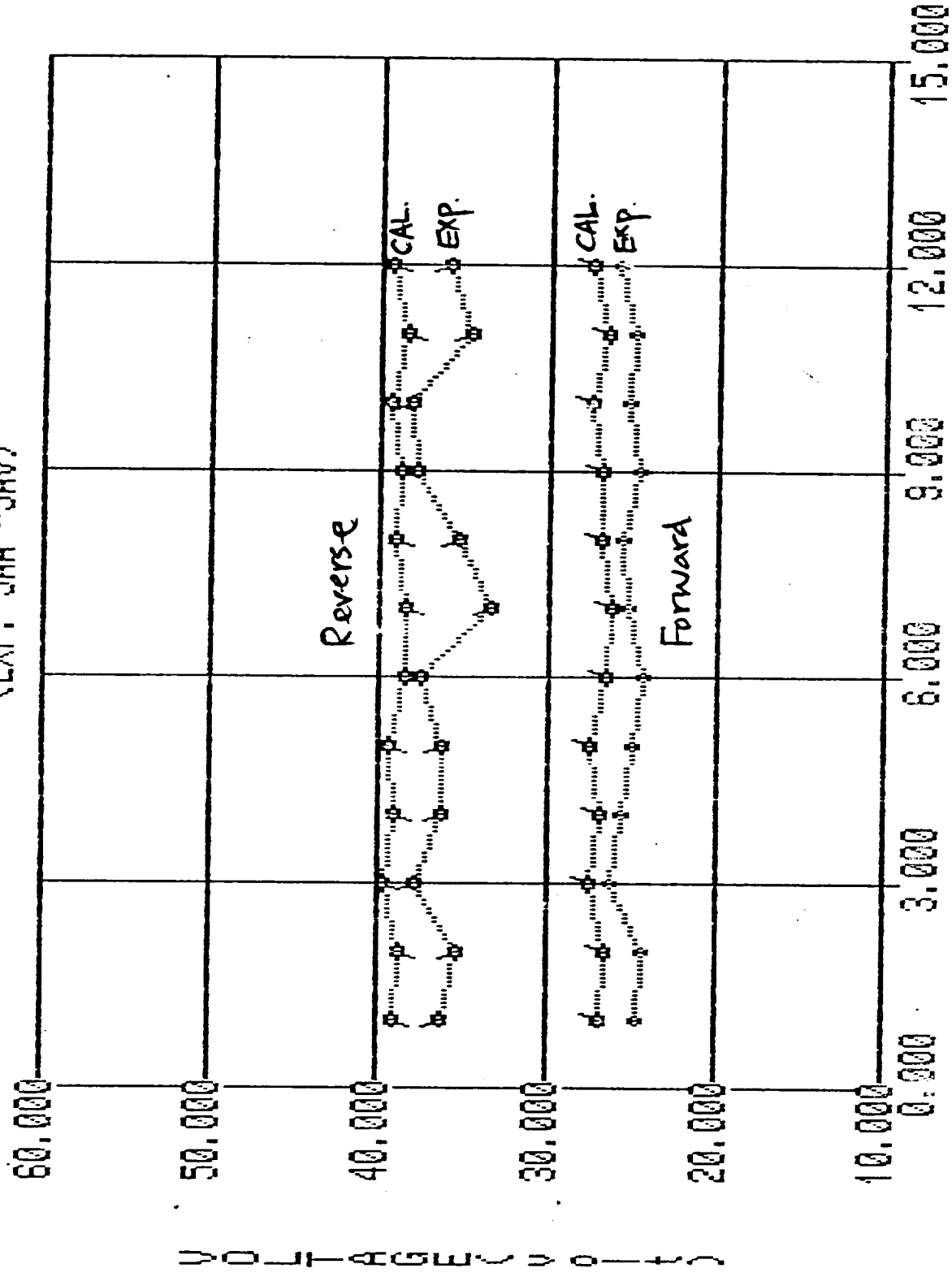


Fig. H-31

LEADING EDGE ANGLE (EXP. 2A---2L)

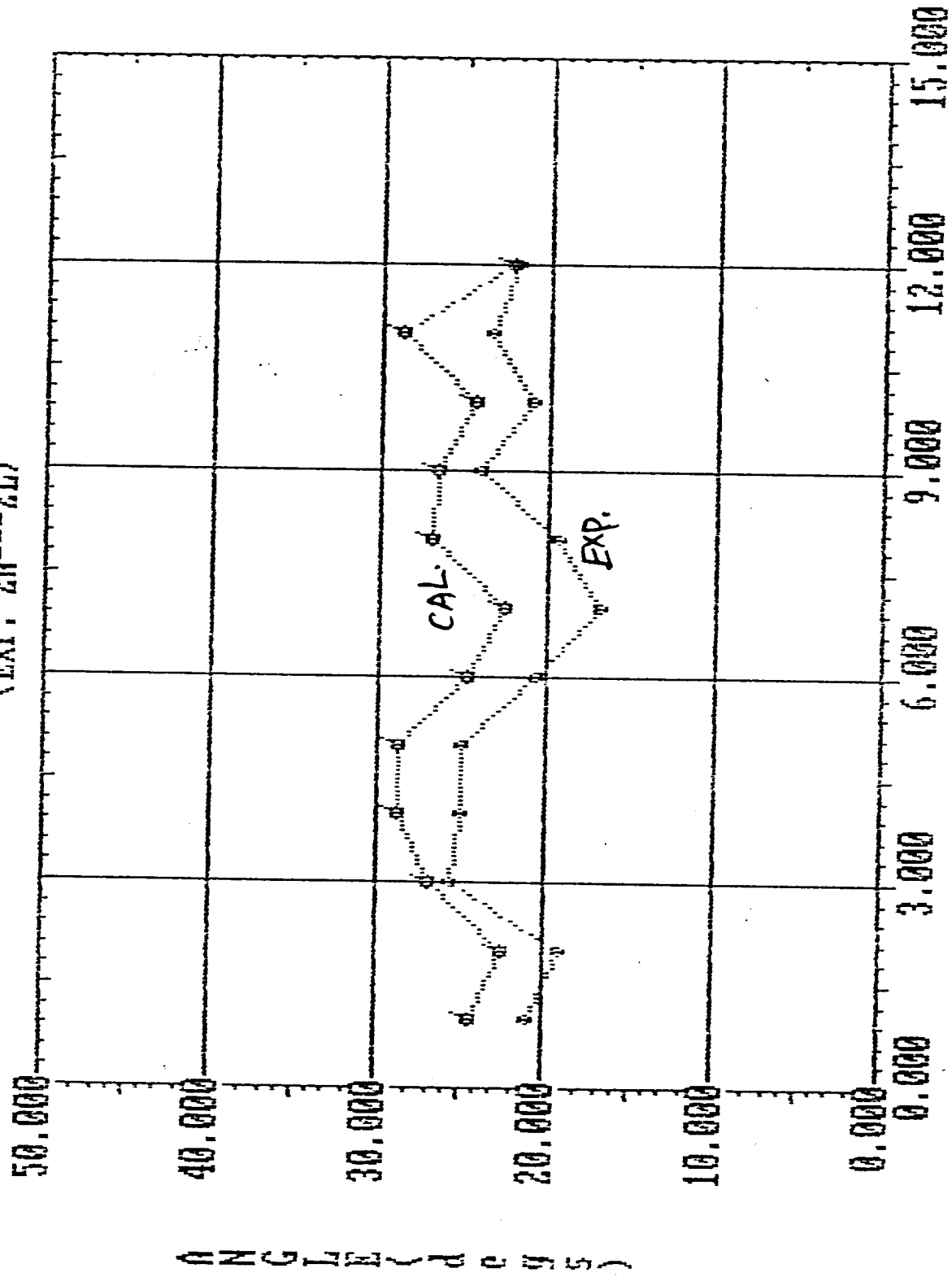


Fig. H-32

LEADING EDGE ANGLE
(EXP. 2M---2X)

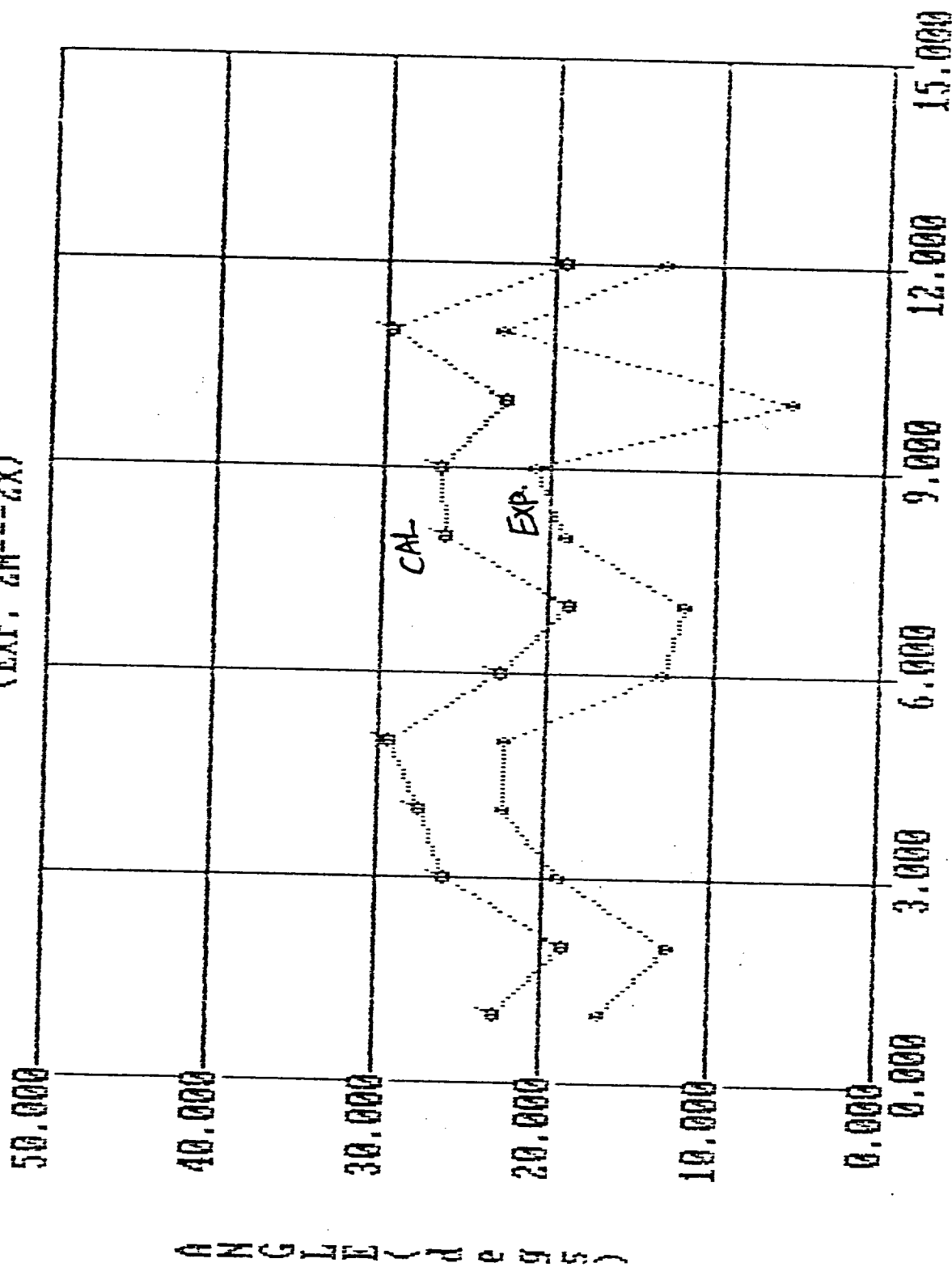


Fig. H-33

LEADING EDGE ANGLE (EXP. 3A---3L)

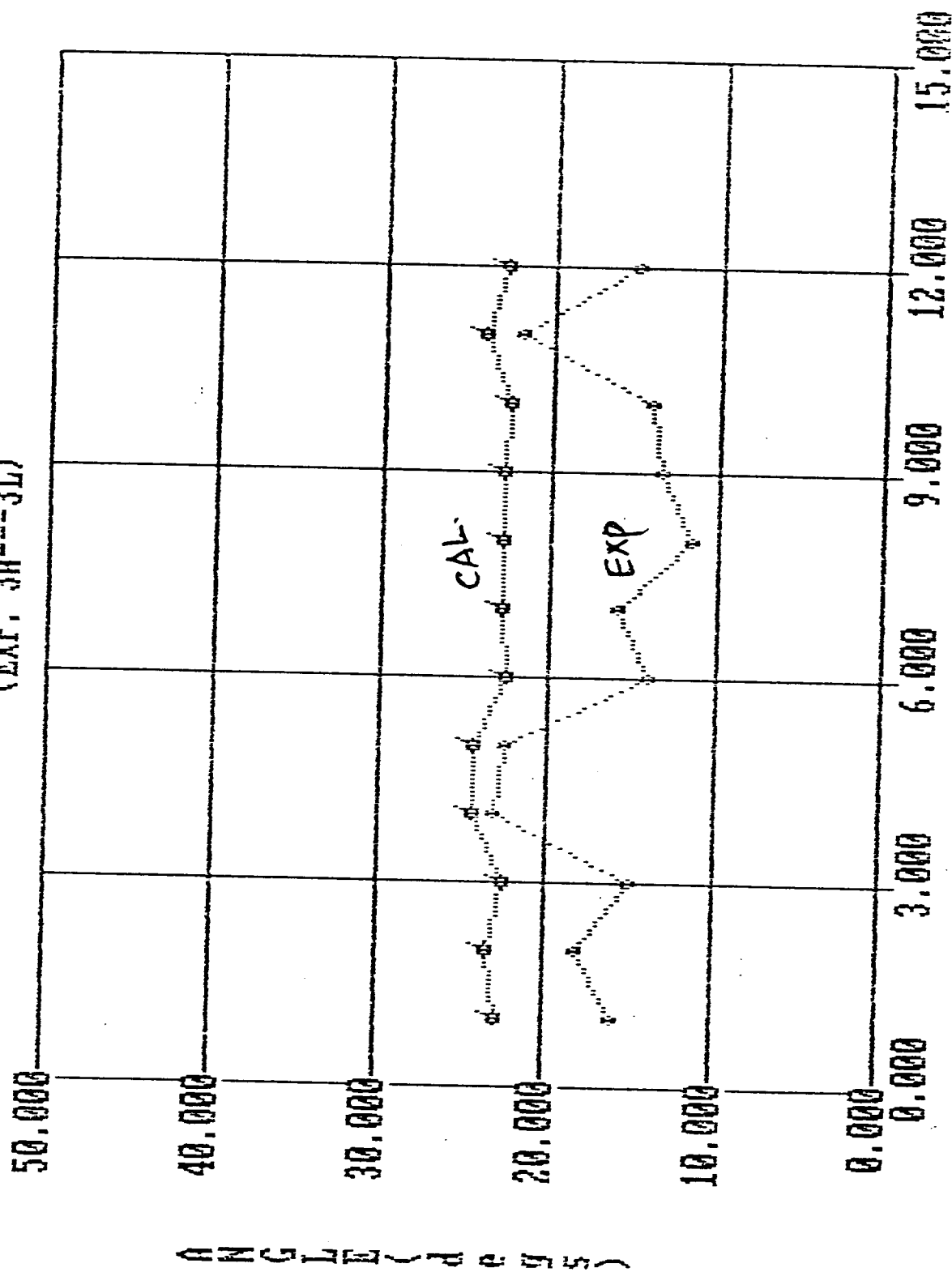


Fig. H-34

LEADING EDGE ANGLE (EXP. 3M---3X)

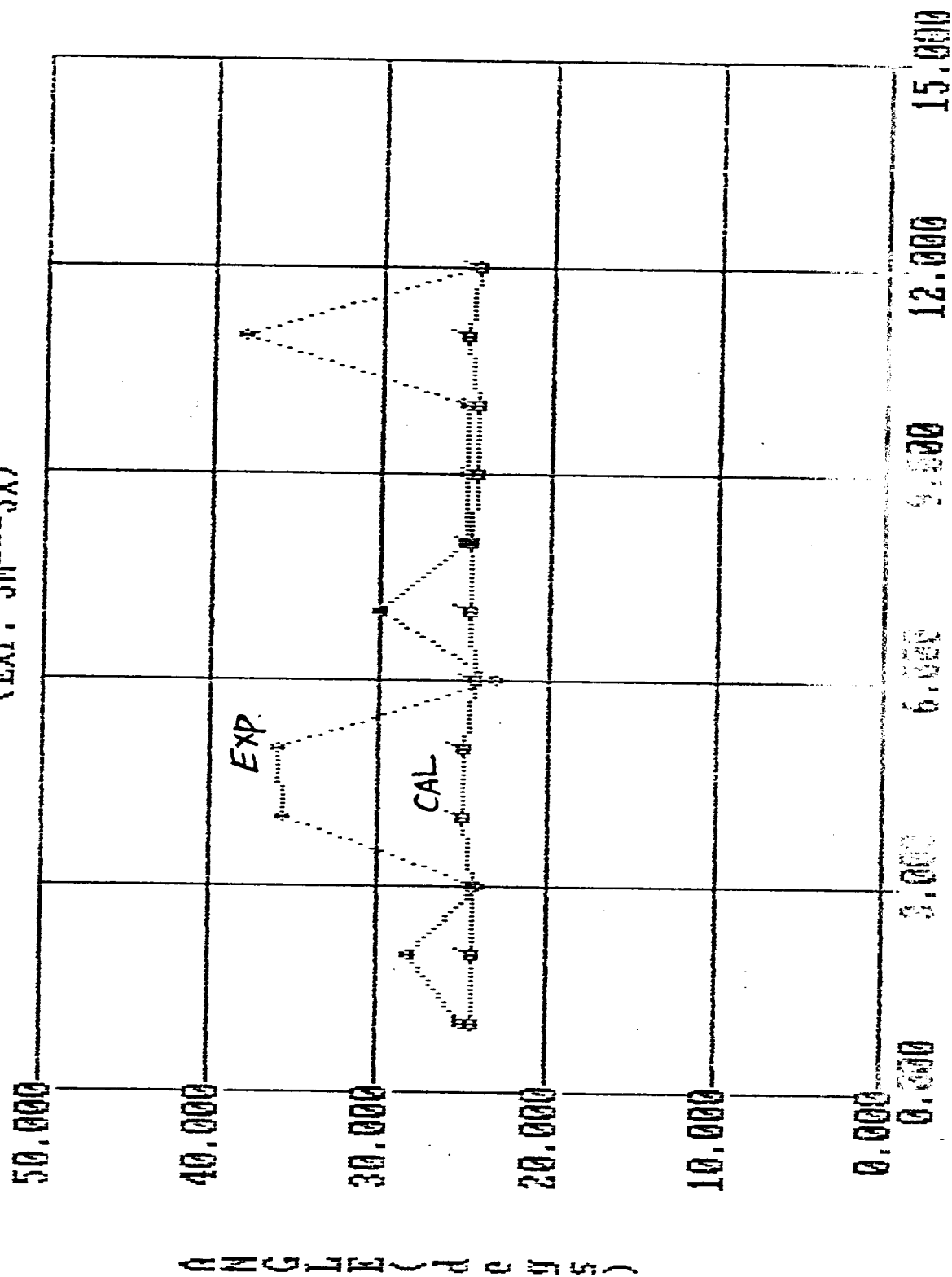


Fig. H-35

LEADING EDGE ANGLE (EXP. 40---4C)

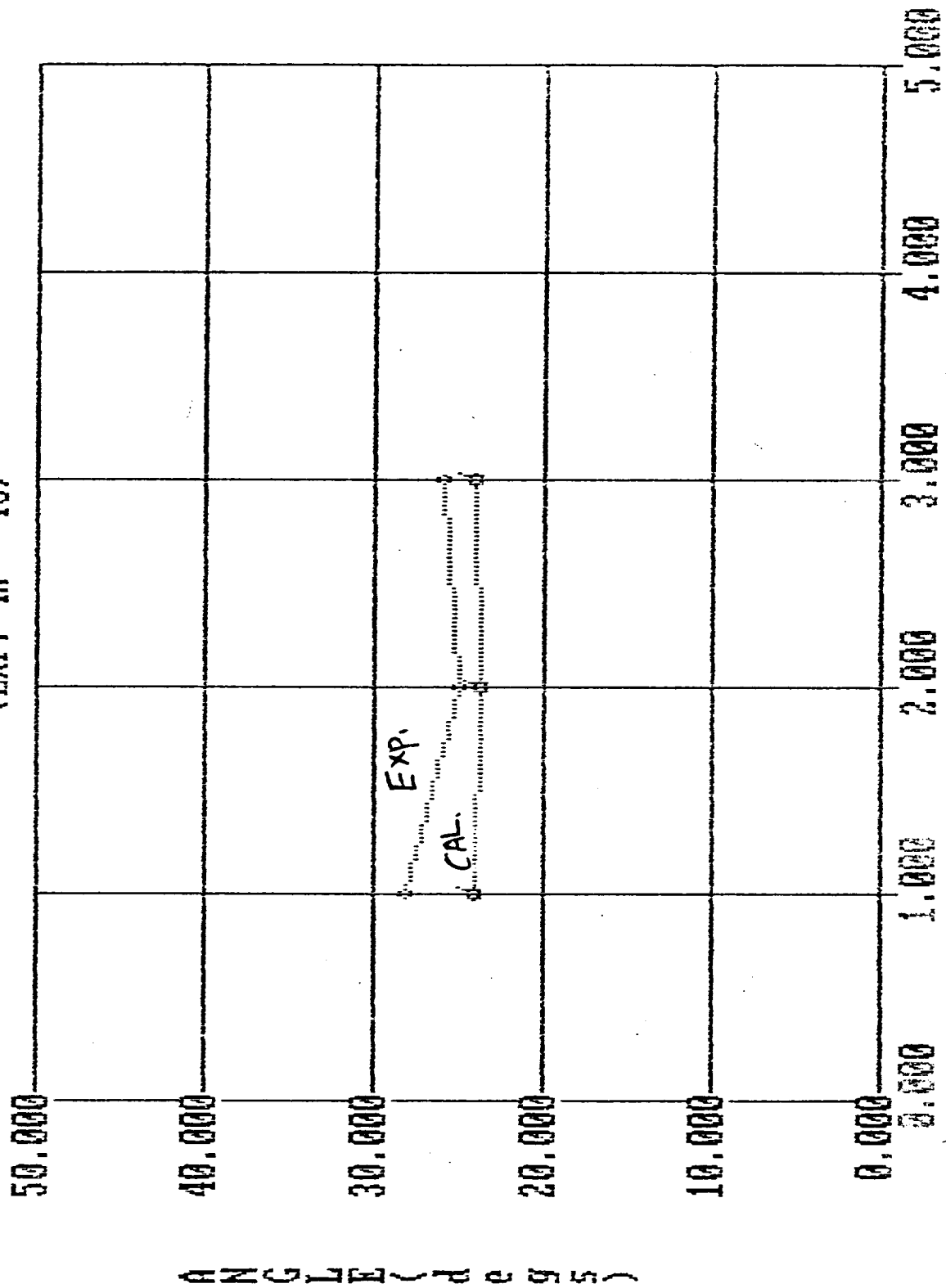


Fig. H-36

LEADING EDGE ANGLE (EXP. 5A---5H)

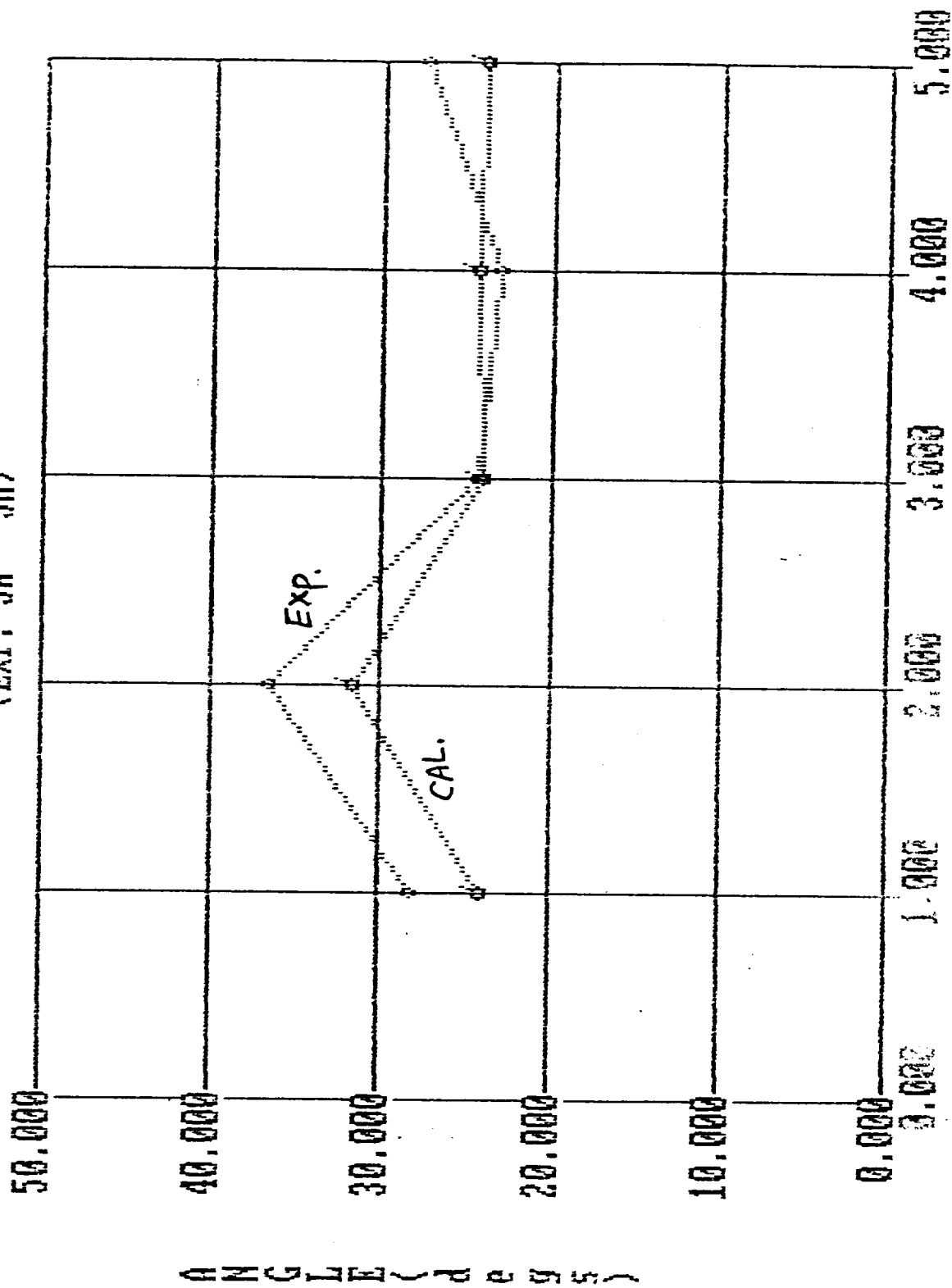


Fig. H-37

LEADING EDGE ANGLE
(EXP. 60---61)

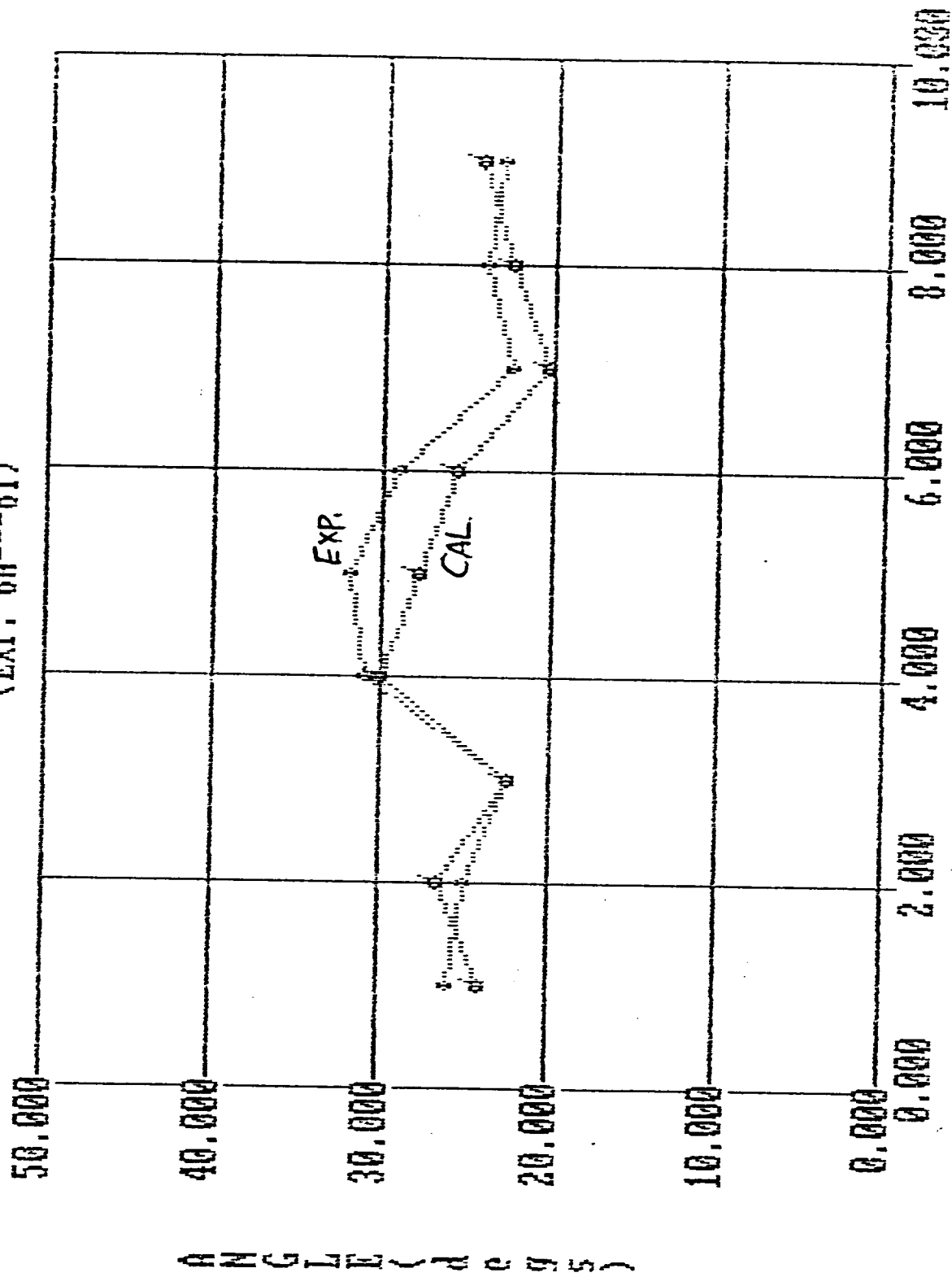


Fig. H-38

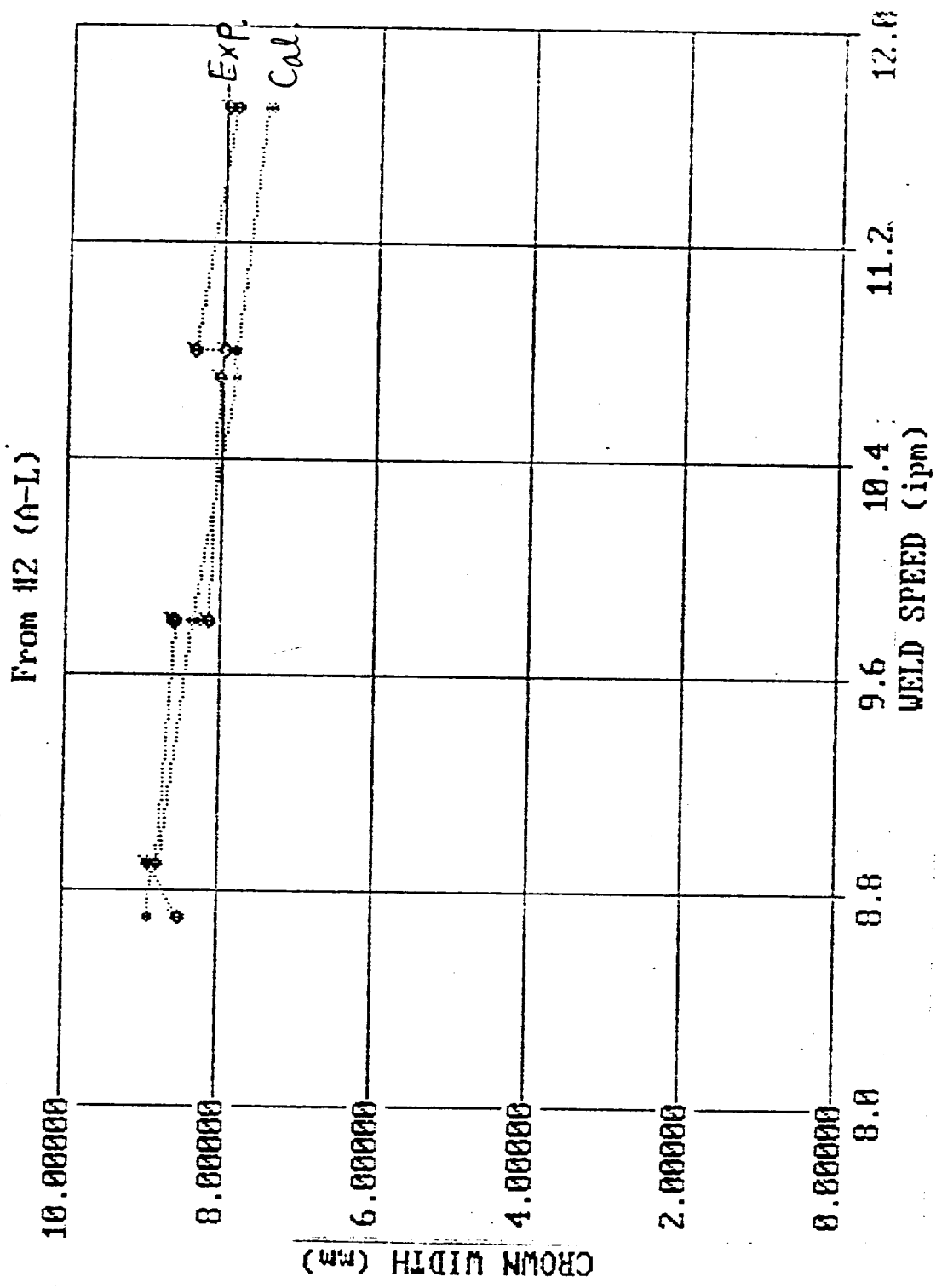


Fig. H-39

From #2 (A-L)

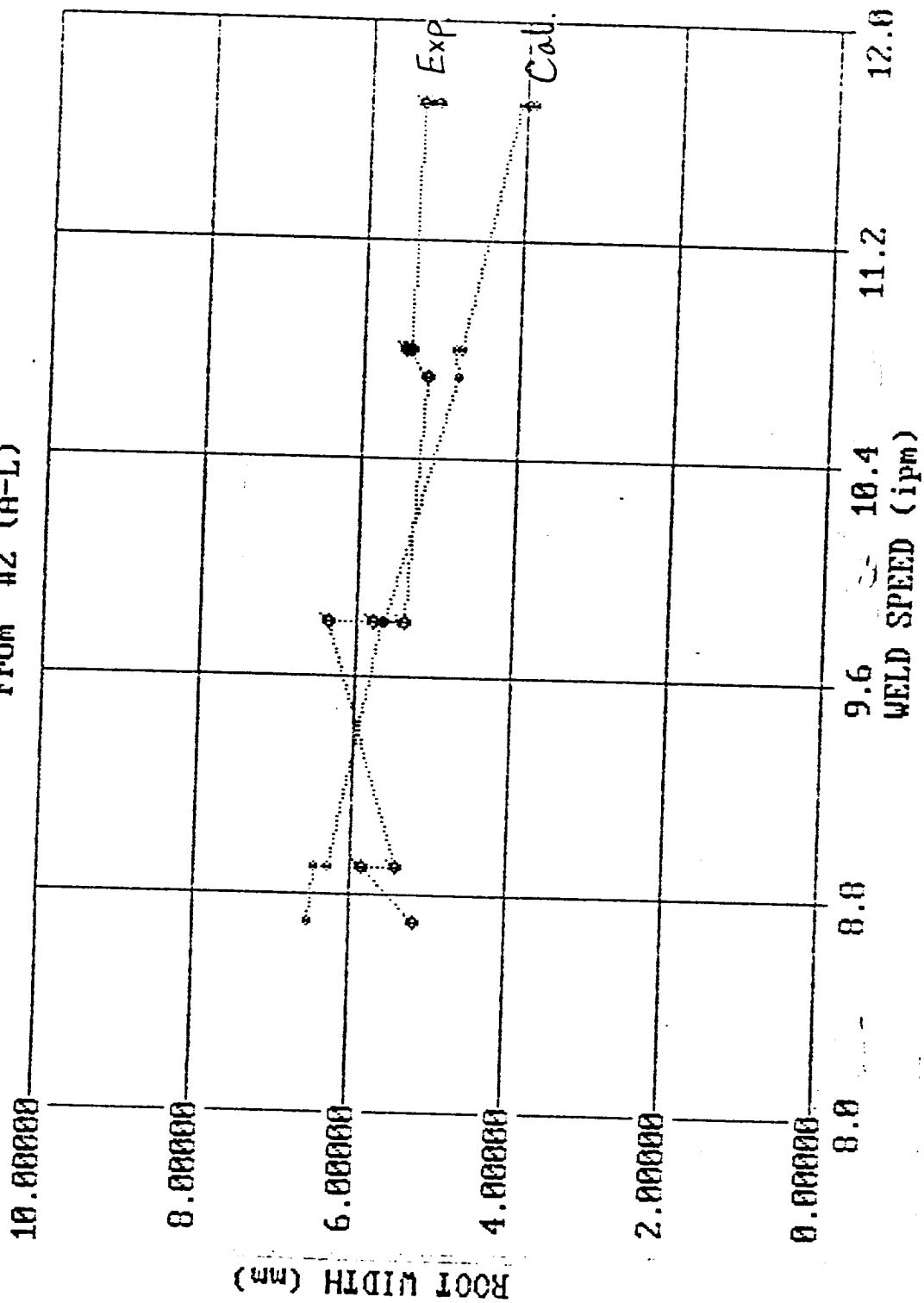


Fig. H-40

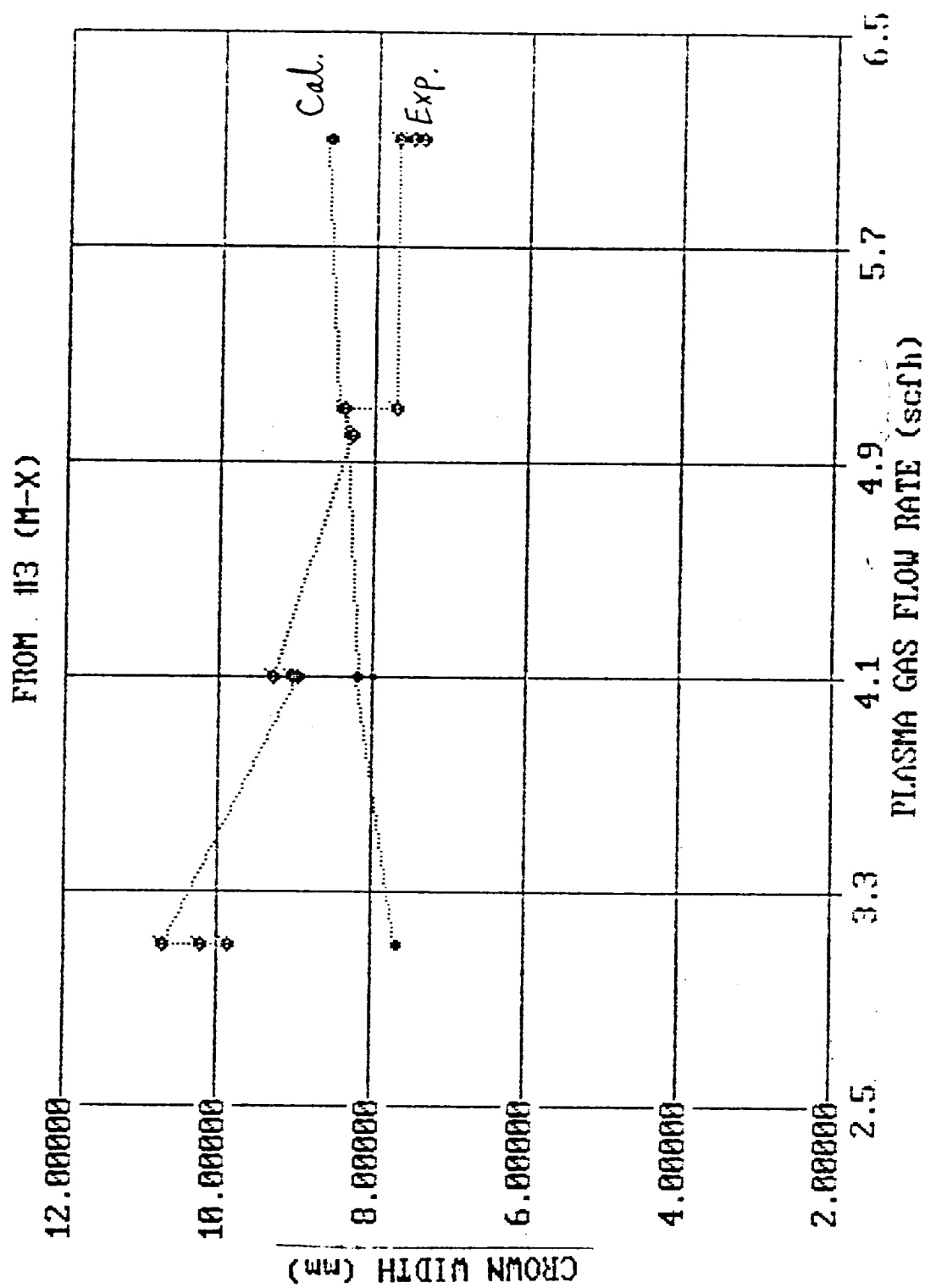


Fig. H-41

Fig. H-42

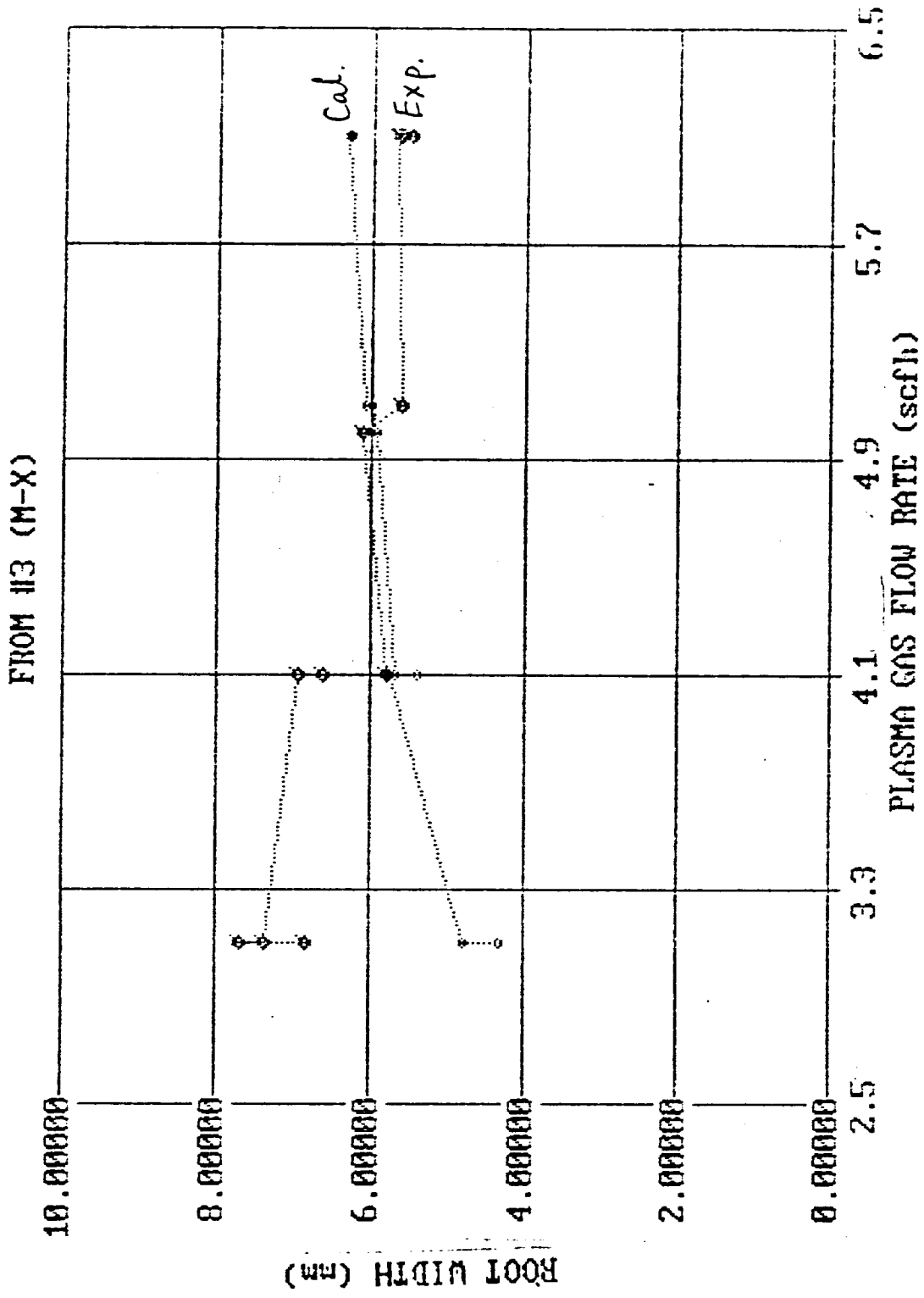


Fig. H-42

From #15 (A-B)

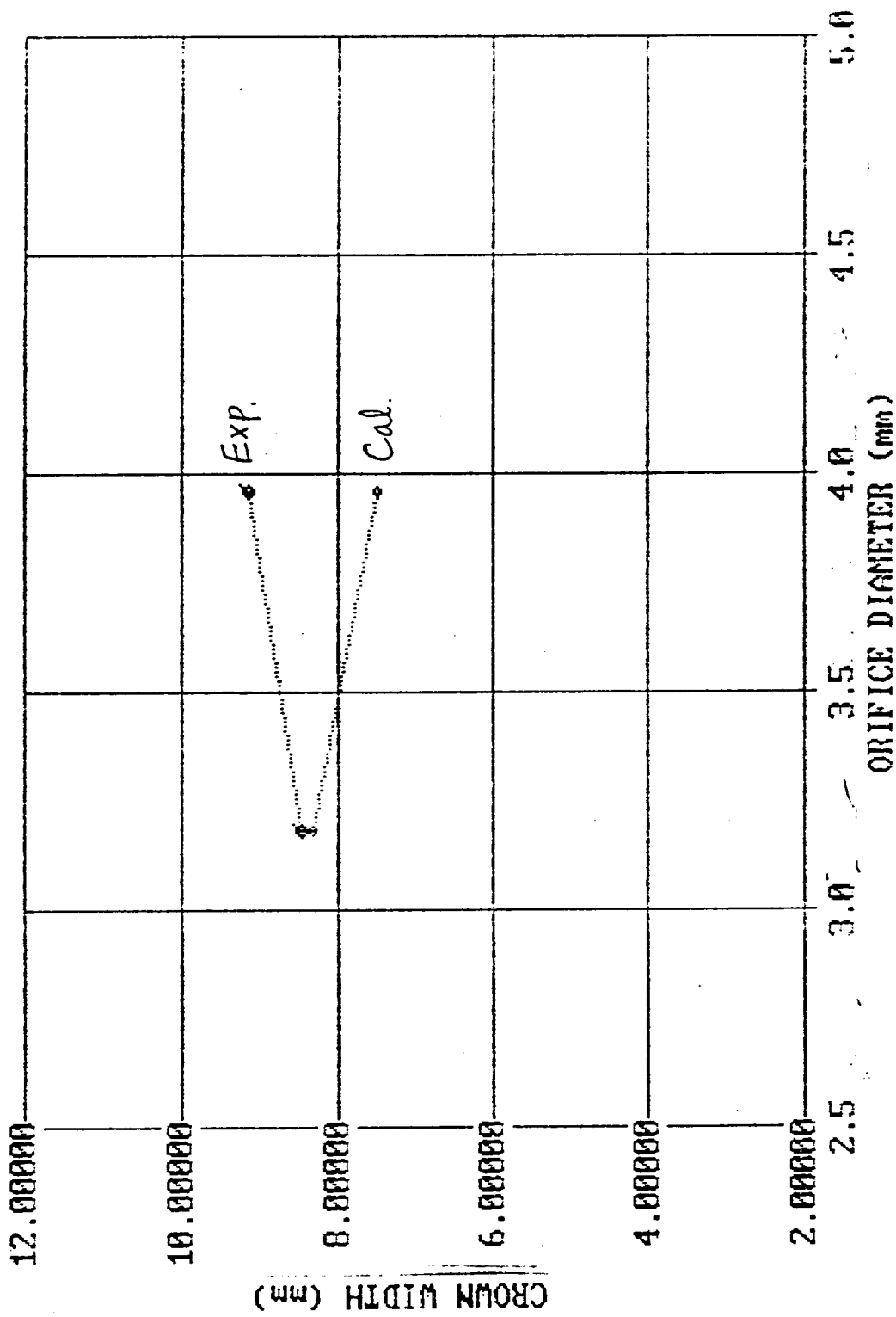


Fig. H-43

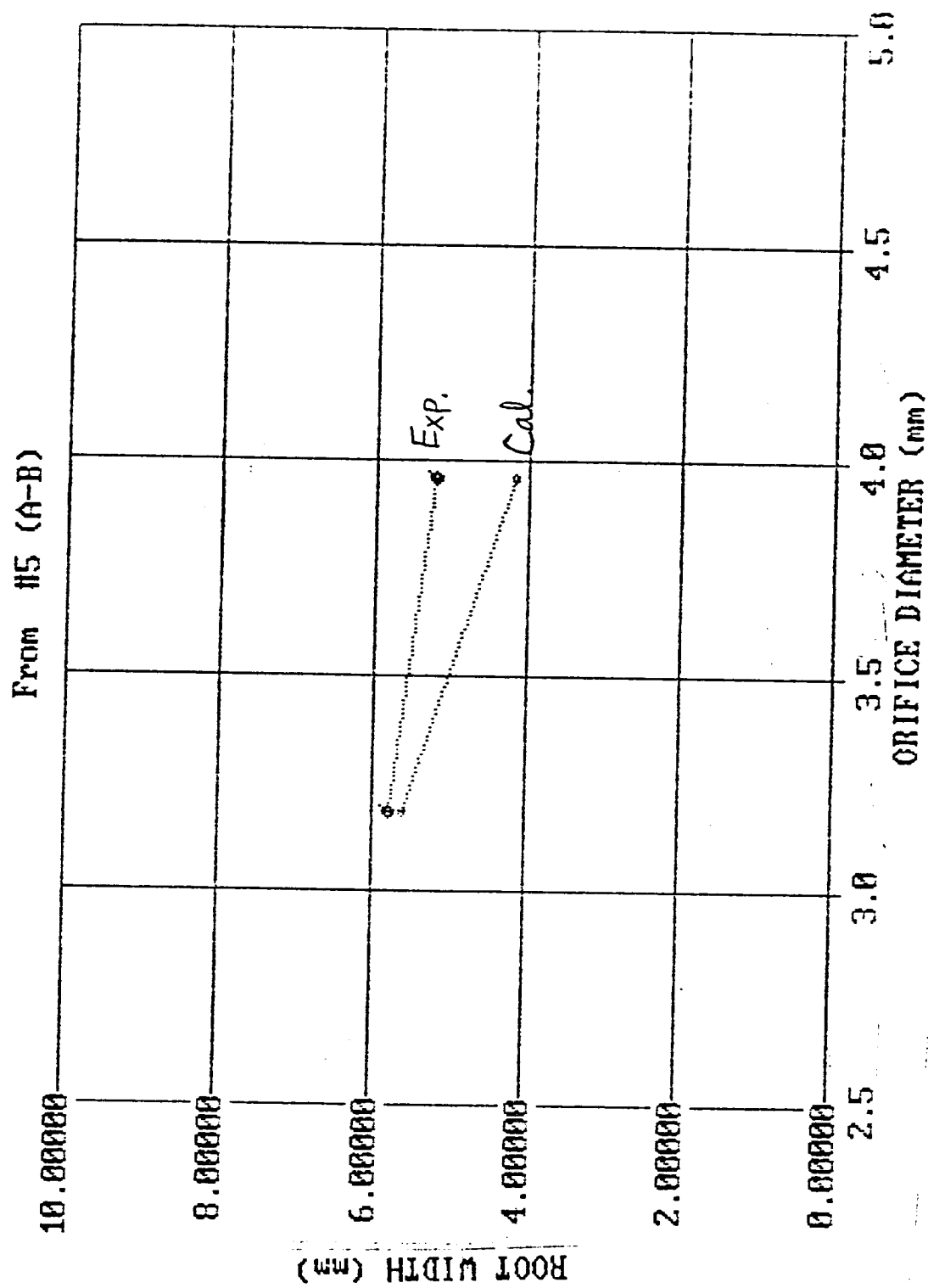


Fig. H-44

Fig H-45

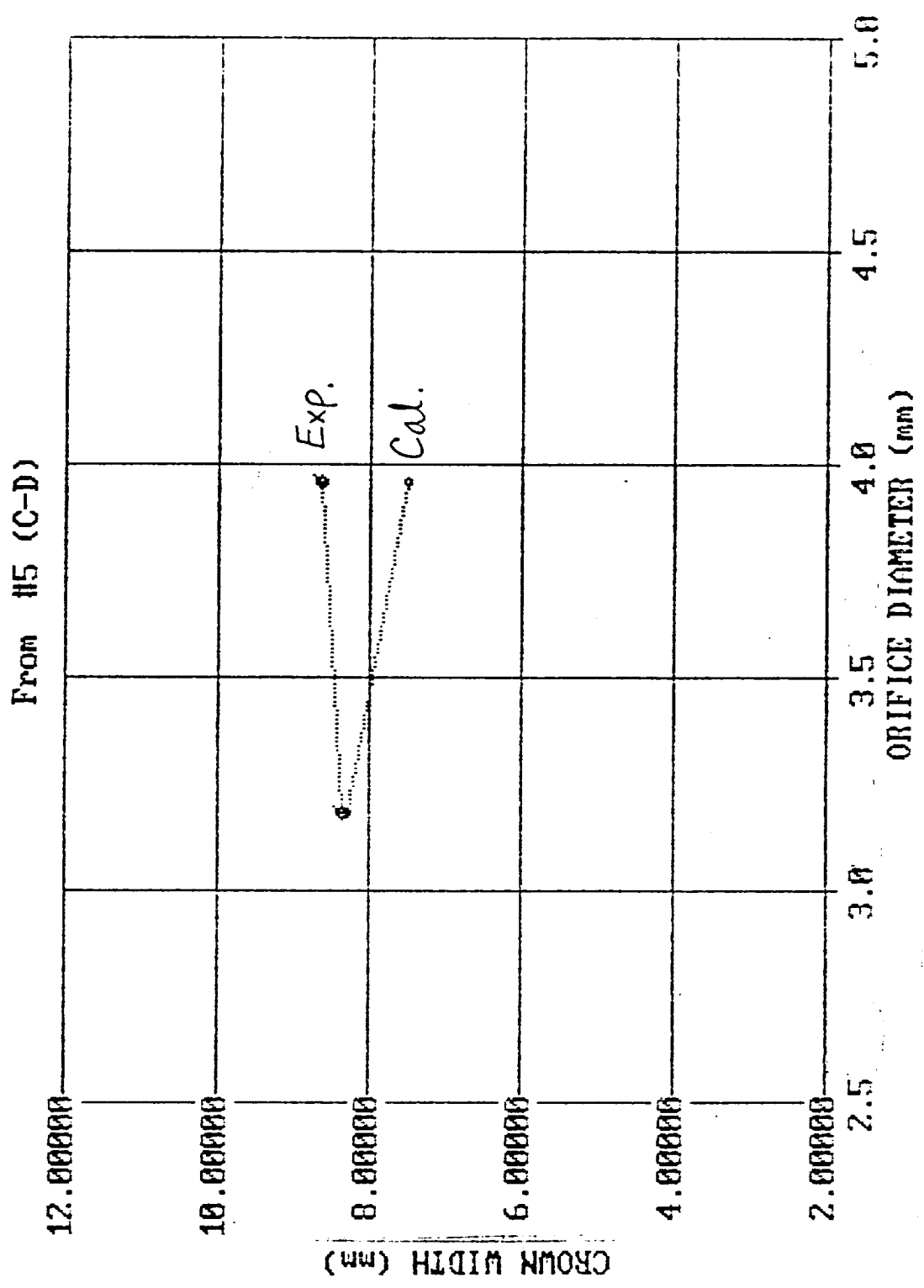


Fig. H-45

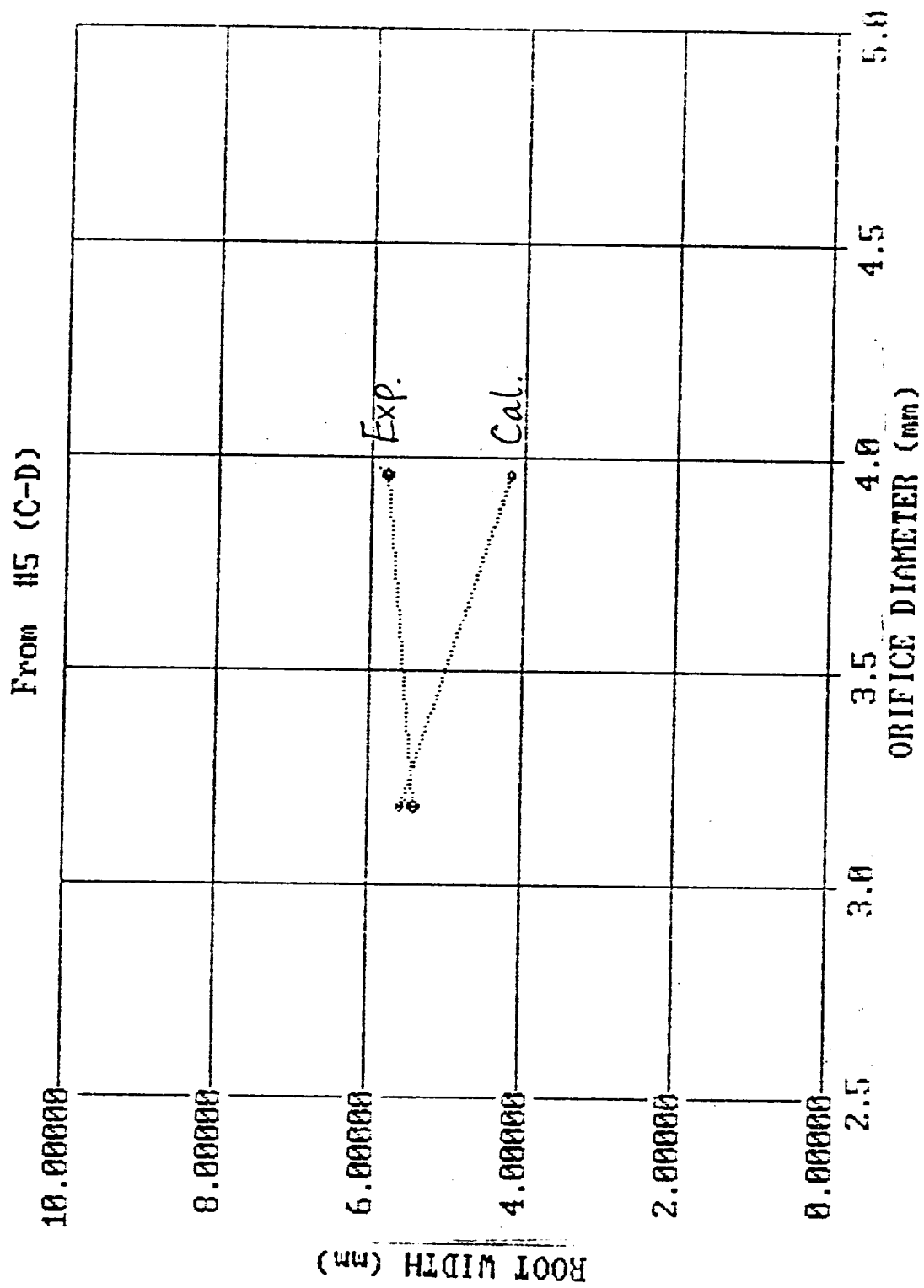


Fig. H-46

From H5 (E-F)

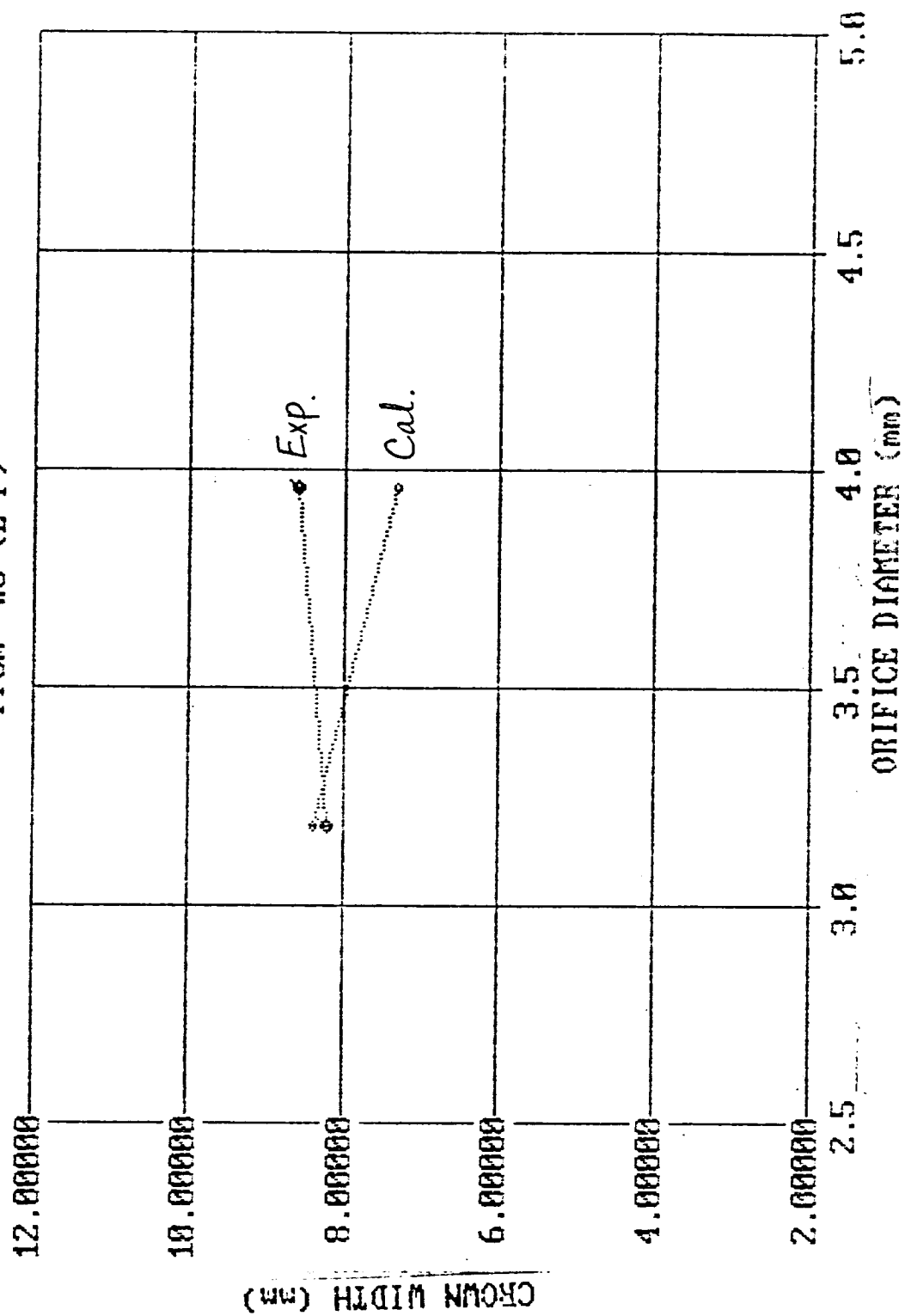


Fig. H-47

From #5 (E-F)

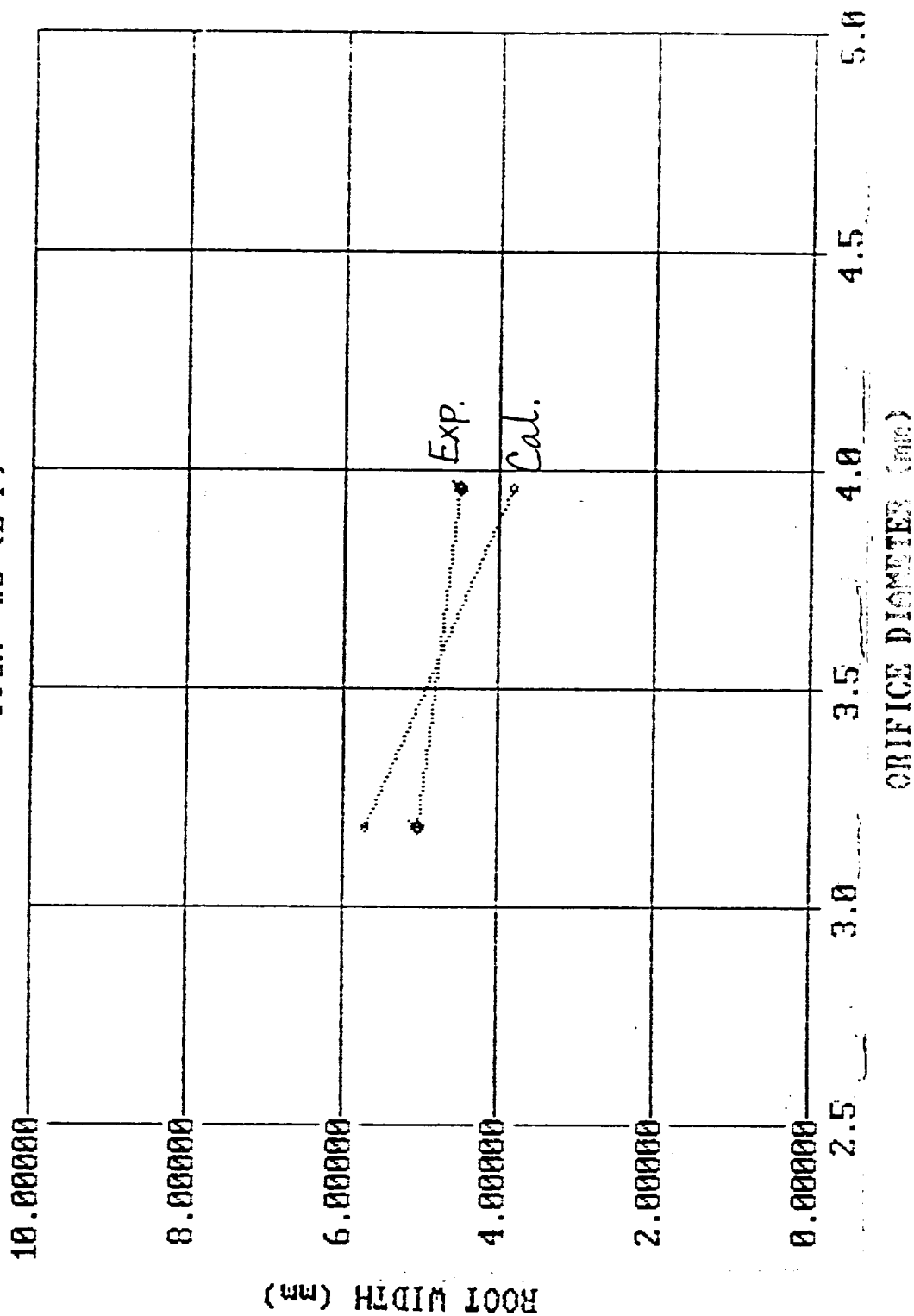


Fig. H-48

ORIGINAL PAGE IS
OF POOR QUALITY

From #5 (G-H)

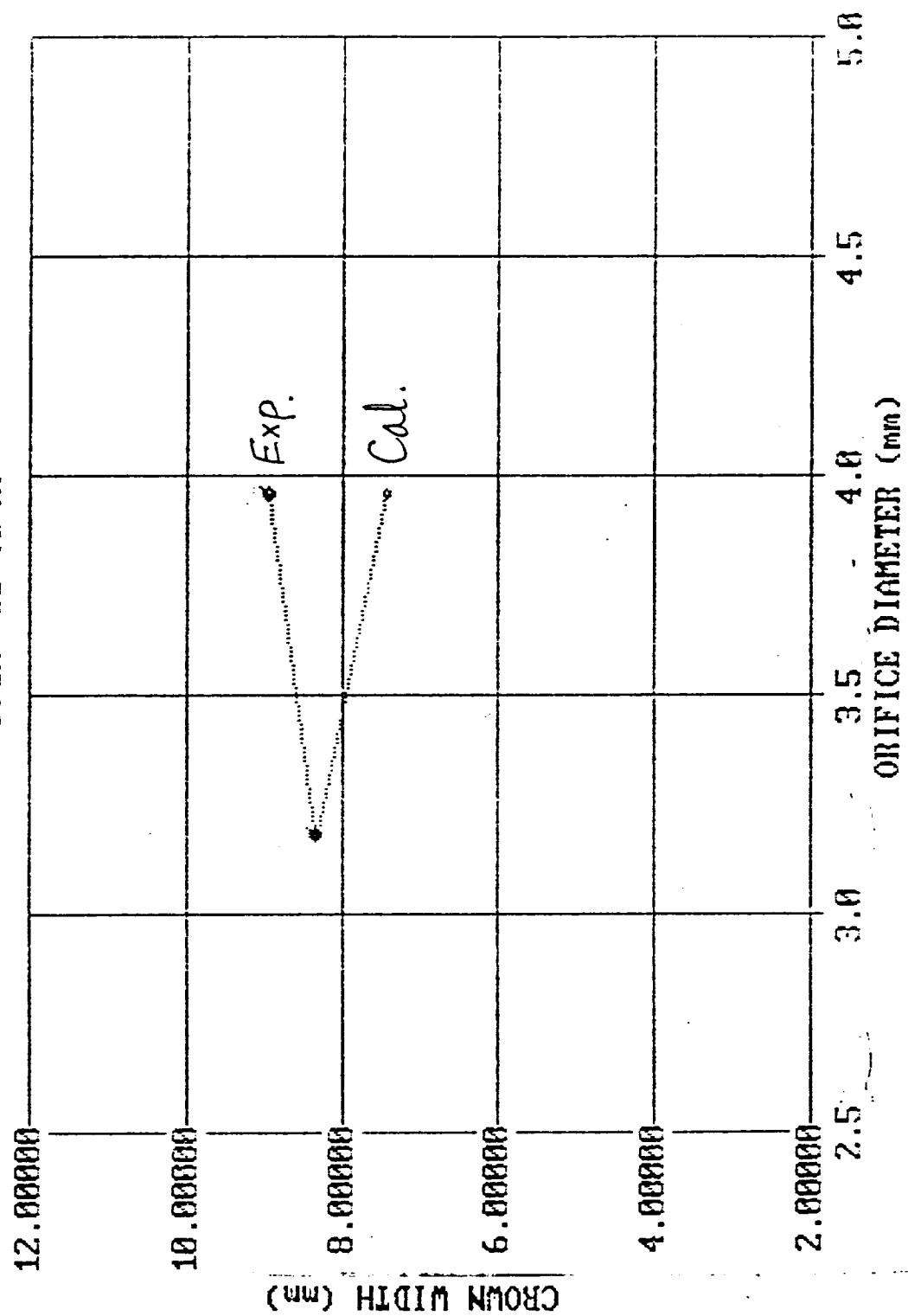


Fig. H-49

From #15 (G-H)

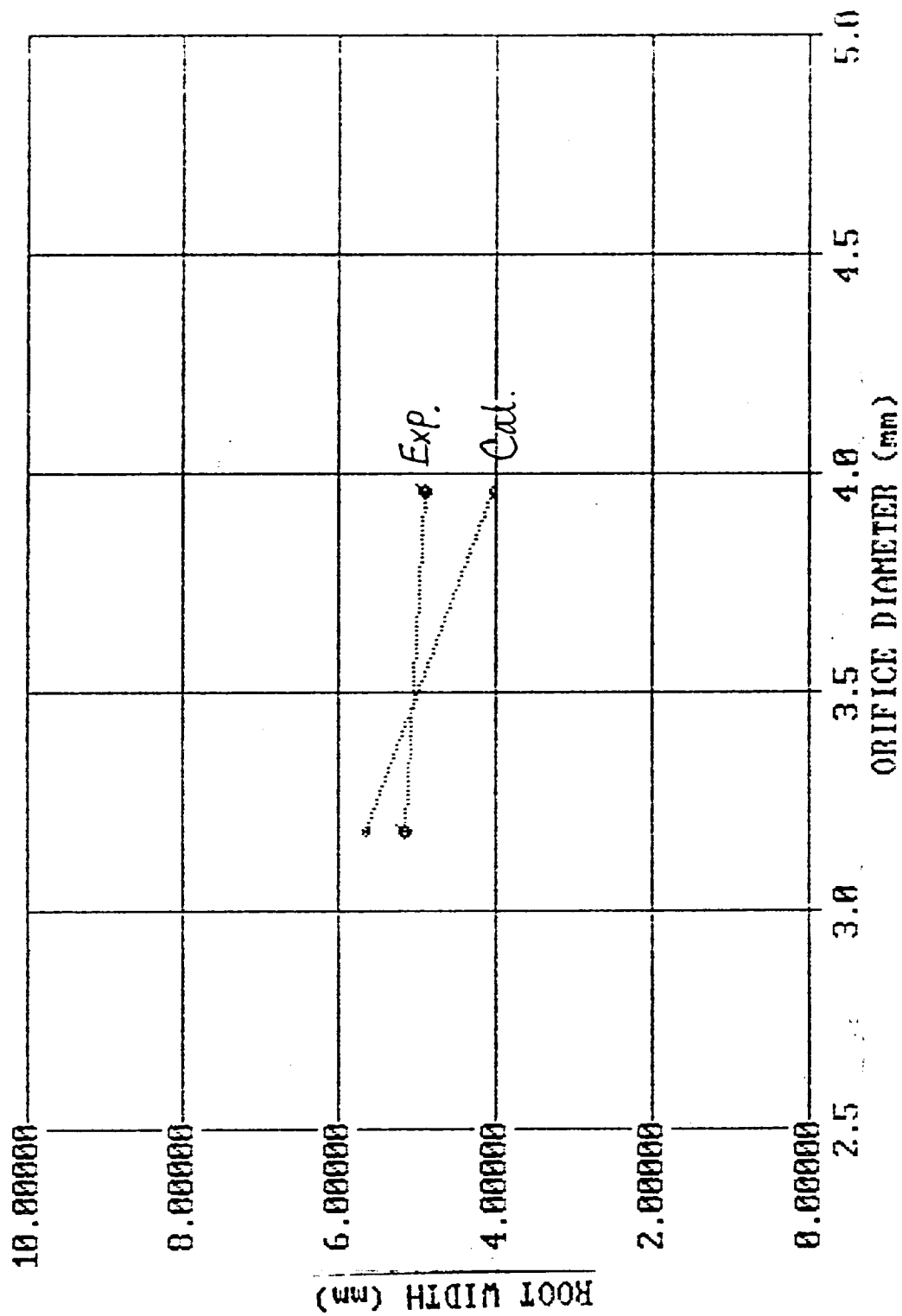


Fig. H-50

From H6 (A B C)

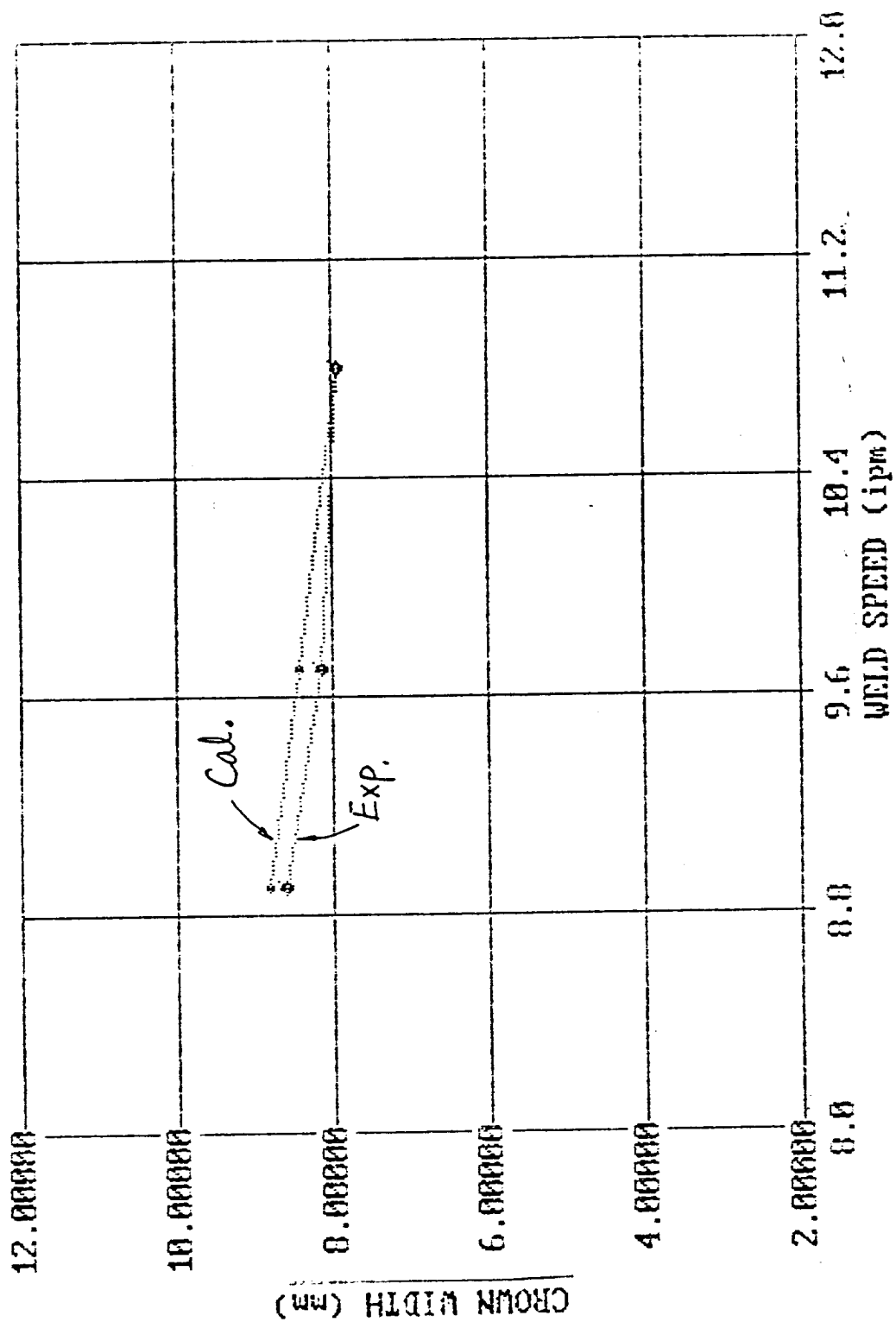


Fig. H-51

From #6 (A B C)

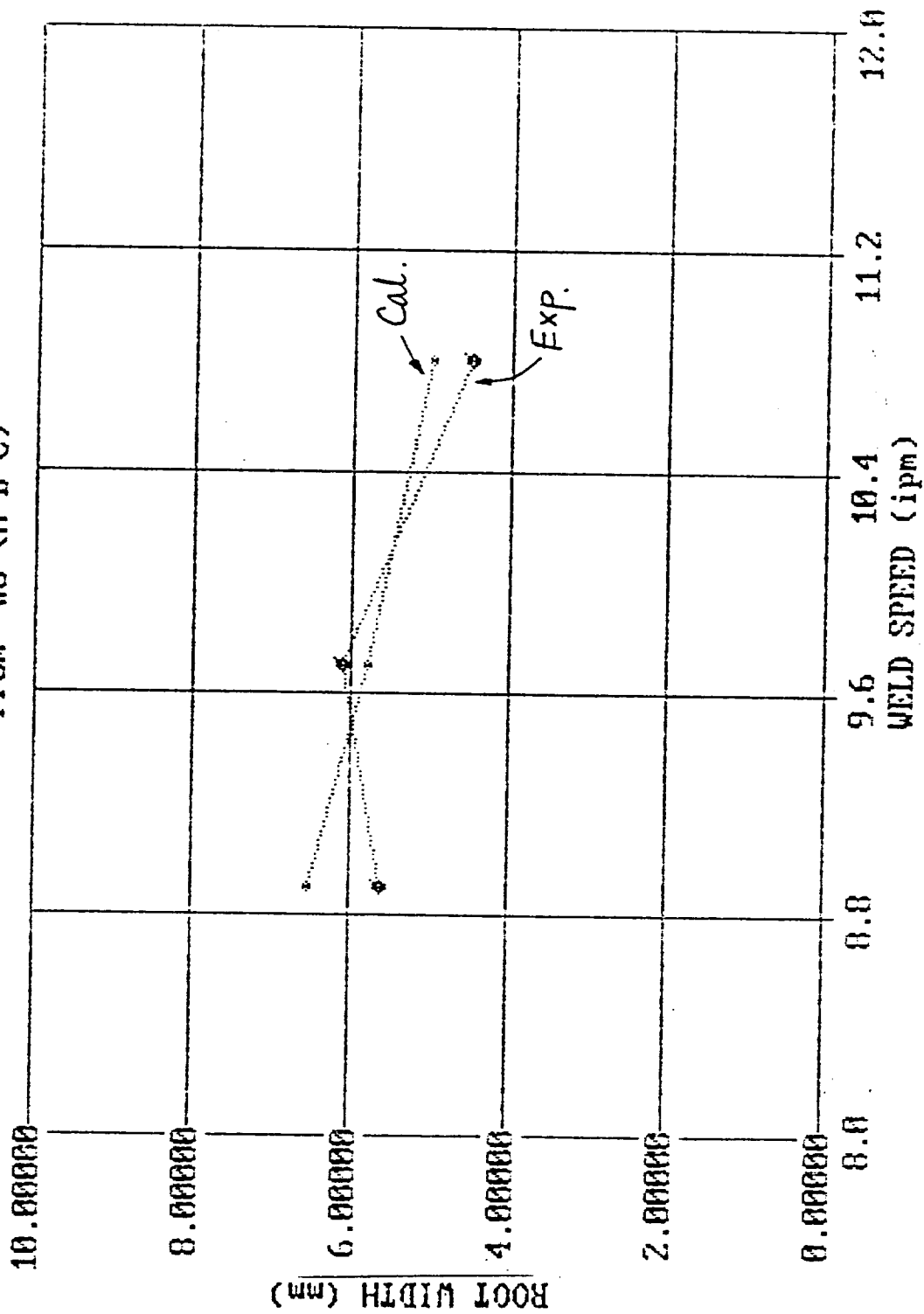


Fig. H-52

From H6 (D E F)

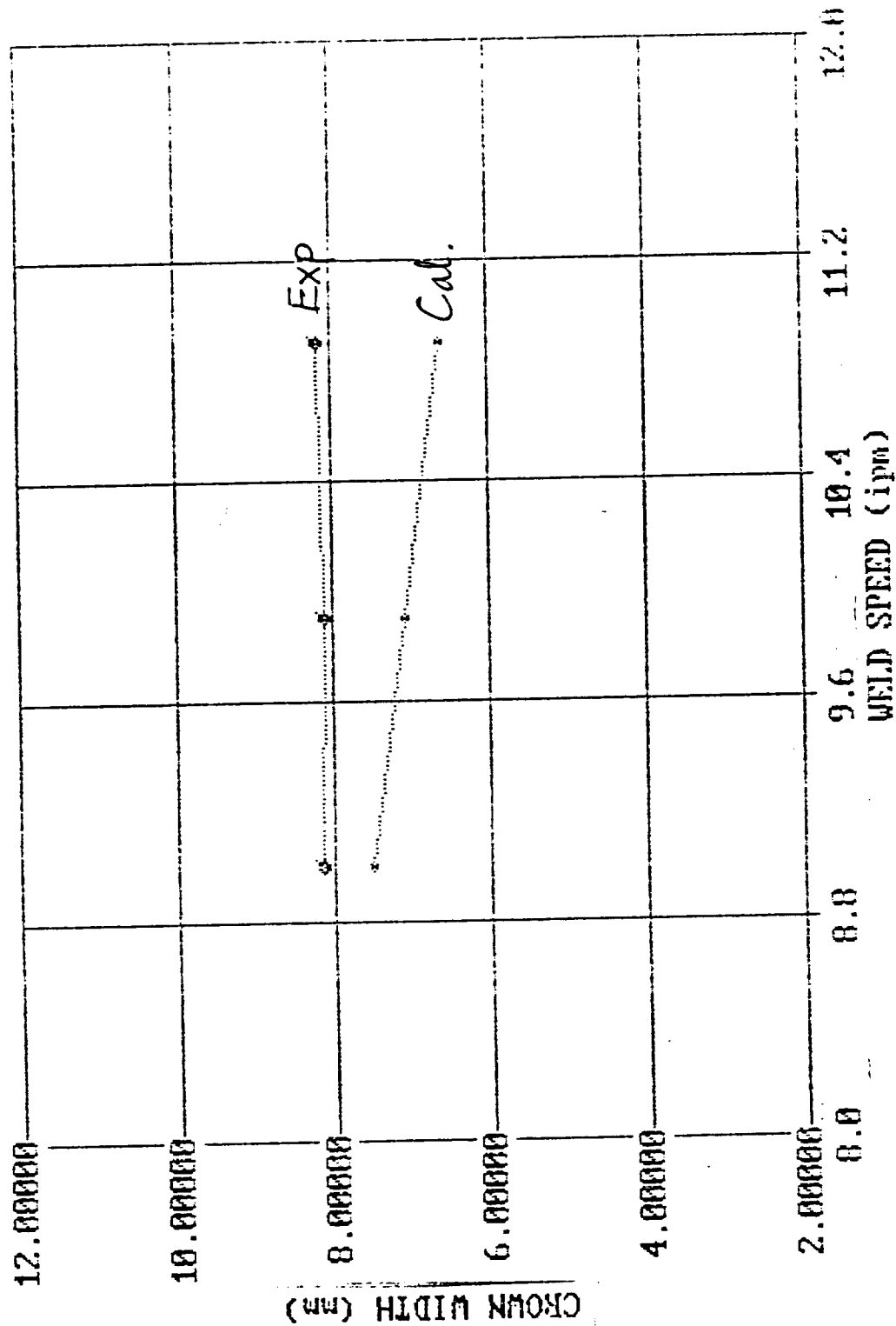


Fig. H-53

From #6 (D E F)

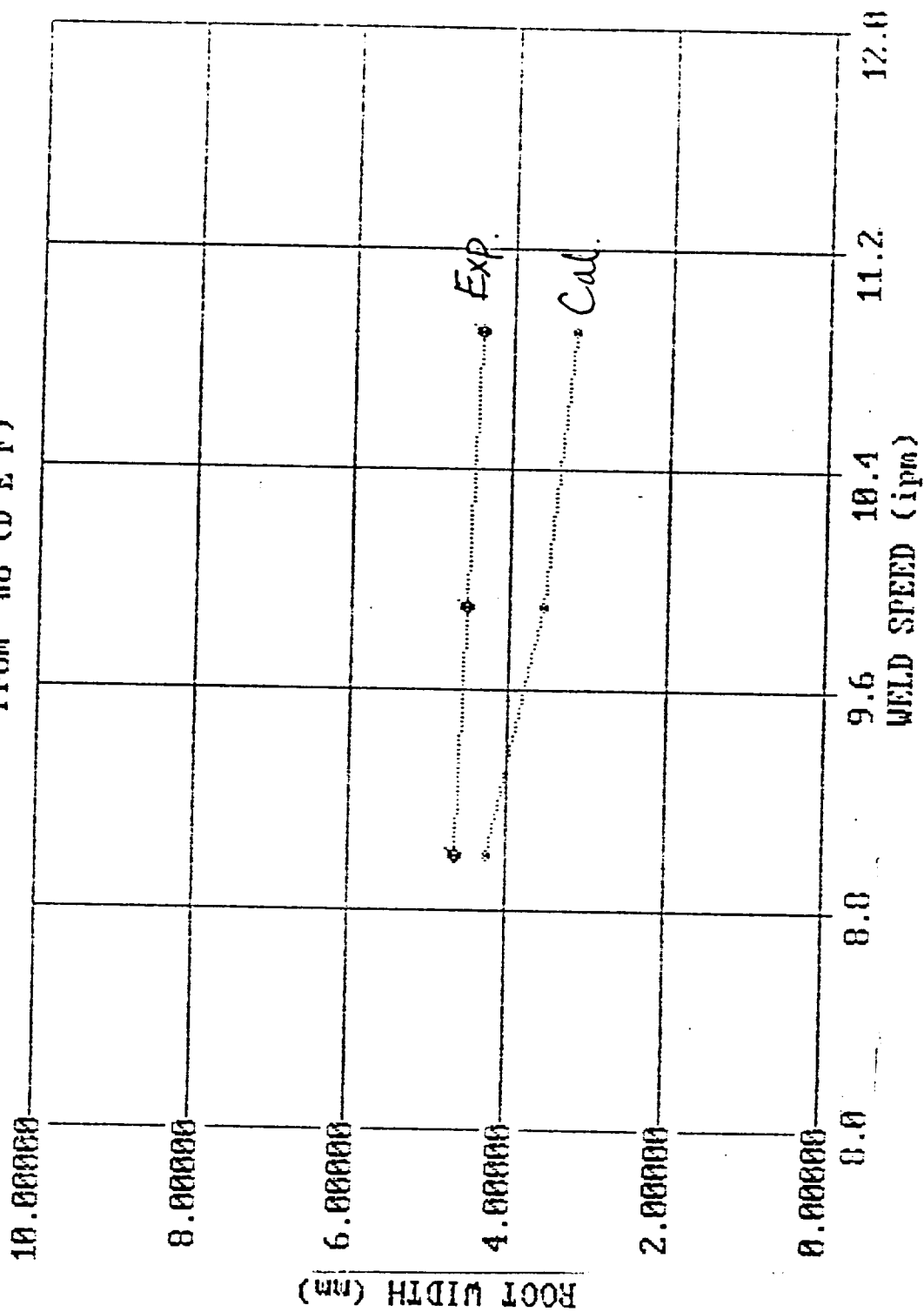


Fig. H-84

From #16 (G H I)

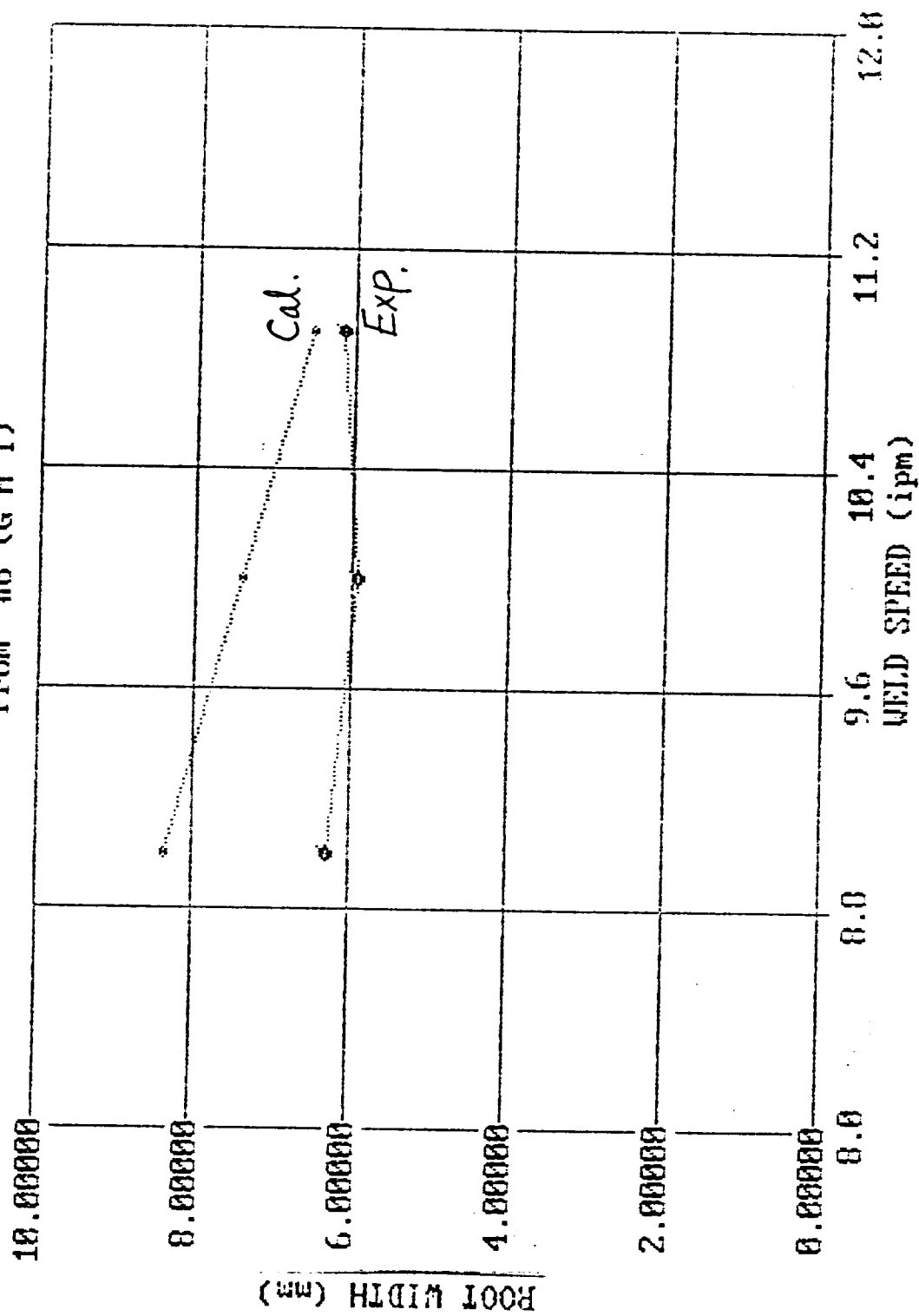


Fig. H-55

From H6 (G H I)

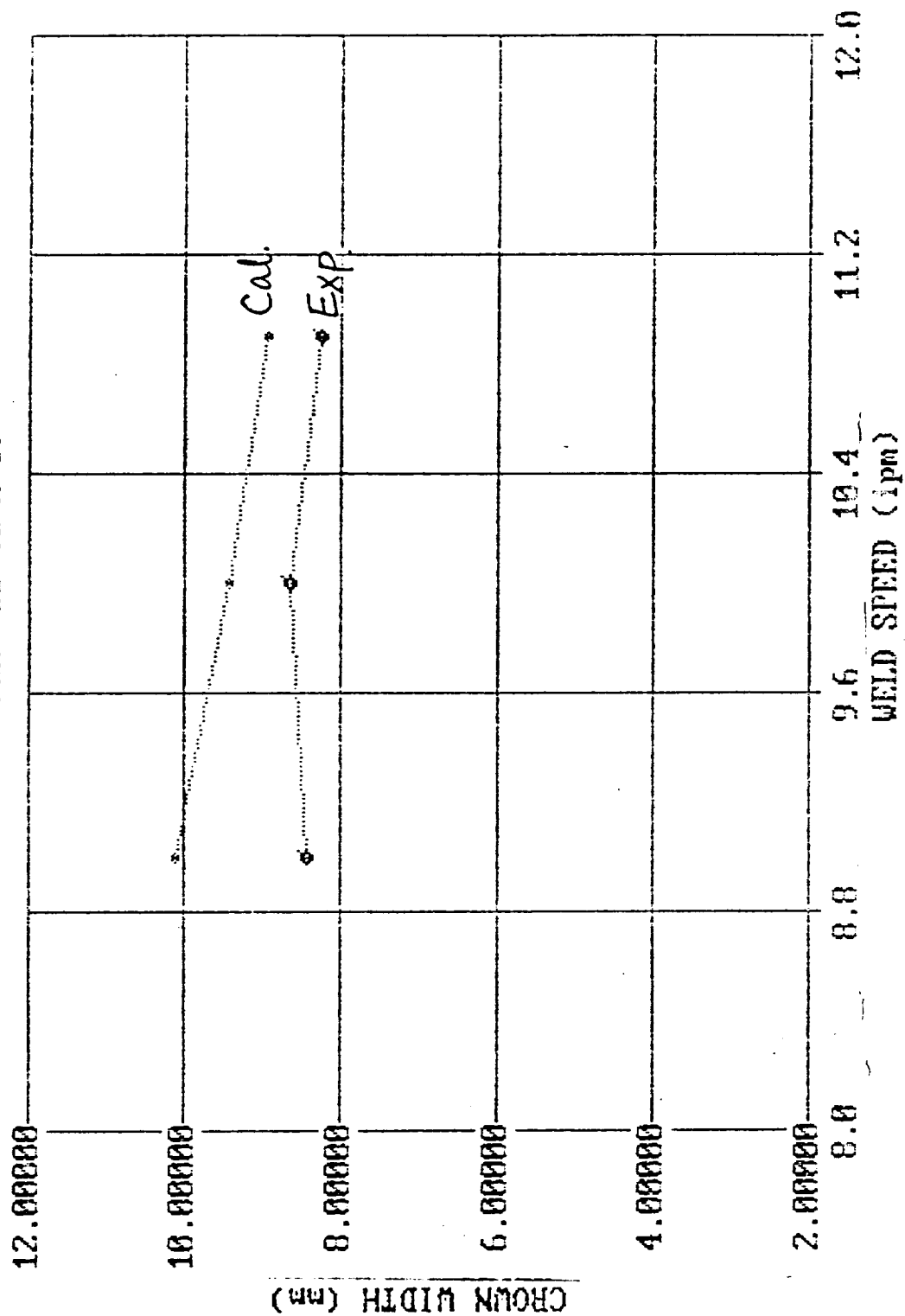


Fig. H-56

From #6 (A E H)

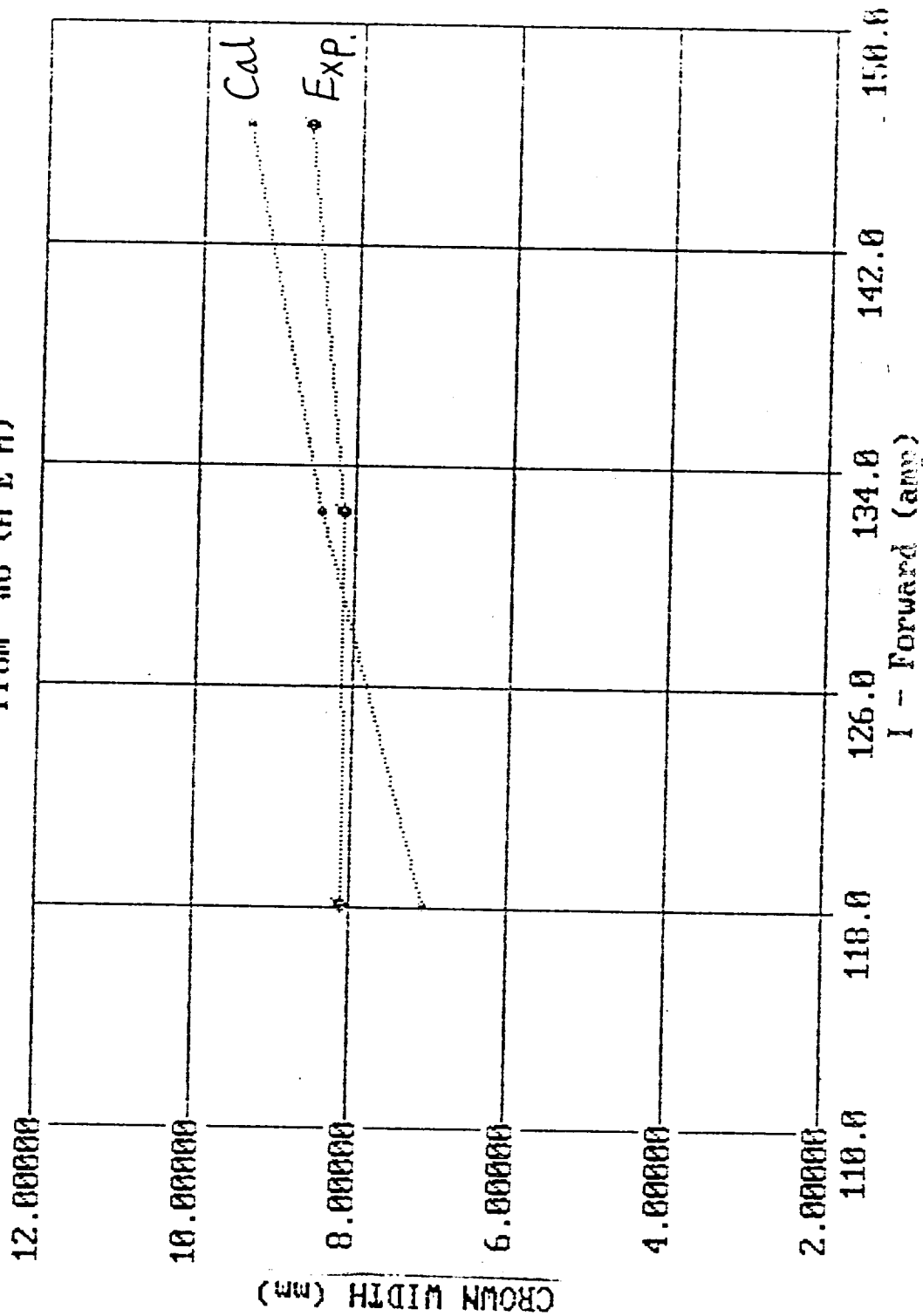


Fig. H-57

From #16 (A E H)

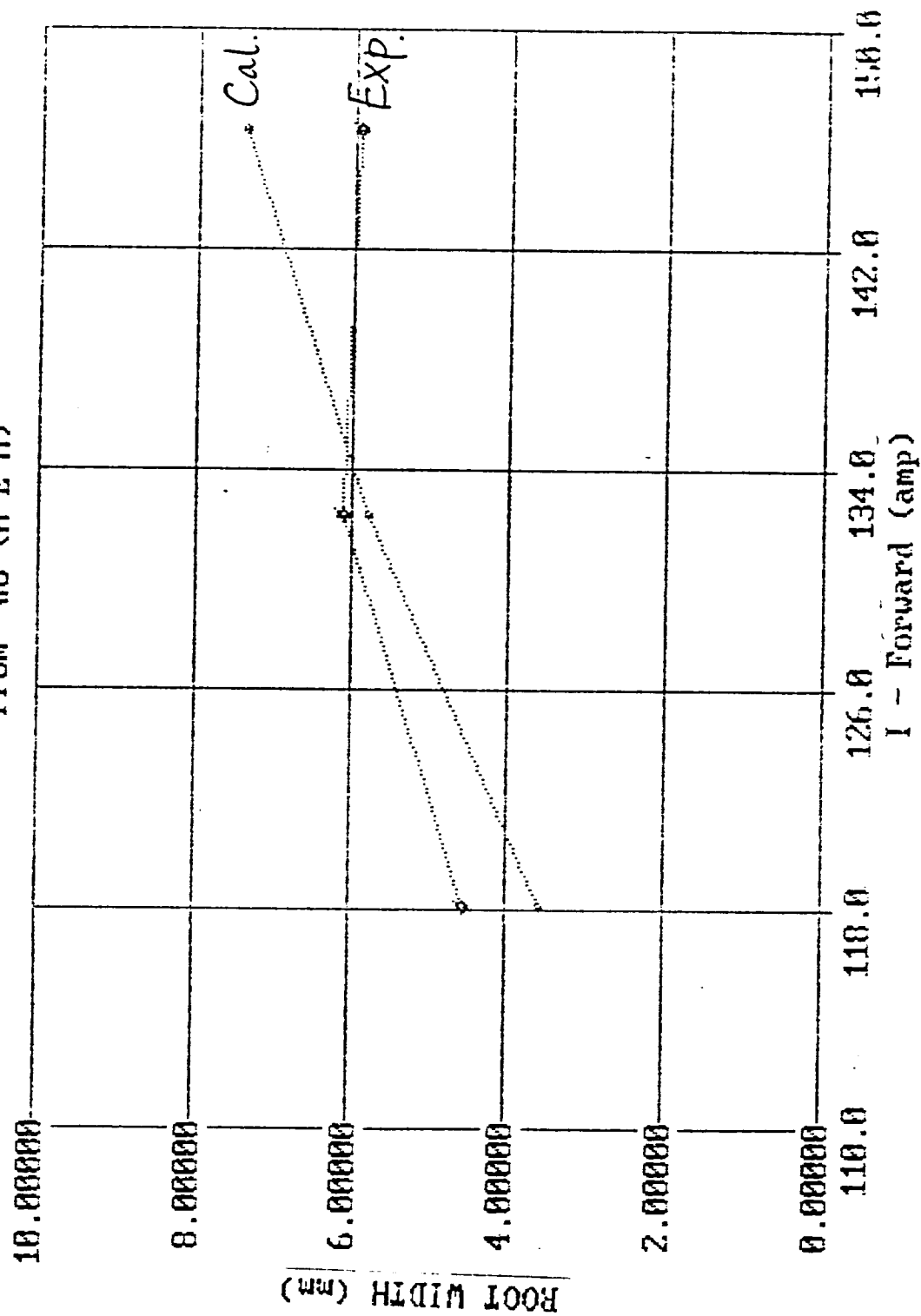


Fig. H-58

From #6 (B D I)

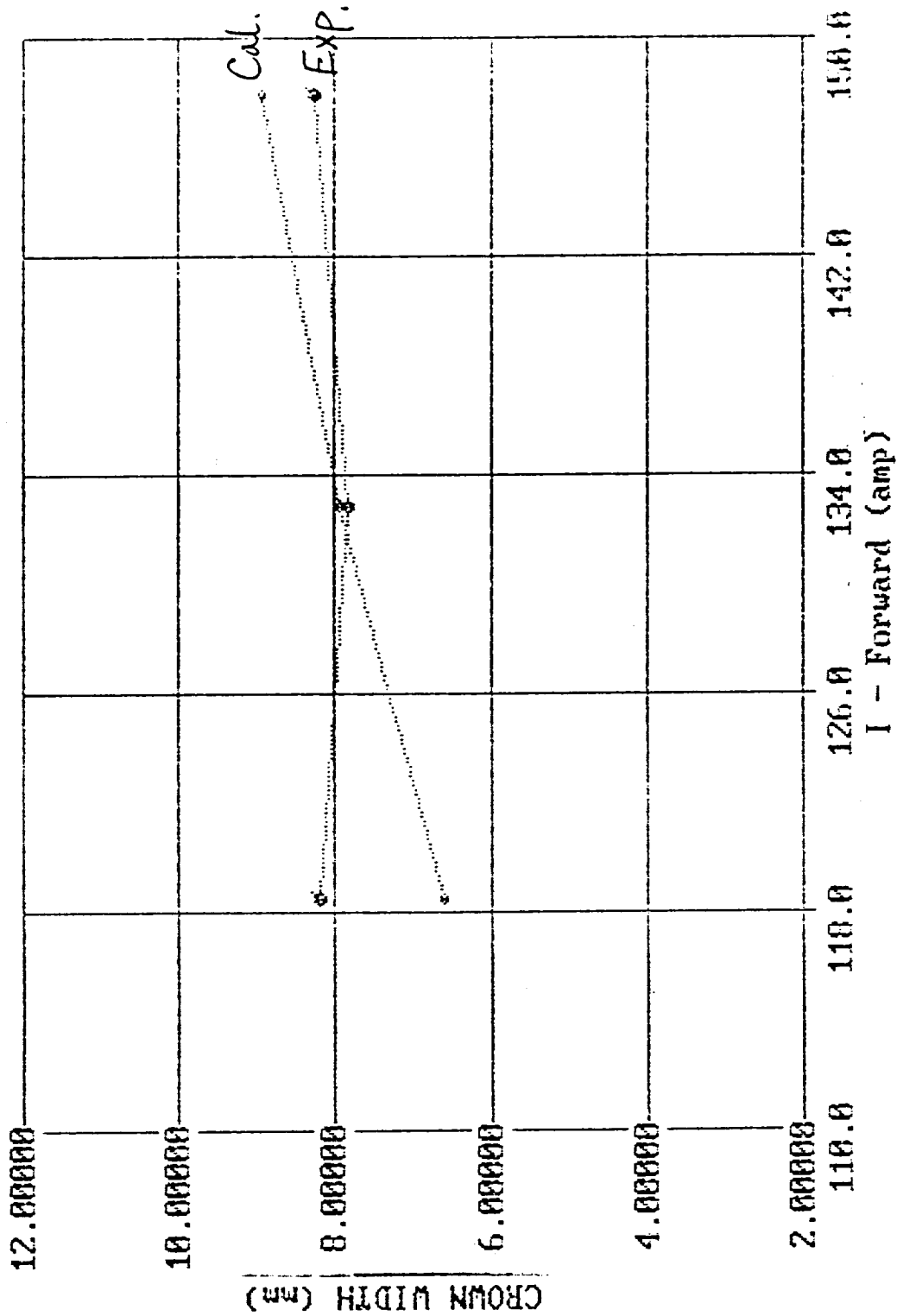


Fig. H-59

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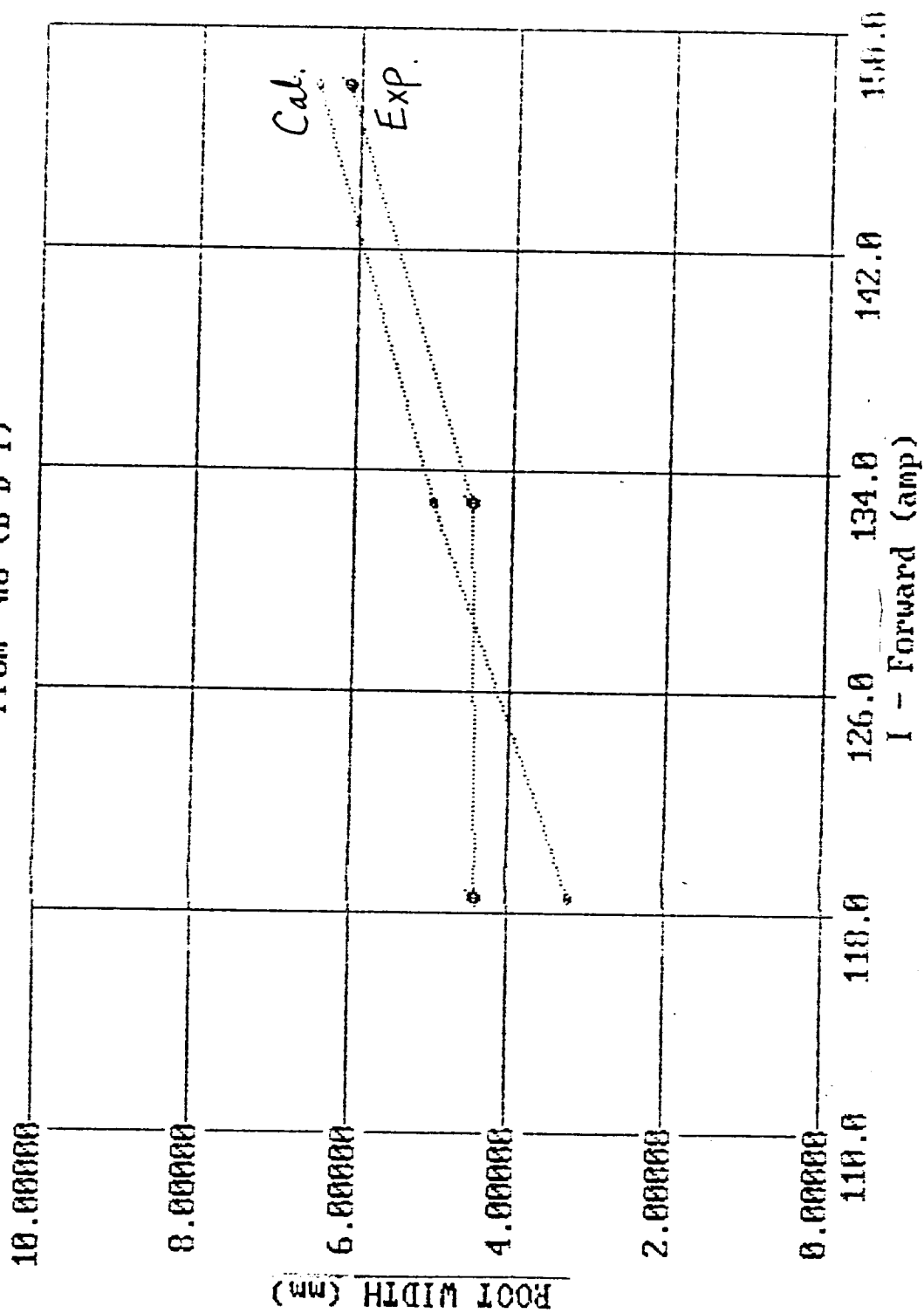


Fig. H-60

From #6 (C F G)

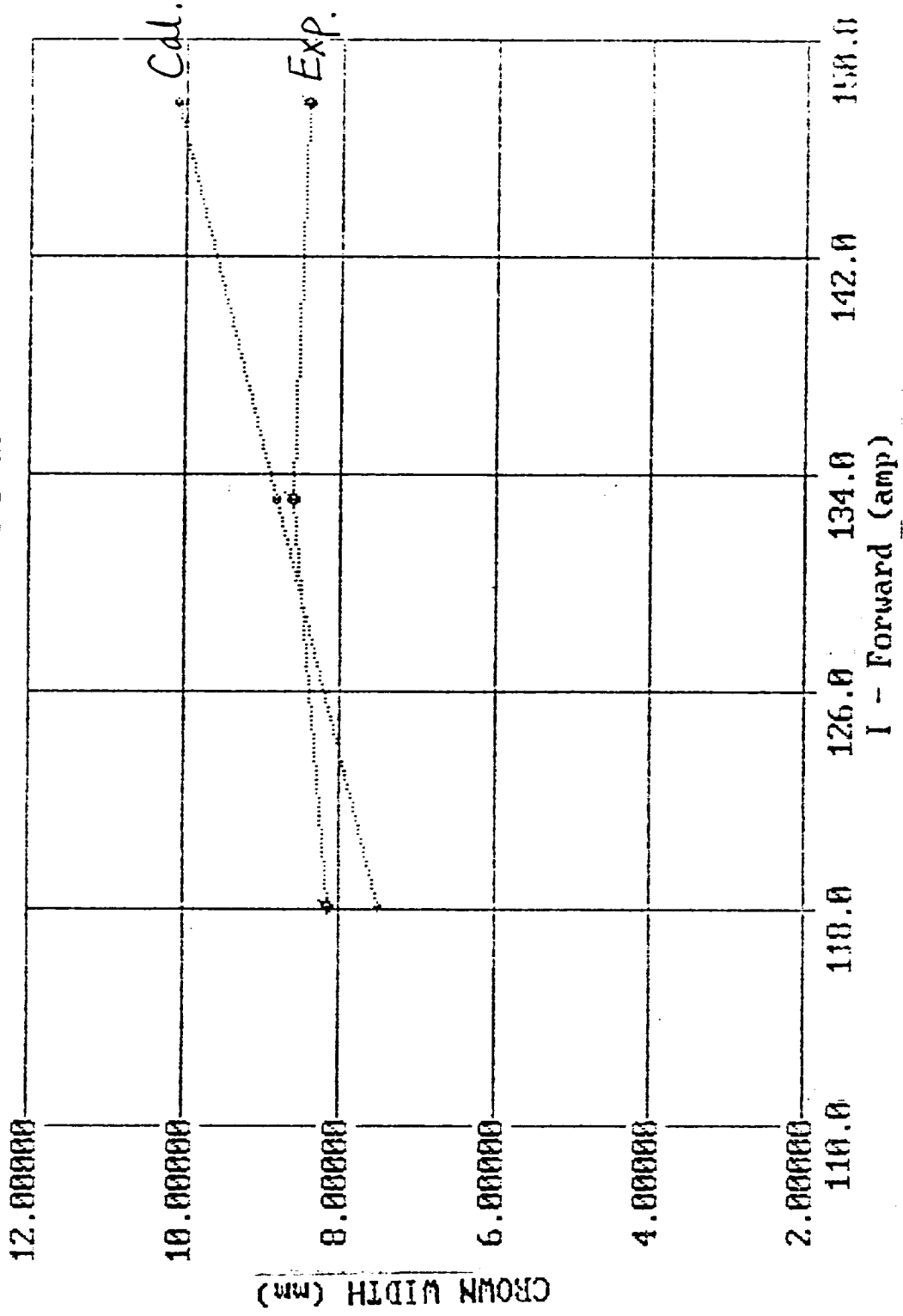


Fig. H-61

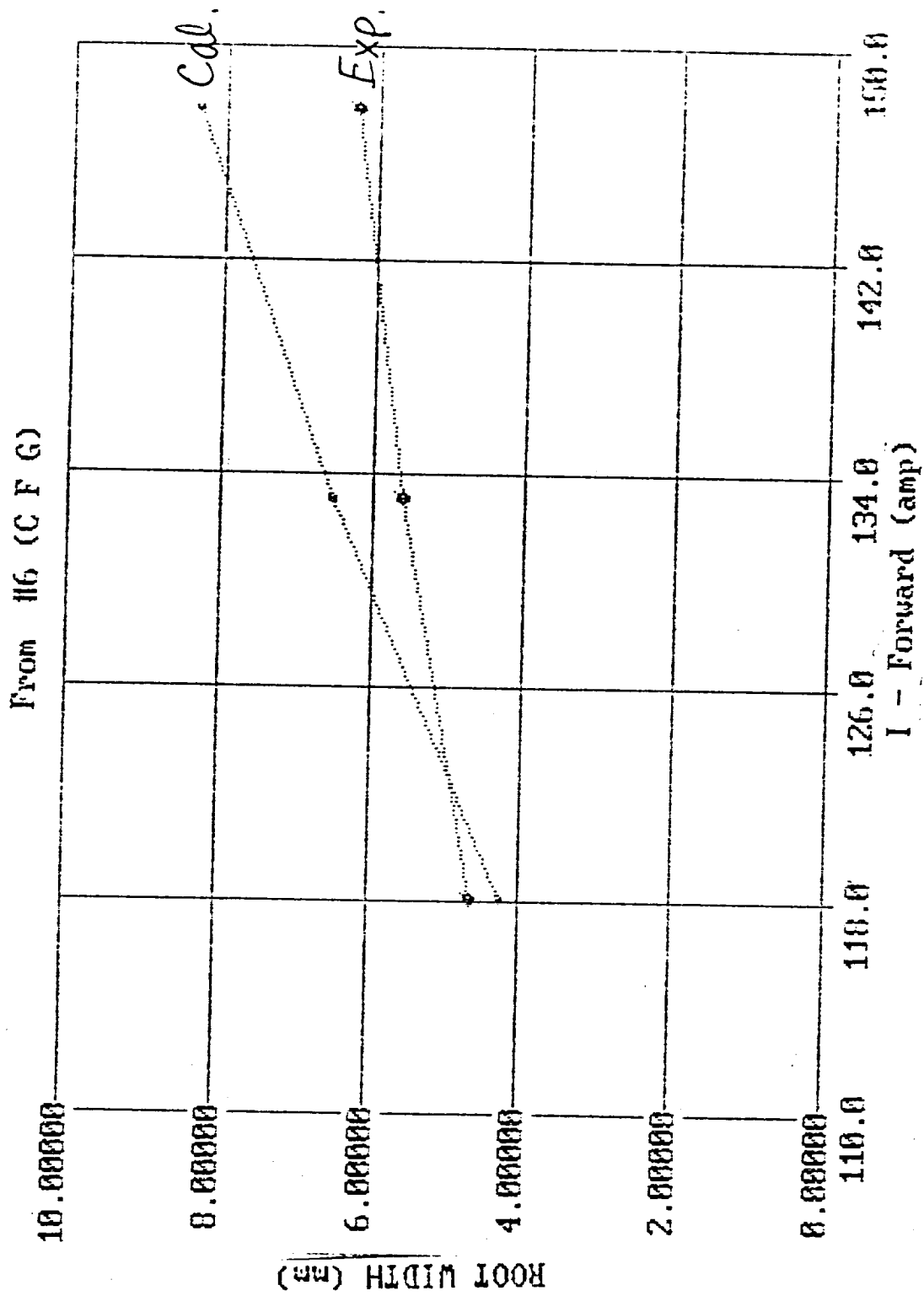


Fig. H-62

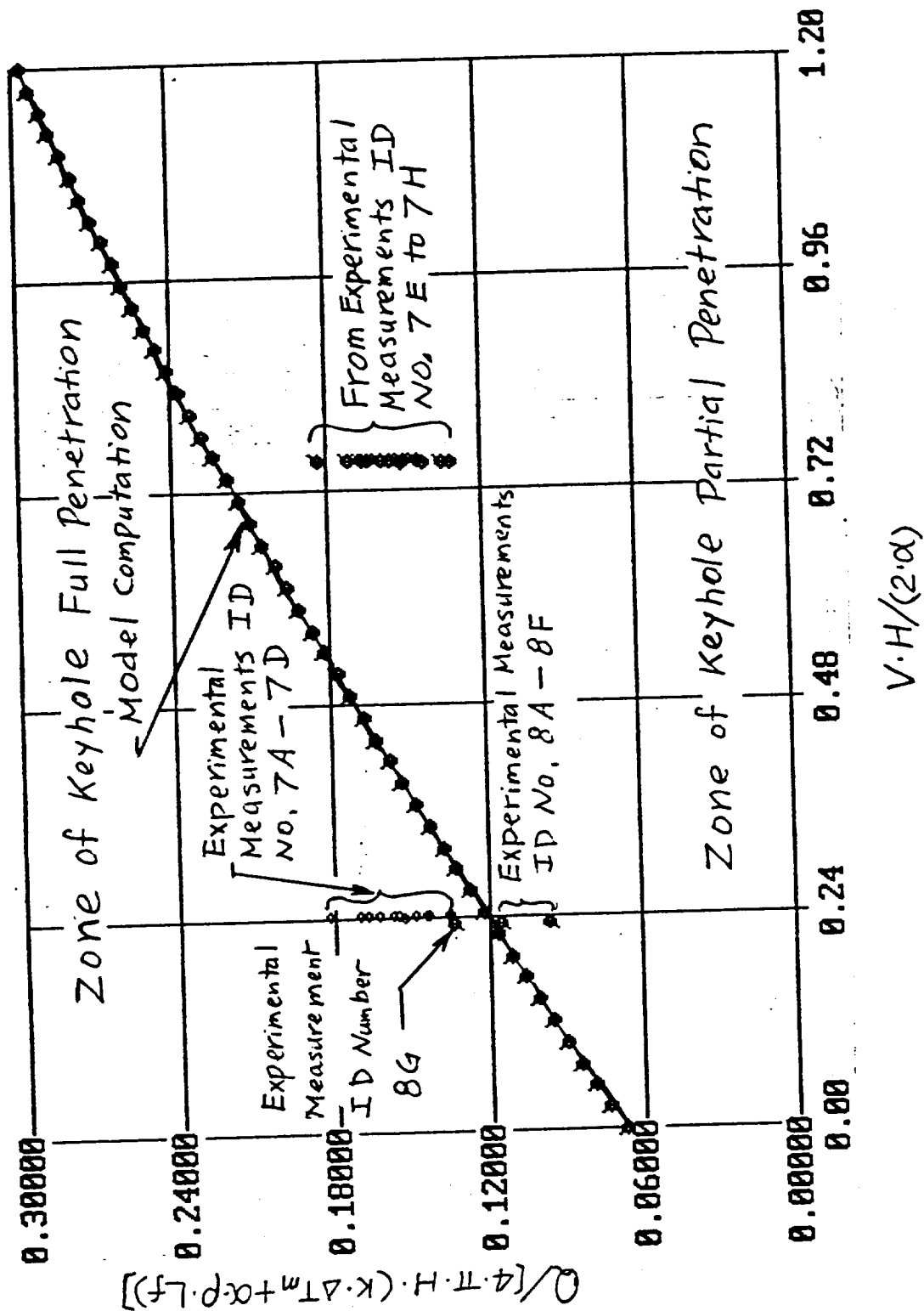


Fig. H-63

Report Document Page

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16. Abstract Significant advantages of Variable Polarity Plasma Arc (VPPA) welding process include faster welding, fewer repairs, less joint preparation, reduced weldment distortion, and absence of porosity. In this report, a mathematical model is have been compared with the experimental observation accomplished by the GDI team.					
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